

WATER RESOURCES

ST. LOUIS AREA MISSOURI

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WATER RESOURCES OF THE ST. LOUIS AREA, MISSOURI

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MISSOURI GEOLOGICAL SURVEY AND WATER RESOURCES

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U.S. GEOLOGICAL SURVEY

PREPARED UNDER A COOPERATIVE AGREEMENT BETWEEN

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WATER RESOURCES OF THE ST. LOUIS AREA, MISSOURI

ABSTRACT

Water supplies in the St. Louis area, Missouri, are available from streams and from bedrock and alluvial aquifers that underlie the region. Of the 1200 million gallons of water used daily, about 82 percent is pumped from the Mississippi River and about 15 percent from the Missouri and Meramec Rivers. Approximately two-thirds of this pumpage is used for cooling in the generation of electric power. The bedrock and alluvial aquifers account for 1 and 2 percent of the total pumpage, respectively.

The bedrock aquifers are primarily dolomite and limestone with one notable exception, the St. Peter Sandstone. Wells finished in these aquifers furnish water to 22 towns, 7 rural water-supply districts and most households not served by a central water supply. The principal bedrock aquifers are the St. Peter, the Roubidoux, the Gasconade, and the Potosi.

Wells yielding more than 50 gpm (gallons per minute) of potable water can be developed in bedrock aquifers in the western one-third of St. Charles County, the extreme western part of St. Louis County, and the southwestern three-fourths of Jefferson County. In these areas, wells finished in the Potosi Dolomite have yielded a maximum of 500 gpm, while others finished in the Gasconade and Roubidoux Formations have yielded a maximum of 300 gpm. Yields of 140 gpm have been reported from wells tapping the St. Peter Sandstone.

Only a small percentage of the water available in the alluvial aquifers of the area is being used. Areas having the greatest potential for development of ground water are in the Mississippi and Missouri River floodplains. Wells reportedly yielding as much

as 3,000 gpm have been drilled in the Mississippi River floodplain in St. Charles County. A yield of over 2,500 gpm has been measured from a well in the Missouri River floodplain. In the Meramec River floodplain, municipal and industrial wells at Valley Park are capable of yielding as much as 500 gpm, while a few miles downstream the city of Kirkwood has a collector well capable of pumping 2.6 mgd (million gallons per day). Water from the alluvial deposits generally is a very hard calcium-magnesium-bicarbonate type with iron and manganese content commonly being high. Saline water has moved upward from the underlying bedrock into the alluvial aquifers at Valley Park and Times Beach in the Meramec River valley and in the Mississippi River valley near St. Peters. This upward leakage may be a naturally occurring phenomenon, but part of it probably is through boreholes of abandoned deep wells or test holes.

The median 7-day low flows of small unregulated tributary streams generally range from 0 to 0.005 cfs (cubic feet per second) per square mile in the northern two-thirds of the area and from 0.02 to 0.05 cfs per square mile elsewhere. These values can be as high as 0.3 cfs per square mile in urban areas because of augmentation from sewage treatment plants. Because the natural low flow of many of these tributary streams is less than 0.5 cfs, an influx of poor-quality effluent, even though in small amounts, will be enough to seriously degrade the water quality in the stream.

Except for larger streams such as the Meramec, Big, and Cuivre Rivers, storage facilities would be required to develop dependable surface-water supplies

in the tributary basins. The principal factors limiting future development will be a lack of natural sustained low flows and the quality of the water, which is often very poor in urbanized areas and requires extensive treatment prior to use.

Flooding can occur in the area during all months, but is most common in the March-through-July period. Many of the larger floods on record were caused by intense, local summer thunderstorms. Analysis of data from an urbanized basin in the area

indicates that peak flows are increased at least one-and-a-half to two times by significant urbanization.

Quality of surface water varies from good in the tributary streams of southern Jefferson County to very poor in the highly urbanized areas. The major sources of surface-water supplies are the Missouri, Mississippi and Meramec Rivers. Except for water used for once-through cooling, extensive treatment of water from these streams is required prior to use for domestic and most manufacturing purposes.

INTRODUCTION

PURPOSE AND SCOPE

A consistent pattern of rapid growth during the past two decades has increasingly concentrated people and activities around metropolitan areas such as St. Louis. This concentration has caused a multitude of problems with some of the most pressing being in the field of water resources, where coordinated planning is essential to optimum management.

The purpose of this report is to summarize and interpret hydrologic data presently available for St.

Louis, St. Charles and Jefferson Counties; to evaluate the water resources of the area; and to relate water needs to available supplies.

A generalized description of the hydrologic effects of urbanization in the area is also presented. Data now being collected on small urban and rural streams in St. Louis County will eventually provide more precise design data for use by urban planners and water managers.

COOPERATION AND ACKNOWLEDGMENTS

This report is the result of a cooperative study conducted by the Missouri Geological Survey and Water Resources (Dr. William C. Hayes, State Geologist and Director, succeeded by Dr. Wallace B. Howe) and the U.S. Geological Survey (Anthony Homyk, District Chief, Missouri District).

Appreciation is expressed to the Missouri Clean Water Commission (formerly the Missouri Water Pollution Board), the City of St. Louis (Water Division), and the St. Louis County Water Company for their assistance in the collection of water-quality information.

Thanks are also due the State Highway Depart-

ment, drilling contractors, and many homeowners who furnished information and helped in collecting supporting data.

The authors drew heavily on hydrogeologic data collected over a period of many years by the Missouri Geological Survey and Water Resources. Of particular value were the extensive well-log files accumulated by the Missouri Geological Survey through the cooperation of many well-drilling contractors throughout the state and data obtained through a continuing cooperative stream-gaging program between the Missouri Geological Survey and the U.S. Geological Survey.

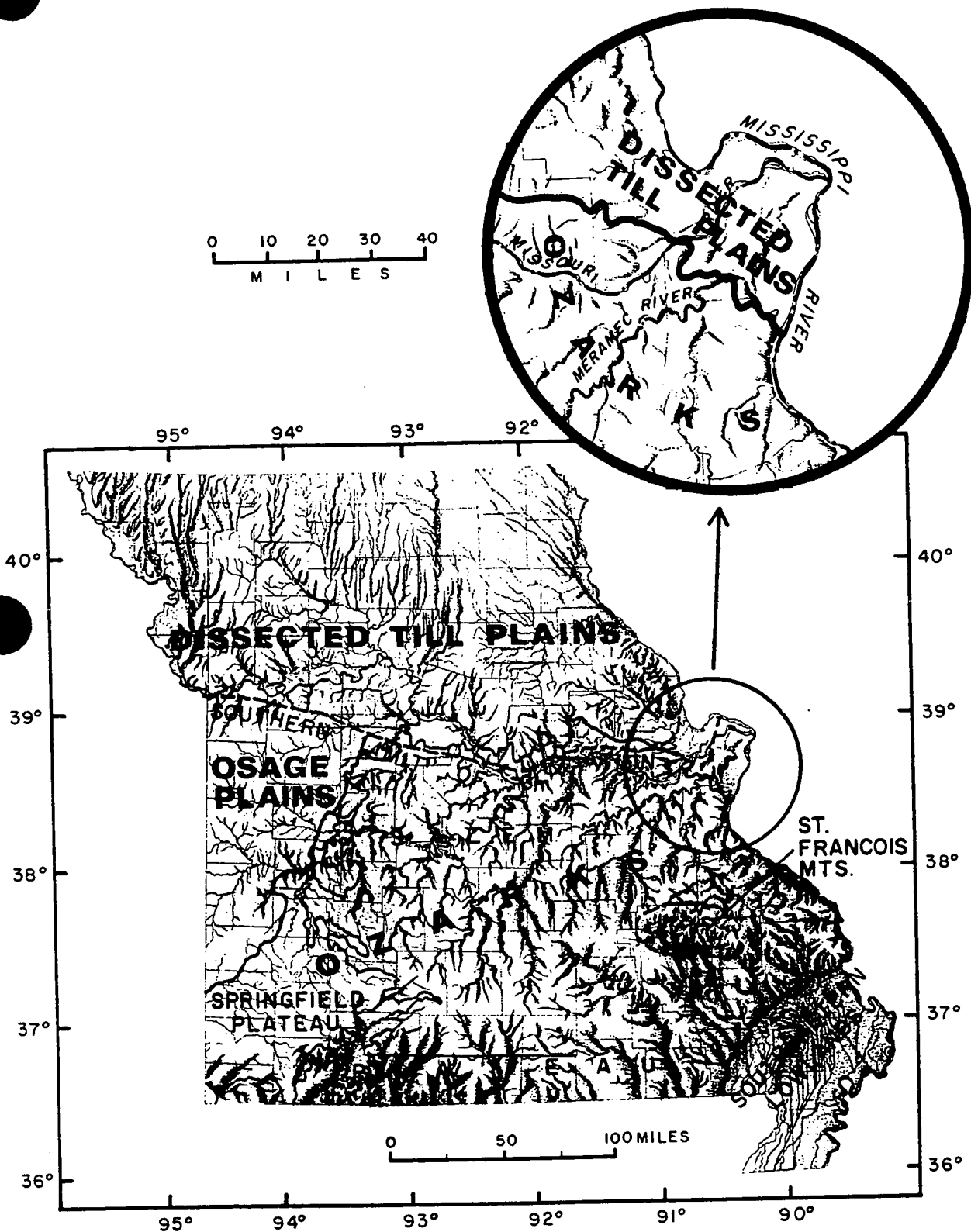


Figure 1

Location and physiography of study area.

GEOGRAPHY

The study area (fig. 1) is in a part of eastern Missouri which includes the confluence of two of the nation's largest rivers — the Missouri and the Mississippi. A diversity of land forms and drainage features are included in the area encompassed by St. Louis, St. Charles and Jefferson Counties.

The area lies within two physiographic provinces. The northeastern two-thirds of St. Charles and St. Louis Counties and the extreme northeastern part of Jefferson County, adjacent to the Meramec River, lie within the Dissected Till Plains. The remainder of the area lies within the Salem Plateau of the Ozarks (Fenneman, 1946).

The Dissected Till Plains is gently undulating, with altitudes ranging from 500 to 700 feet. The morainal topography seen over much of the adjacent glaciated areas is noticeably lacking here. This particular area was glaciated twice during the Pleistocene, but the till deposits are thin and dissected.

The topography developed in the Ozarks province of the study area is submature to mature. The

uplands may be broad flats, but are generally thoroughly dissected while most of the divides are narrow and irregular. Topographic slopes are locally reflections of the regional dip of from 60 to 80 feet per mile to the northeast. Variations in hardness of the Paleozoic rocks are shown by escarpments on the more resistant formations. These escarpments face southwestward, more or less parallel to the Ozark uplift (Marbut, 1896). Altitudes in the Ozarks range from 650 to 1,000 feet, except in the stream valleys where altitudes are from 400 to 650 feet.

All runoff from the land surface in the area eventually reaches the Mississippi or Missouri Rivers through a network of tributary streams that form a dendritic drainage pattern (fig. 2). The floodplains of each of these two great rivers are as much as 11 miles wide in some places and are bordered by loess-covered uplands.

Practically all of the area is shown on modern 7½-minute topographic maps (fig. 3). The balance has 15-minute topographic map coverage.

WELL LOCATION SYSTEM

Wells used in this report are located in accordance with the Bureau of Land Management Survey system, in this order: township, range, section, quarter section, quarter-quarter section and quarter-quarter-quarter section (10-acre tract). The sub-

divisions of a section are designated a, b, c, and d in counterclockwise direction beginning in the northeast quarter. If several wells are in a 10-acre tract, they are numbered serially after the above letters, and in the order in which they were inventoried (fig. 4).

GEOLOGY

It is beyond the scope of this report to describe in detail the stratigraphic and structural setting of the study area. It will be necessary, however, to acquaint the reader with the rock units and their structural attitudes so that references to these rocks as aquifers

can be understood. Numerous published and unpublished stratigraphic studies have been made in this area and the reader is referred to these (Stout, 1969, p. 50-57) for more detailed geologic information.

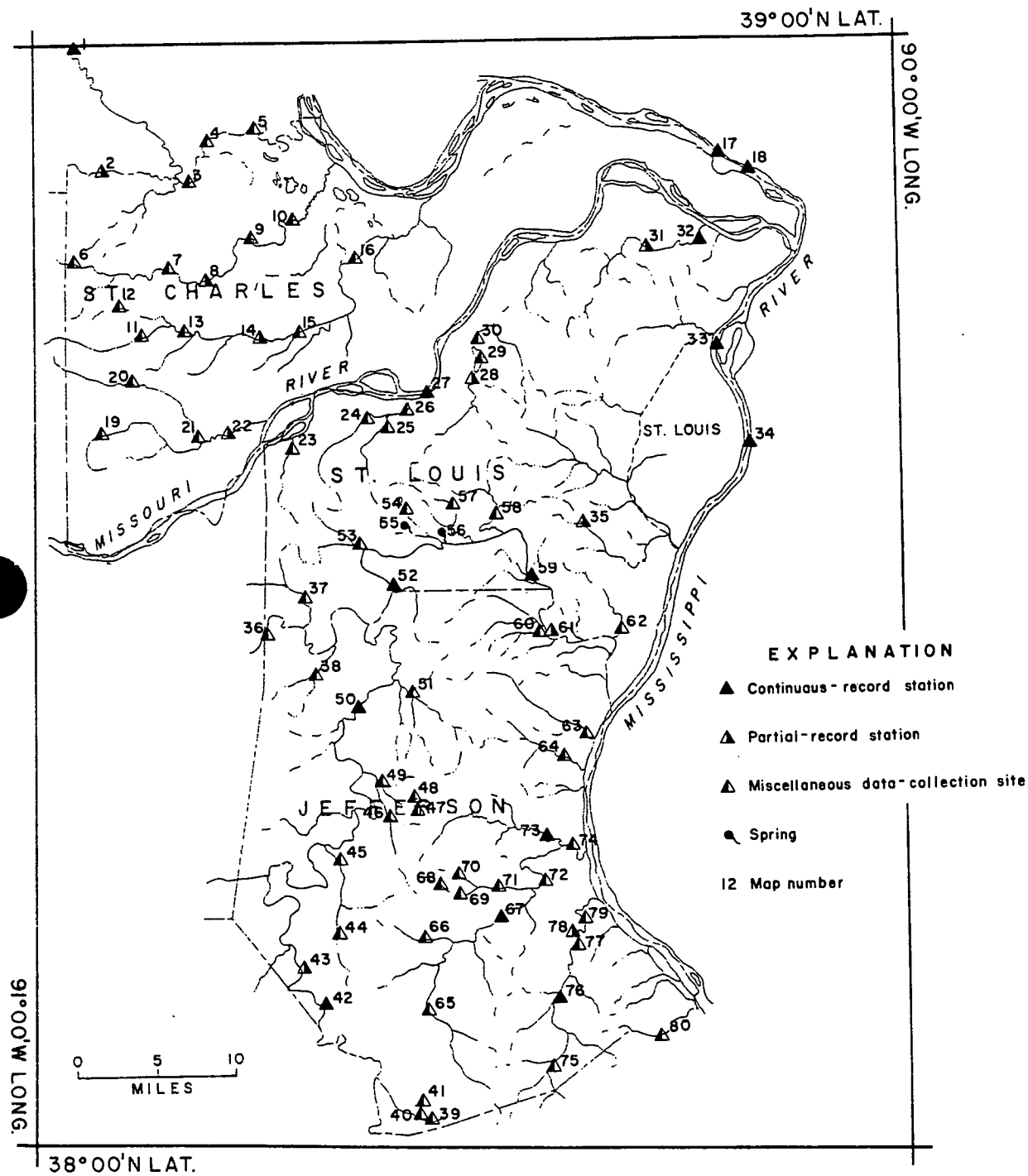
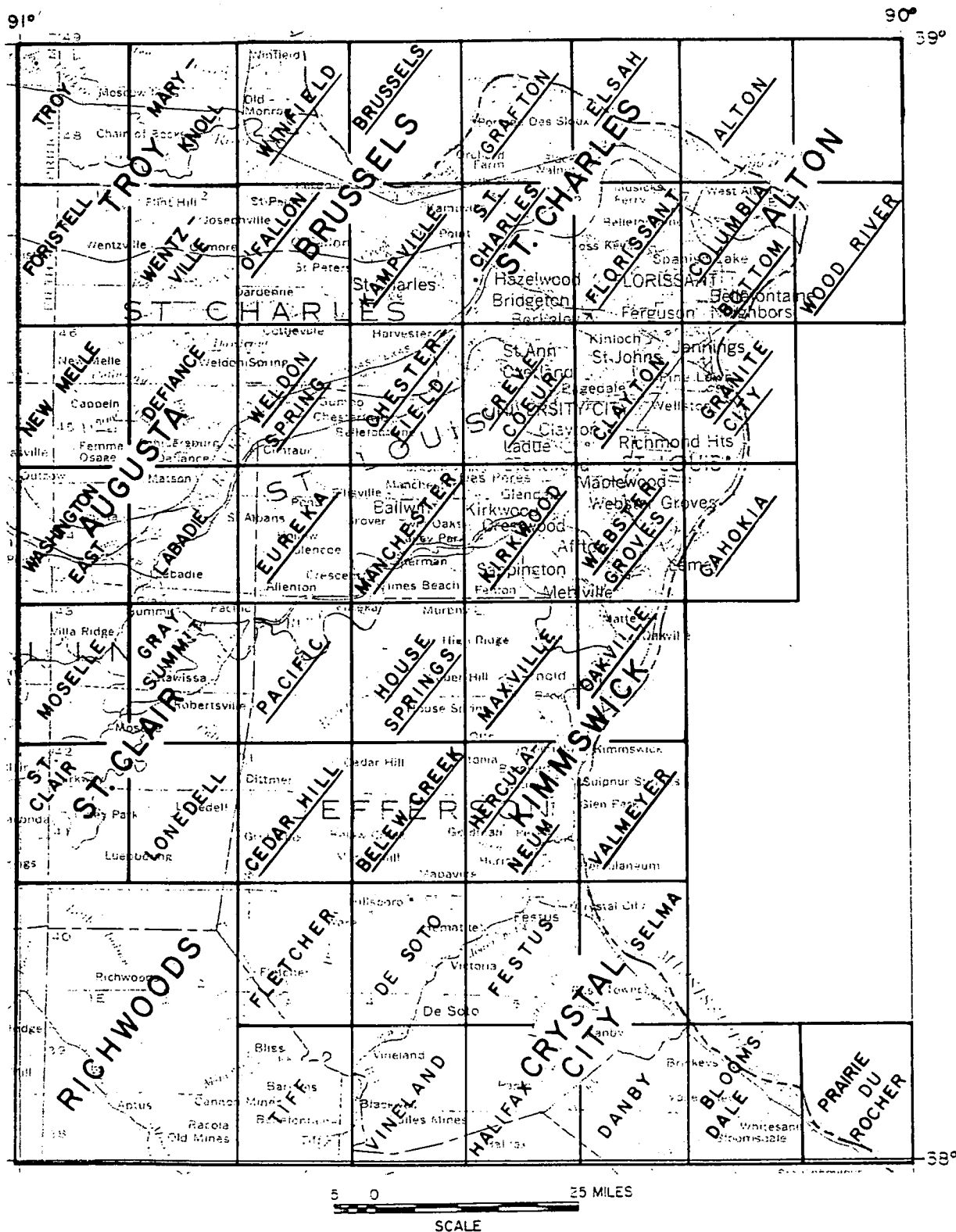


Figure 2

Streamflow data-collection sites in the St. Louis area, Missouri.

WATER RESOURCES OF THE ST. LOUIS AREA, MISSOURI



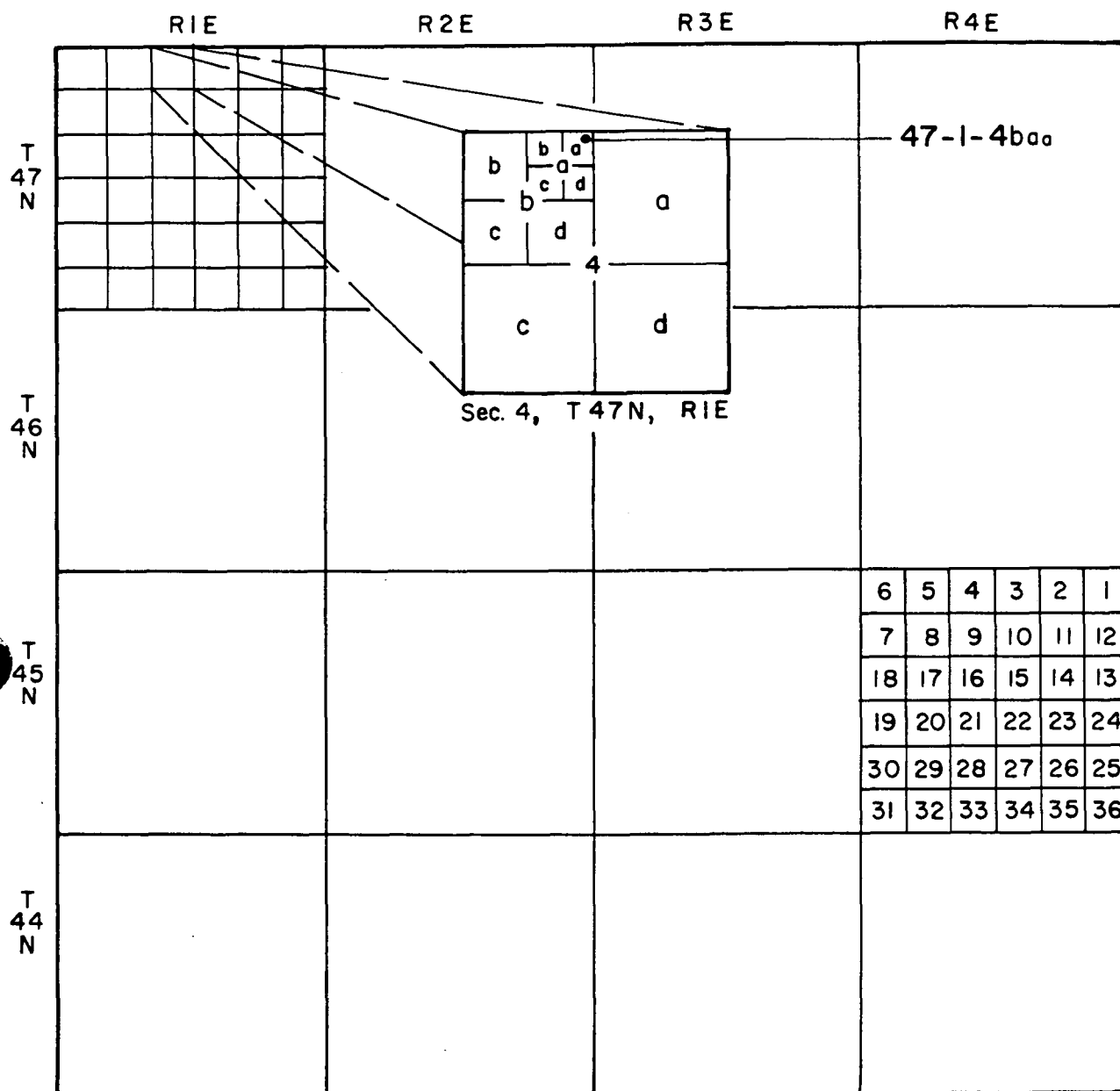


Figure 4

The well location system used in this report is a shortened version of that normally used to describe

a location. Subdivisions of the section are shown by letters.

WATER RESOURCES OF THE ST. LOUIS AREA, MISSOURI

Table 1

Generalized stratigraphic column for St. Louis, St. Charles, and Jefferson Counties, Missouri

Aquifers most favorable as water sources are shaded									
System	Series	Group	Formation	Aquifer group	Thickness (feet)	Dominant lithology	Water-bearing character		
Quaternary	Holocene		Alluvium ^{1/}		0-150	Sand, gravel, silt, and clay.	Some wells yield more than 2,000 gpm.		
	Pleistocene		Loess Glacial till		0-110 0-55	Silt Pebbly clay and silt.	Essentially not water yielding		
Pennsylvanian	Missourian	Pleasanton	Undifferentiated		0-75	Shales, siltstones, "dirty" sandstones, coal beds and thin limestone beds.	Generally yields very small quantities of water to wells. Yields range from 0-10 gpm.		
	Desmoinesian	Marmaton	Undifferentiated		0-90				
		Cherokee	Undifferentiated		0-700				
	Atokan		Undifferentiated						
Mississippian	Meramecian		Ste. Genevieve Formation	1	0-160	Argillaceous to arenaceous limestone.	Yields small to moderate quantities of water to wells. Yields range from 5 to 50 gpm. Higher yields are reported for this interval locally.		
			St. Louis Limestone		0-180				
			Salem Formation		0-180				
			Warsaw Formation		0-110				
	Osagean		Burlington-Keokuk Limestone		0-240	Cherty limestone			
			Fern Glen Formation		0-105	Red limestone and shale.			
Kinderhookian	Chouteau	Undifferentiated		0-122	Limestone, dolomitic limestone, shale, and siltstone.				
	Devonian	Sulphur Springs	Bushberg Sandstone		0-60	Limestone and sandstone.			
Glen Park Limestone				0-50	Fissile, carbonaceous shale.				
Grassy Creek Shale				0-200	Cherty limestone.				
Silurian			Undifferentiated						
Ordovician			Maquoketa Shale		0-163	Silty, calcareous or dolomitic shale.	Probably constitutes a confining influence on water movement.		
	Cincinnatian		Cape Limestone		0-5	Argillaceous limestone.	Yields small to moderate quantities of water to wells. Yields range from 3 to 50 gpm. Decorah Formation probably acts as a confining bed locally.		
			Kimmswick Formation		0-145	Massive limestone			
	Champlainian		Decorah Formation	2	0-50	Shale with interbedded limestone.			
			Plattin Formation		0-240	Finely crystalline limestone.			
			Rock Levee Formation		0-93	Dolomite and limestone, some shale.			
			Joachim Dolomite		0-135	Primarily argillaceous dolomite.			
			St. Peter Sandstone		0-160				
	Everton Formation	3		0-130	Silty sandstone, cherty limestone grading upward into quartzose sandstone.	Yields moderate quantities of water to wells. Yields range from 10-140 gpm.			
			Canadian		Powell Dolomite	4	0-150	Sandy and cherty dolomites and sandstone.	Yields small to large quantities of water to wells. Yields range from 10 to 300 gpm. Upper part of aquifer group yields only small amounts of water to wells.
					Cotter Dolomite		0-320		
		Jefferson City Dolomite		0-225					
		Roubidoux Formation		0-177					
		Gasconade Dolomite		0-280					
Cambrian	Upper	Elvins	Eminence Dolomite	5	0-172	Cherty dolomites, siltstones, sandstone, and shale.	Yields moderate to large quantities of water to wells. Yields range from 10 to 400 gpm.		
			Potosi Dolomite		0-325				
			Derby-Doerun Dolomite		0-165				
			Davis Formation		0-150				
			Bonneterre Formation		245-385				
			Lamotte Sandstone		2354				
Proterozoic						Igneous and metamorphic rocks.	Does not yield water to wells in this area.		

^{1/} Basal part may be of Pleistocene age.

NOTE: Stratigraphic nomenclature may not necessarily be that of the U.S. Geological Survey.

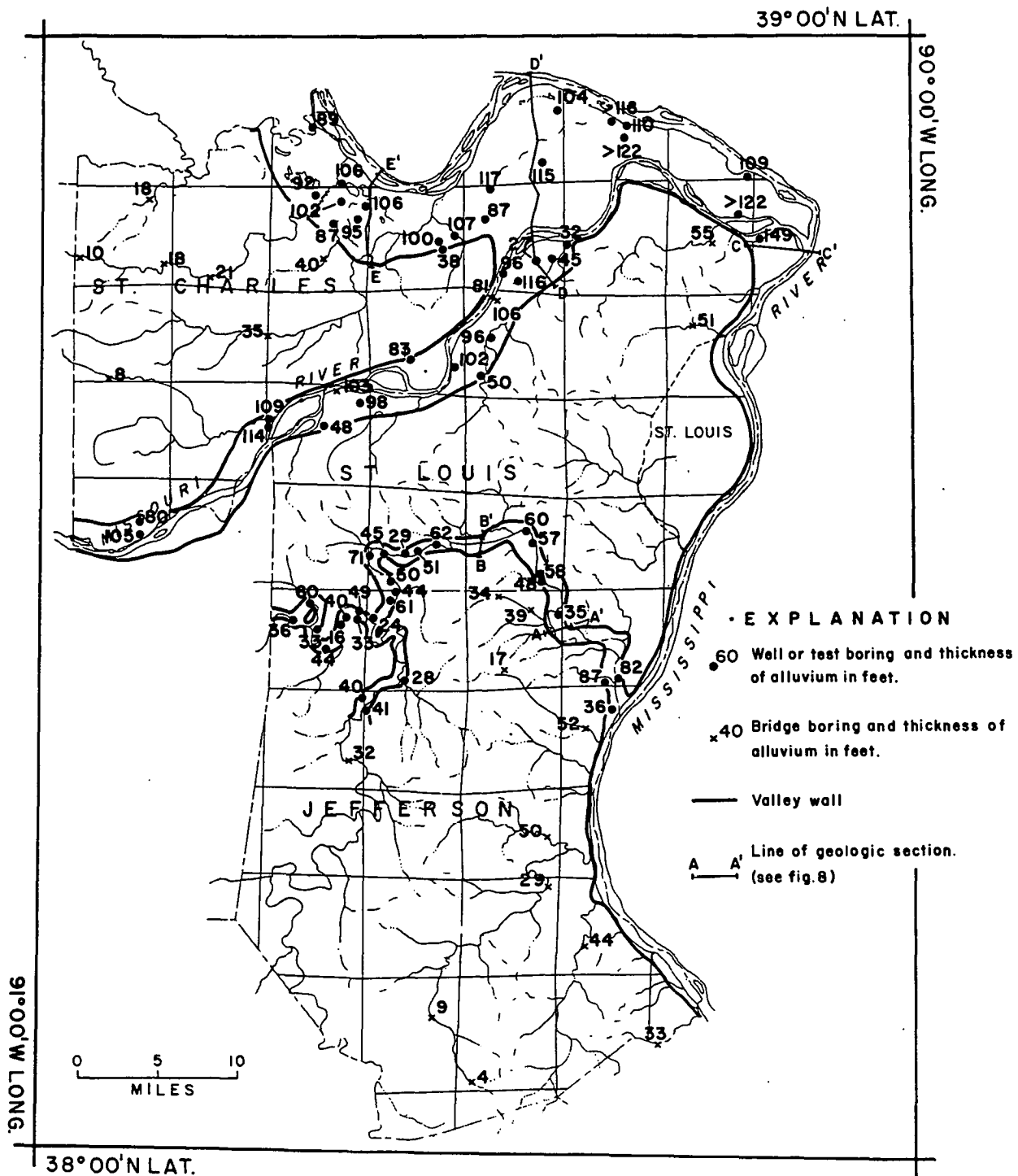


Figure 5

Thickness of alluvium along the Mississippi, Missouri, Meramec and lower Big Rivers, and some tributary streams.

STRATIGRAPHY

The stratigraphic sequence consists primarily of limestone and dolomite which were deposited, for the most part, in shallow epicontinental seas. Rocks range in age from Precambrian to Holocene. A composite stratigraphic section showing these rocks and their water-bearing properties is given in table 1. The Precambrian rocks, the Lamotte Sandstone, and the lower part of the Bonneterre Formation are the only units that do not crop out in the area; they are, however, present in the subsurface. Many periods of emergence, nondeposition or erosion are implied by the disconformities and local unconformities observed in surface exposures and well data. These breaks in the stratigraphic record are shown in table 1 by wavy lines.

Many of the stratigraphic units are not present locally; consequently, no wells penetrated all the formations shown in table 1. Formations penetrated while drilling a well depend on the geographic location. For example, wells drilled in southern Jefferson County start lower in the stratigraphic section and hence do not penetrate many of the formations shown in table 1.

STRUCTURE

The present structural attitude of the rock units is the result of compressional, tensional and uplifting forces which moved and altered the units from their original depositional positions. These forces have folded, fractured, faulted, and tilted the rocks in the study area, and the resulting structures are superimposed on a regional dip or

The only deposits of Cenozoic age having significant water-yielding properties are the water-saturated sands and gravels in the alluvium. It is possible that the basal portion of part of the fill in the large valleys is actually of Pleistocene age (Bergstrom and Walker, 1956, p. 31). However, since no attempt has been made to differentiate the valley fill as to age in this report, it is referred to as alluvium.

Alluvium underlying the floodplains and terraces of the Mississippi, Missouri and Meramec Rivers extends over 277 square miles in the three-county area. The thickness of the alluvium is variable because of irregularities in the bedrock surface upon which it was deposited. The maximum known thickness of alluvium (150 feet) was penetrated by a test hole drilled in the Columbia Bottoms near the mouth of the Missouri River. The areal extent and the thickness of the alluvium at selected points is shown in figure 5. The alluvium is composed of clay, silt, sand and gravel. In general, the alluvium becomes coarser-grained with depth. It is this deeply buried, coarser-grained material which, when well-sorted and water-saturated, comprises the most water-productive part of the alluvial aquifer.

large-scale tilting of the rock units of from 60 to 80 feet per mile to the northeast. Figure 6 shows some of the major structures in the St. Louis area.

The reader is referred to McCracken (1966) and Trapp (1961, unpublished data) for a more complete description of the structures in the St. Louis area.

SOURCES OF WATER

St. Louis, near the confluence of the Missouri and Mississippi Rivers, is well situated with respect to surface-water supplies. In addition, the area has the

benefit of the Meramec River, which carries a large flow of good-quality water to the Mississippi just south of St. Louis. These rivers furnish nearly all of

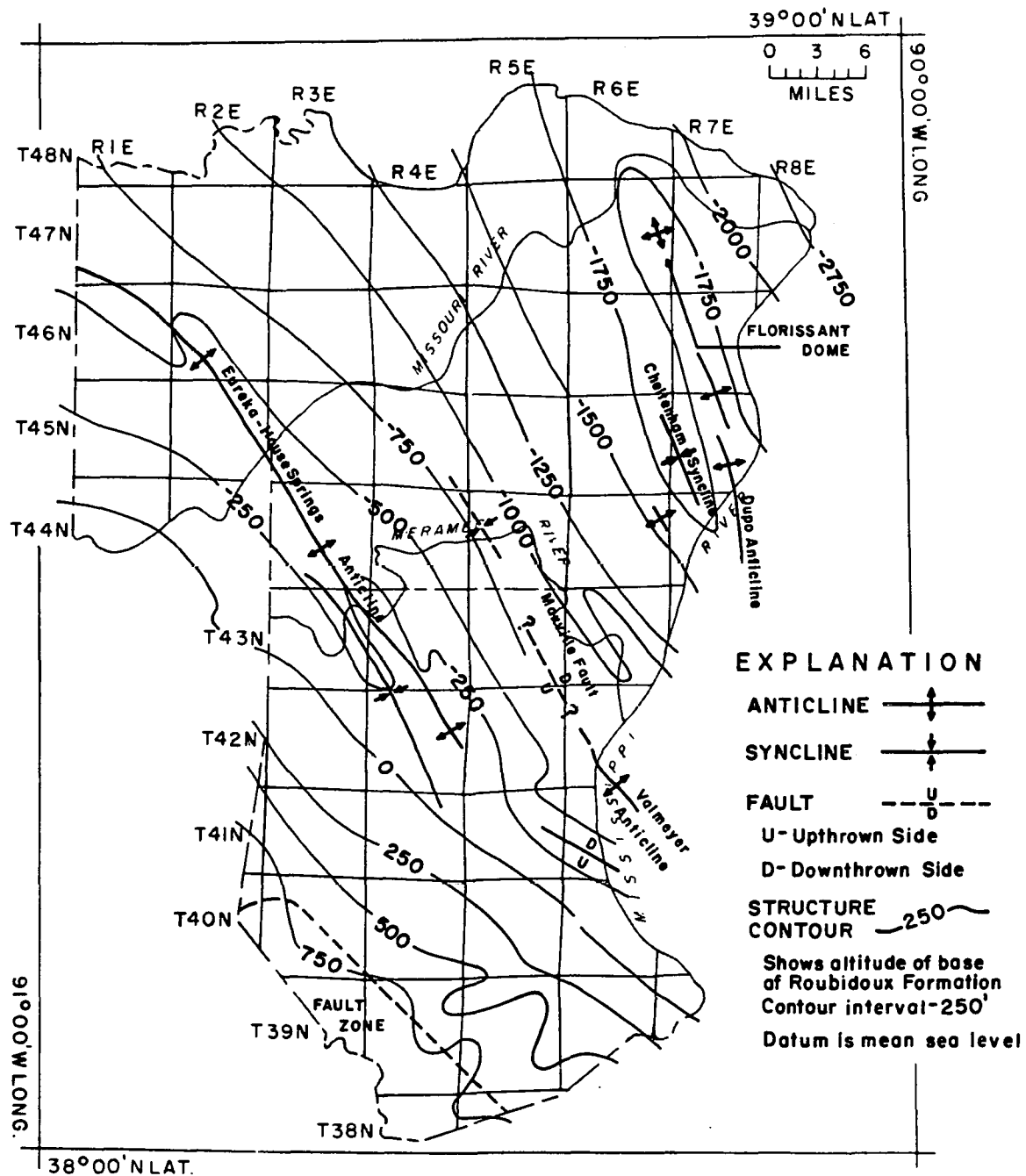


Figure 6

Major structural features of the St. Louis area
and structural contours on the base of the Roubidoux

Formation (based on McCracken and McCracken,
1965).

the water used in the three counties while their tributary streams are used for recreation or waste transportation. In addition to surface-water sources, a large amount of water is available to the area from

the underlying rocks. Though some ground water is too mineralized to use, much is fresh and of good quality. Little of the ground water in storage is used.

GROUND WATER

Large amounts of fresh water are stored in the bedrock and alluvium underlying the area. Water occurs in the bedrock along fractures and bedding planes as well as in solution openings in the limestone and dolomite, and in voids between the grains in sandstone. Shale is generally impervious to the movement of water and is usually not a source of supply. The availability of water from bedrock depends upon the amount of fracturing and solution which the rocks have undergone and the degree to which these openings are interconnected. Water in

the alluvium occurs in the openings between the individual sand and gravel particles of which the aquifer is composed. The availability of water from the alluvium depends upon the degree of sorting of the material, its saturated thickness, its hydraulic connection with a surface-water source, and infiltration of rainfall.

Locations of wells and test holes used for compiling hydrogeologic data for this report are shown on plate 1.

AQUIFERS

Most wells drilled into bedrock in the study area are left open below a certain casing depth. This casing depth is determined by the presence and degree of weathering, and by connections with surface-water sources. Individually, many of the rock units shown on table 1 yield only small amounts of water. Collectively, however, these units may yield sufficient water to supply the needs of most water users. For this reason, it was considered practical to treat large sequences of both water-bearing and non-water-bearing rocks as one large aquifer or aquifer group. The bedrock units are thus assigned to five groups based on similar lithologic characteristics, geographic distribution, and overall similarity of water quality. Also of prime importance are the presence of confining beds at aquifer group boundaries and the presence of thick sequences of rock which, although not to be considered confining, yield very little water to wells (see table 1).

Group 1 (Post-Maquoketa) includes all bedrock units above the Maquoketa Shale, which probably acts as a confining bed in the study area. Pennsylvanian rocks at the upper boundary of Group 1 are relatively impermeable and yield very little water to wells. Group 2 (Kimmswick-Joachim) includes all

aquifers between the base of the Maquoketa Formation and the base of the Joachim Formation. The Joachim is not considered to be a good aquifer in other parts of the state and, although it is not a confining bed, it probably does not yield water in quantities large enough for it to be considered an aquifer.

Group 3 (St. Peter-Everton) includes the St. Peter Sandstone and the Everton Formation. Group 4 (Powell-Gasconade) includes all units in the Canadian Series of Early Ordovician age. The lower part of the Everton Formation and the upper three units of the Canadian (Powell, Cotter, and Jefferson City Dolomites) are not prolific water-bearing units. Small supplies can be developed in these units, but they are subject to failure during extended periods of drought or sustained pumping.

Group 5 (Eminence-Lamotte) includes all units below the base of the Gasconade Dolomite. The Eminence Dolomite is similar to the upper three units of the Canadian Series in its water-bearing characteristics and hence constitutes a good boundary marker between more prolific aquifers. Figure 7 is a geologic map showing the distribution of the aquifer groups discussed above.

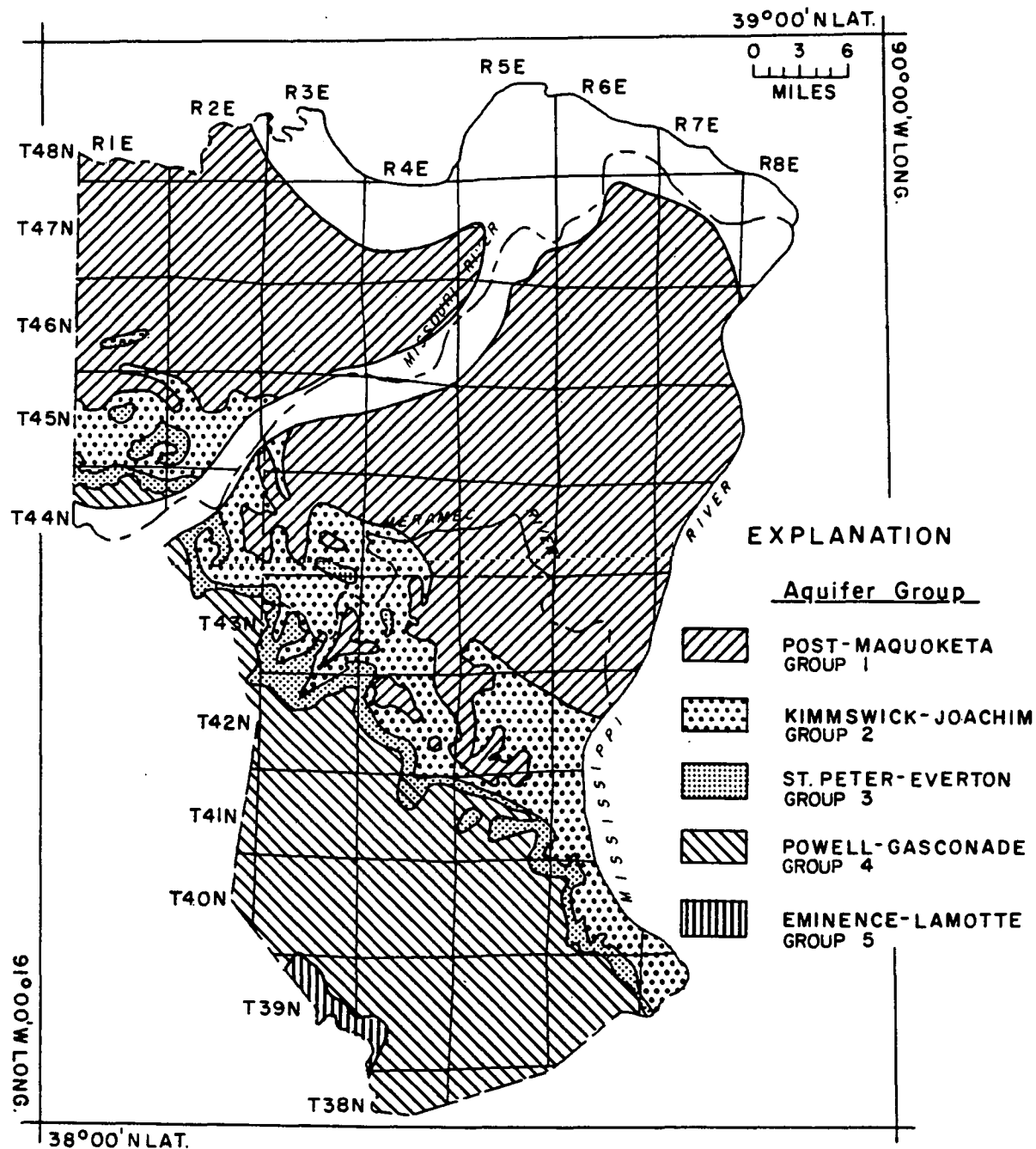


Figure 7

Geologic map showing distribution of aquifer groups. Numerals indicate aquifer groups.
(See table 1 for more detail.)

WATER RESOURCES OF THE ST. LOUIS AREA, MISSOURI

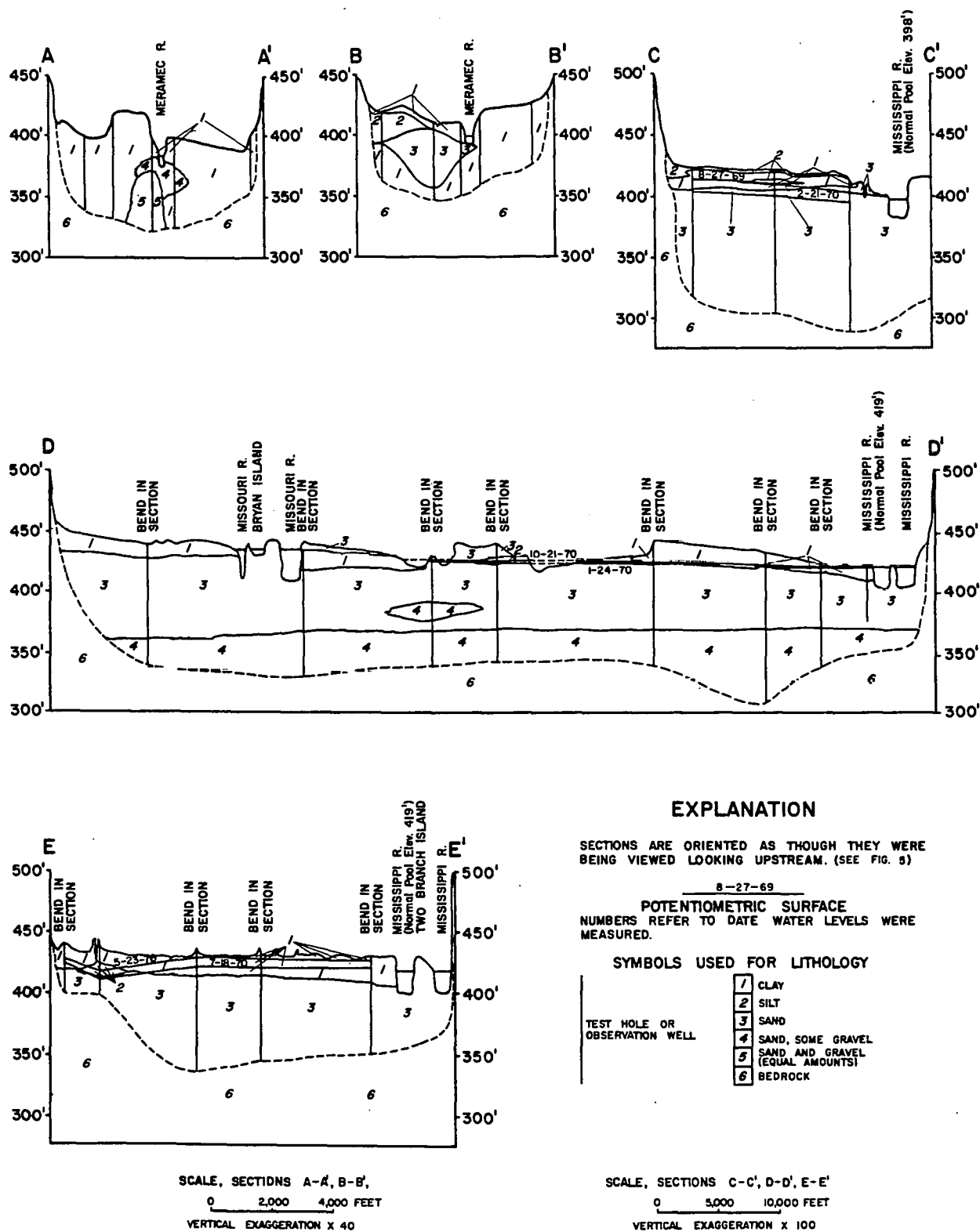


Figure 8
Hydrogeologic sections.

Major alluvial aquifers in the area are the water-saturated sands and gravels in the basal part of the alluvium underlying the floodplains of the Mississippi, Missouri and Meramec Rivers. Water-bearing sands and gravels also underlie the floodplains of the Big River and other perennial streams of the area. Records of well yields from these relatively thin alluvial deposits are not available, but it is believed that yields would generally be small to conventional vertical wells because of less saturated thickness.

The alluvial deposits are composed of varying proportions of clay, silt, sand, and gravel. The value of the alluvium as a source of water depends on its thickness and the size and sorting of the materials. The greater the proportion of clay, silt and fine sand, the poorer the aquifer would be. Conversely, well-sorted, clean sands and gravels would yield large quantities of water.

GROUNDWATER RECHARGE

The bedrock aquifers receive recharge from precipitation falling directly on the area. The amount of recharge from precipitation depends upon the general configuration and physical character of the land surface, the amount and type of vegetation, the distribution and quantity of precipitation, and the composition and moisture content of the soil and underlying rock. Movement of water from the soil and subsoil into the bedrock takes place along fractures and solution openings in the rock.

In areas where bedrock is exposed at the surface, conditions are not as favorable for recharge as in areas where the bedrock is not exposed. Recharge to the groundwater reservoir in the bedrock outcrop area is minimal and almost all of the precipitation leaves the area directly as runoff. Shallow bedrock aquifers that are hydraulically connected with the rivers also receive recharge from natural infiltration of the rivers during sustained high-river stage and flooding.

Alluvial aquifers in the area are recharged by infiltration of stream water during sustained high-river stage and flooding, by direct precipitation, and by underflow from underlying and adjacent bedrock.

Recharge from precipitation to the hydrogeologically-similar East St. Louis alluvial area, adjacent to the study area, has been estimated to be 65

Because of the scour-and-fill method of deposition, alluvial deposits may vary considerably in sorting and texture within a small area. This is readily apparent in a comparison of geologic sections (fig. 8) of the Mississippi and Missouri Rivers with sections of the Meramec River. This variability points up the need for adequate test drilling prior to any large-scale development of ground water from the alluvium.

Geologic logs of some of the more favorable sites for potential groundwater development in the alluvial areas are included in Appendix 1, and their locations are shown on plate 1. Geologic logs of many of the wells shown on plate 1 are available in the files of the Missouri Geological Survey and Water Resources.

mgd (million gallons per day) for 175 square miles (Schicht, 1965, p. 46). Schicht also estimated the average rate of subsurface flow of water from the valley wall to be 329,000 gpd/mi (gallons per day per mile). If the Mississippi, Missouri and Meramec River alluvium in the study area were to receive recharge from precipitation at a rate comparable to that estimated for the East St. Louis area, it would amount to approximately 100 mgd. However, because pumpage from the alluvium is not sufficient to lower water levels and make more storage area available, not all of the potential recharge enters the aquifer.

The sum of these sources, recharge from precipitation and underflow from the underlying and adjacent bedrock, theoretically is the amount of water that can be pumped from the alluvial aquifers without causing an overdraft or recharge from the rivers. This information is presented only to show the magnitude of the potential yield from alluvial aquifers by natural recharge alone.

An alluvial aquifer may also receive recharge from the river when large-capacity wells lower the water level in the aquifer so that the natural groundwater flow toward the stream is reversed. This causes water to move from the stream through the aquifer to the wells. Such induced recharge occurs in the Meramec River alluvium at Times Beach and in the Valley Park-Kirkwood area. Induced recharge undoubtedly occurred in the Missouri River alluvium

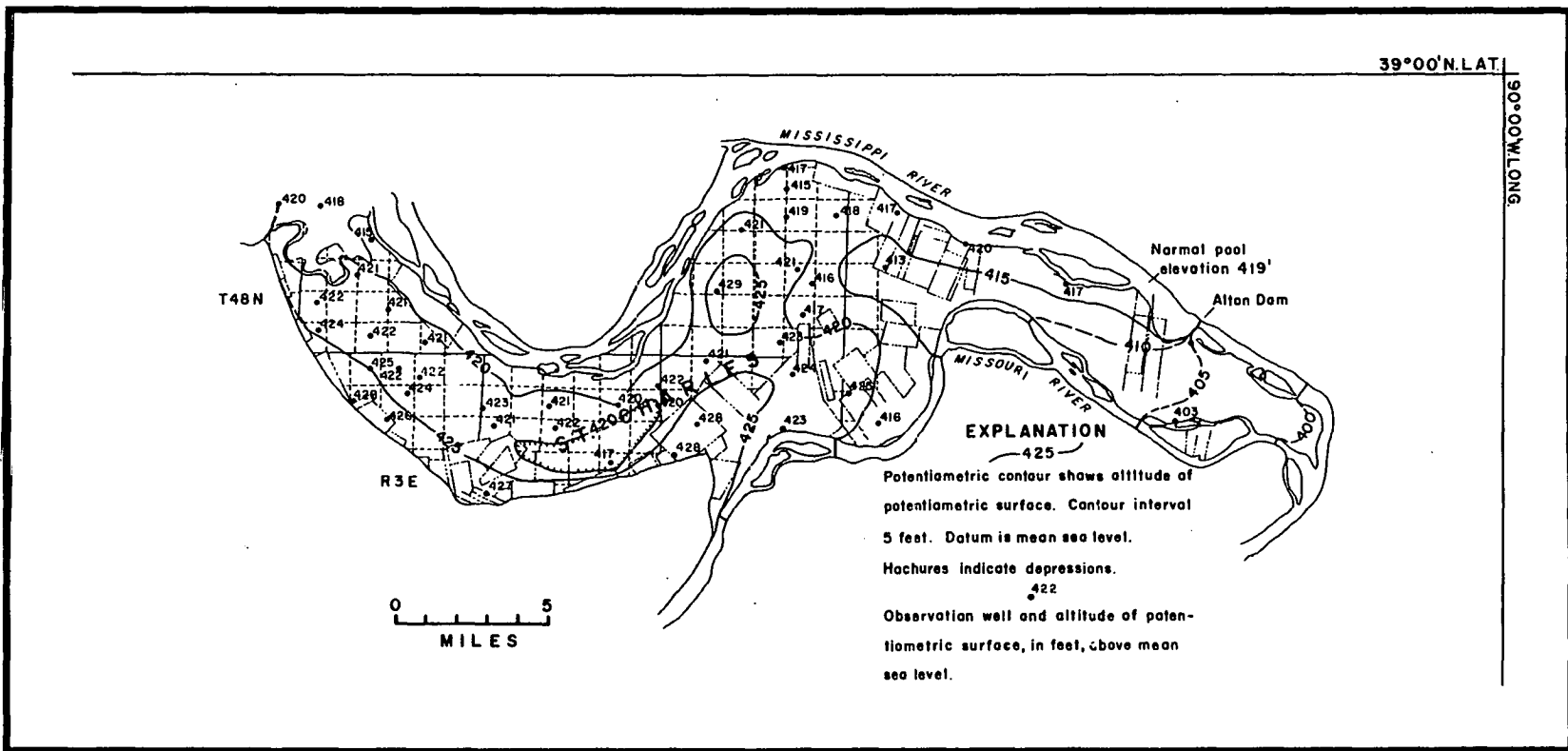


Figure 9

Potentiometric surface of the alluvial aquifer, Alton Lake Bottoms, St. Charles County, Mo., September 1970.

when the well field of the Weldon Springs Ordnance Plant was in operation (Emmett and Jeffery, 1968). Areas of induced recharge occur in the Mississippi River alluvium in Illinois (Schicht, 1965, p. 47) and in at least one location (Crystal City) in Missouri. Undoubtedly there are many other areas in the Mississippi River alluvium in Missouri where induced recharge could take place. If extensive development of the alluvial aquifers were to take place in the

study area, sustained pumping would depend upon induced recharge from the rivers.

Data were not available to determine induced infiltration rates of streams in the study area. However, Schicht (1965, p. 1), from analysis of aquifer tests in the East St. Louis, Ill. area, found that the infiltration rate of the Mississippi River bed ranged from 37,500 to 344,000 gpd/acre/ft (gallons per day per acre per foot).

GROUNDWATER MOVEMENT

The direction of groundwater movement can be determined for any specific time from the configuration of the groundwater surface on a potentiometric map. Such a map is shown in figure 9. Ground water moves in a direction that is down gradient and at right angles to contours on the potentiometric surface.

Wells drilled into the bedrock aquifers in the study area encounter confined, or artesian, ground water. The hydrostatic pressure, or "head", in these aquifers raises the water level in the well above the point where it was first encountered in drilling. Any movement of ground water is from areas of higher hydrostatic pressure to areas of lower hydrostatic pressure.

Potentiometric maps of bedrock aquifers could only be constructed in geographically restricted areas because of the manner in which bedrock wells in the study area are constructed. In most instances wells penetrate more than one aquifer group and each aquifer group has a separate and distinct potentiometric surface.

It is probable, however, that some hydraulic connection exists between aquifer groups in the study area. Movement of ground water between aquifers due to head differences in the units occurs in areas where sufficient permeability exists at contacts between units.

Movement of ground water in the alluvial aquifers is generally toward the major streams with which they are hydraulically connected (fig. 9), except where the movement is reversed during floods or sustained high-river stages, or by high-capacity wells pumping close enough to the river to induce recharge. An example of wells causing induced recharge is found in the Valley Park-Kirkwood area (fig. 10).

The groundwater surface in the alluvial aquifer fluctuates in response to changes in the river stage and to variations in precipitation and pumpage from wells. Figure 8 shows maximum and minimum water levels measured in selected parts of the alluvial aquifers during this investigation.

GROUNDWATER DISCHARGE

Water recharged to the groundwater body moves down gradient in the direction of the slope of the potentiometric surface until it moves out of the study area or is discharged by natural or artificial means. Discharge is accomplished by evaporation, plant transpiration, discharge by springs, seepage into streams, or by pumpage from wells. Over long periods of time, discharge is balanced by recharge, and water levels are not drastically affected.

An undetermined amount of discharge from deeper aquifers into shallower aquifers is taking place in the study area. In areas such as Valley Park, where deep wells have been improperly cased or where casings have deteriorated, mineralized water from deeper aquifers has moved up into shallower horizons and, where head differences permit, some water is undoubtedly moving from shallow aquifers into deeper ones through wells.

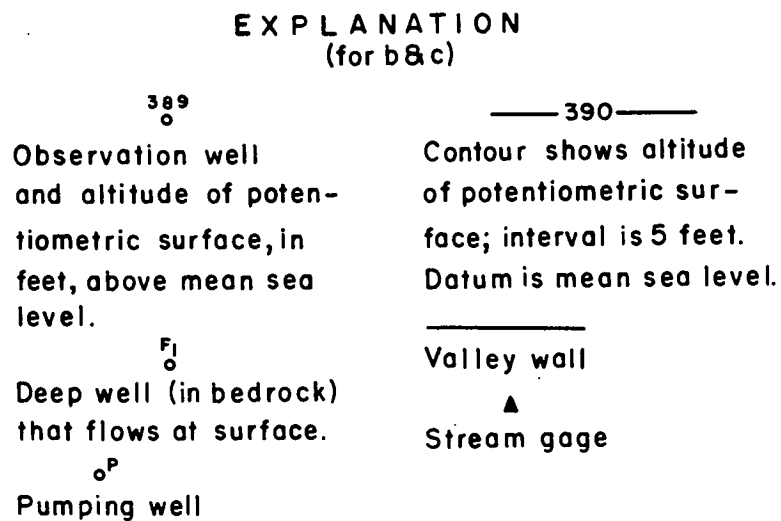
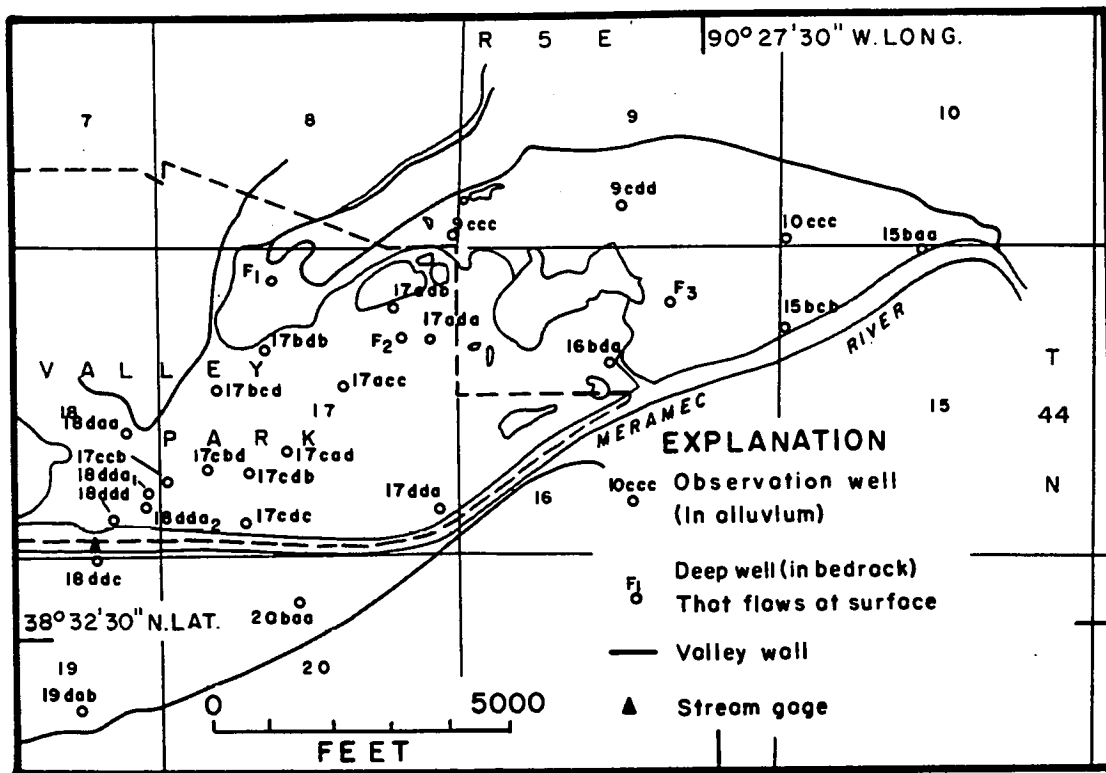
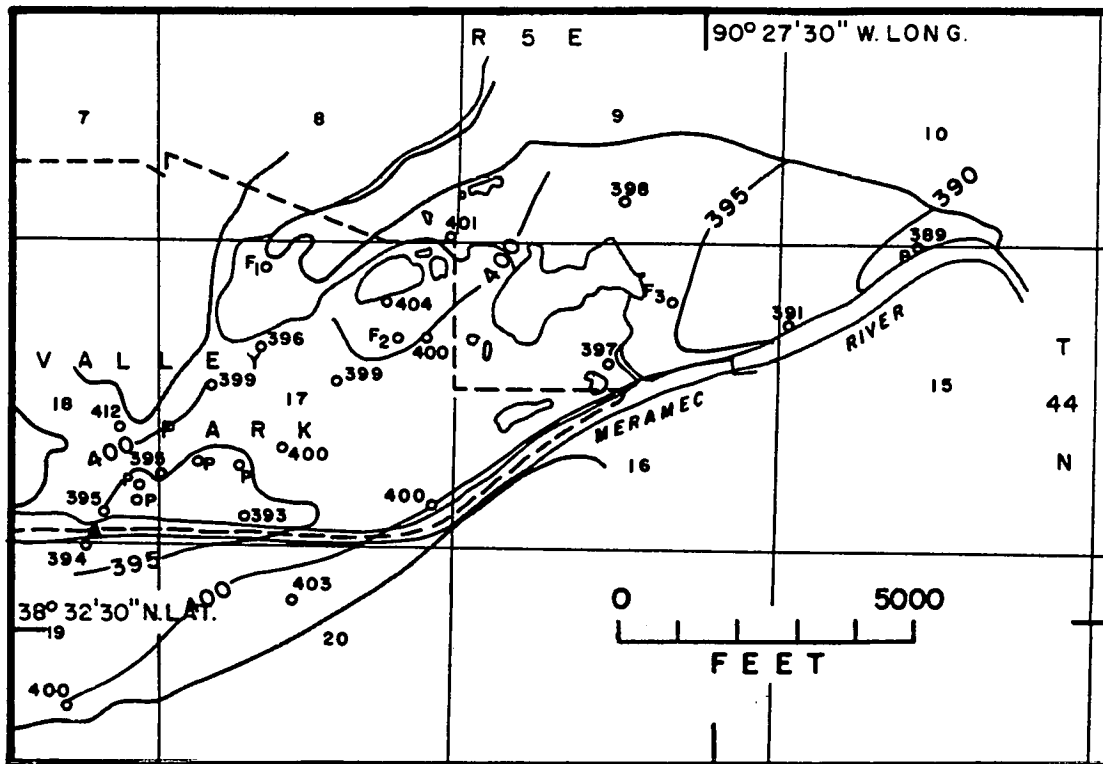


Figure 10a

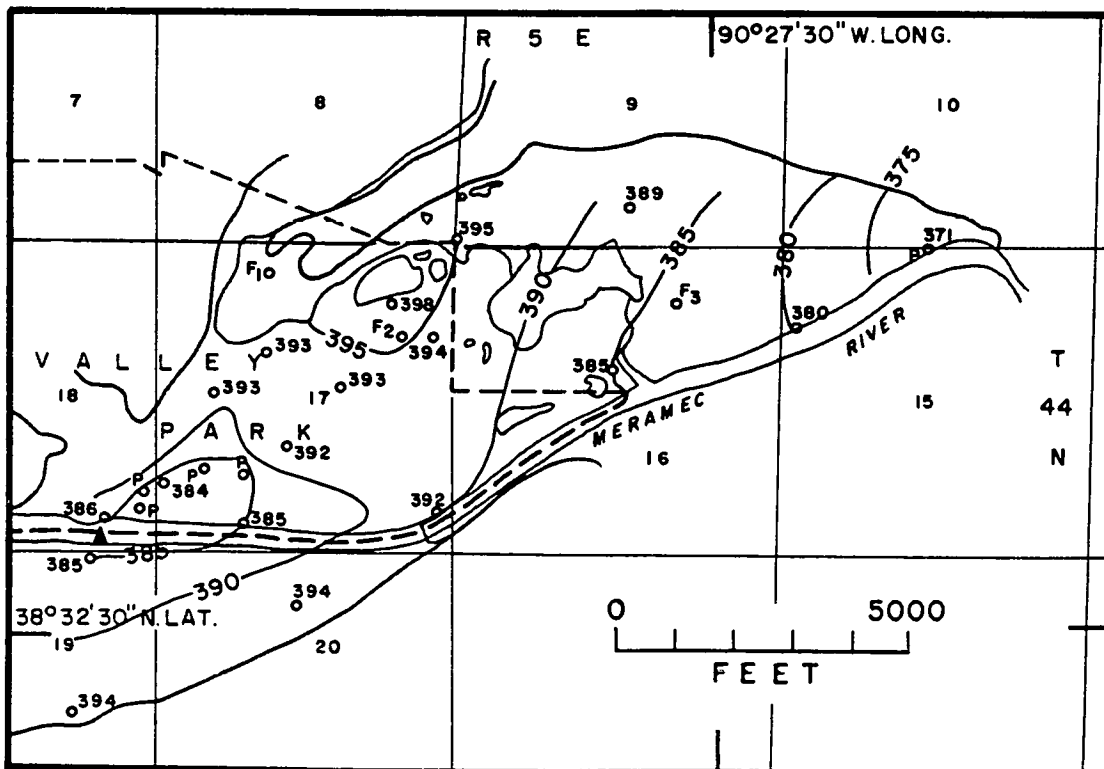
Location of wells in the Valley Park-Kirkwood area.



Potentiometric surface of the Valley Park-Kirkwood area alluvial aquifer:

Figure 10b (top) May 1970. Elevation of the river at Valley Park is 402.5 feet.

Figure 10c (bottom) July 1970. Elevation of the river at Valley Park is 391 feet.



WATER RESOURCES OF THE ST. LOUIS AREA, MISSOURI

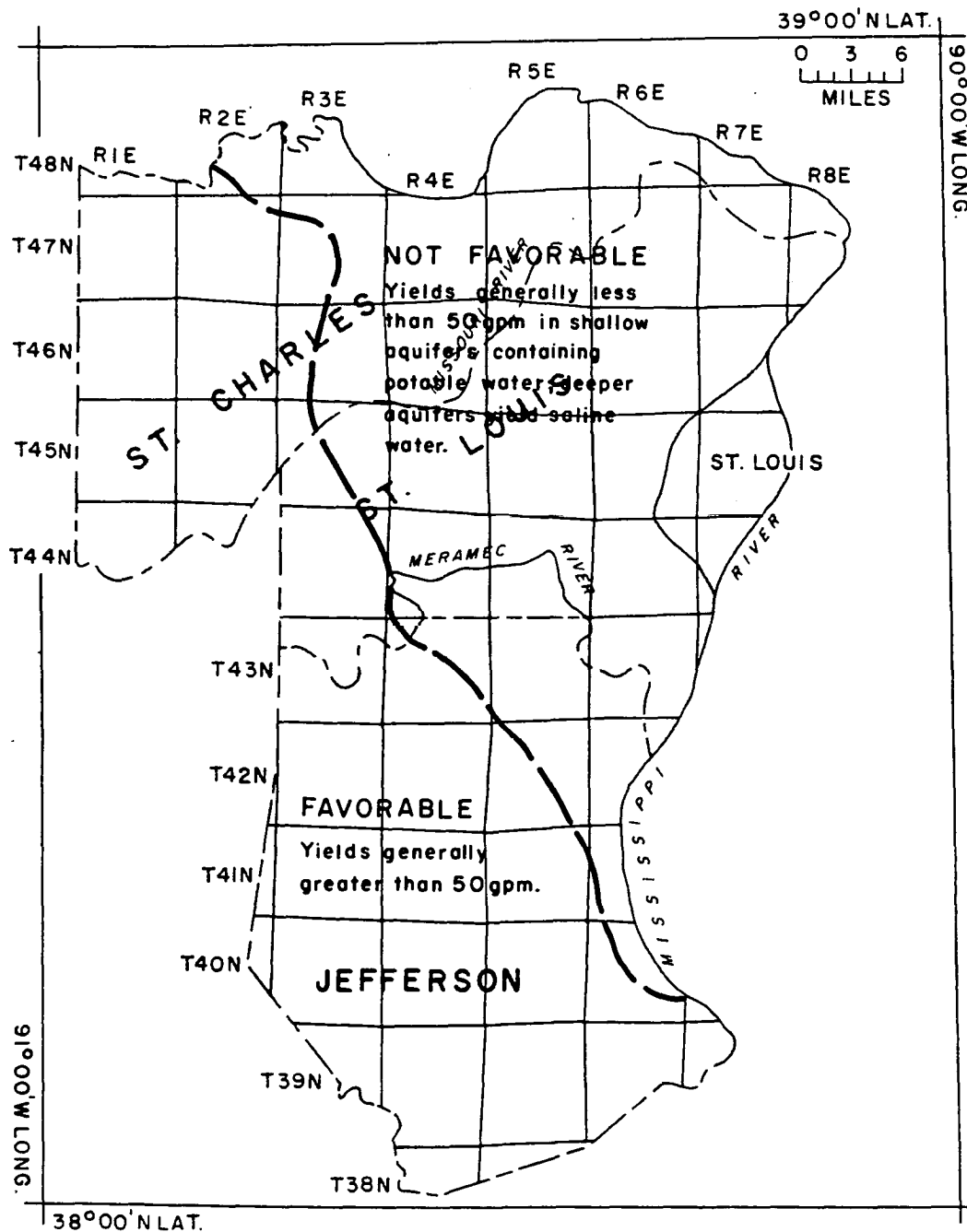


Figure 11

Most favorable area for development of high-yield wells in bedrock aquifers (differentiated by water quality and not by absence of high-yield aquifers).

WELL YIELDS AND AQUIFER CHARACTERISTICS

All bedrock units are locally capable of yielding water in varying amounts to wells. Yields of wells are dependent, of course, on such factors as depth, length and diameter of the open hole; formations penetrated; geographic location (p. 10); structural attitude of the rock; and permeability of the aquifers tapped. Because of the stratigraphic complexity of this area and probable interformational movement of the water, it is difficult to define parameters which describe yield capabilities of individual aquifers. It is possible, however, to use data from wells penetrating various aquifer combinations to arrive at conclusions about the more important water-bearing units in the study area.

A reliable measure of the productivity of a well is its specific capacity. This is the discharge of the well expressed as a rate of yield per unit of drawdown, generally in gallons per minute per foot of drawdown.

Specific capacities and yields of wells penetrating aquifers or groups of aquifers are shown in table 2. Higher specific capacities for wells in bedrock are apparent in the western part of the study area and in the south-central part of Jefferson County because higher-yielding units are penetrated by the wells. On the average, wells penetrating Groups 3 and 4 aquifers (St. Peter Sandstone through the Gunter Member of the lower part of the Gasconade Dolomite) had yields significantly higher (100+gpm) than wells finished in aquifer Groups 1 (Post-Maquoketa) or 2 (Kimmswick-Joachim) which were from 3 to 50 gpm. Many wells started in aquifers in Groups 1 or 2 and finished in aquifers in Groups 3 or 4 had better yields than those actually finished in aquifers in Groups 1 or 2. The yields of wells opened only to aquifers in Group 5 (Eminence-Lamotte) were inconsistent, ranging from less than 10 gpm to as much as 400 gpm.

Wells penetrating the St. Peter Sandstone of Group 3 aquifers, the Roubidoux and Gasconade Formations of Group 4 aquifers and the Potosi Dolomite of Group 5 aquifers consistently had higher yields than wells which did not penetrate these units. Figure 11 shows areas where water in these aquifers (or aquifer groups) was acceptable in quality and should be considered for future

development when high-yield groundwater supplies are needed.

Yields of 500 gpm have been reported from wells in the Meramec River alluvium. In the Missouri River alluvium, a well in the old Weldon Springs Ordnance Plant well field was pumped at approximately 2,600 gpm for 47 hours during an aquifer test (Emmett and Jeffery, 1968). According to Searcy, Baker and Durum (1952, p. 48), this well field consisted of 13 large-capacity wells on a 344-acre tract which supplied water from the Missouri River alluvium at a rate of more than 44 mgd. Discharge exceeding 3,300 gpm has been reported from irrigation wells in the Mississippi River alluvium.

Specific capacities reported for wells in the Mississippi, Missouri and Meramec River alluvium are given in table 2. Durations of the tests are not known in all instances. However, these values can serve as an indication of the productivity of wells in the alluvial aquifers.

Generally, high specific capacities indicate an aquifer with high transmissivity while low specific capacities indicate an aquifer with a low transmissivity.

Two characteristics governing the value of an aquifer as a source of water are its ability to store and to transmit water. These two values can be measured by aquifer tests.

For artesian (confined) aquifers, the storage coefficient may range from 0.00001 to 0.001. The storage coefficients of water-table aquifers range from about 0.05 to 0.30.

The coefficients of storage and transmissivity were determined at two sites. These values are presented in table 2. The transmissivities at the two sites are virtually the same but the coefficients of storage indicate water-table conditions at the Weldon Spring site and artesian conditions at the St. Charles site. Available well logs and water-level measurements indicate that artesian or leaky artesian conditions prevail throughout most of the Mississippi River alluvium.

Results obtained from these two tests are indicators of the hydrologic characteristics of the alluvial aquifers. Any large-scale development of groundwater resources should be based on additional tests.

WATER RESOURCES OF THE ST. LOUIS AREA, MISSOURI

Table 2
Summary of well data for the St. Louis area

City or subdivision	Owner	Well location	Depth (feet)	Well diameter (inches)	Date of test	Pumping rate (gpm)	Duration of test (hours)	Specific capacity (gpm/ft drawdown)	Draw-down (feet)	Remarks
City of De Soto		39-4-3add	800	10	Aug. 1954	465	4	9.3	50	Potosi Dolomite (Group 5)
-	Burt Manor Nursing Home	39-5-20dda	510	6	-	26	6	0.73	36	Lower part of Gasconade Dolomite Eminence Dolomite (Groups 4 & 5)
-	Robert Schroeder	39-5-31dba	285	6	Jan. 1960	18	1	0.09	200	Jefferson City-Roubidoux (Group 4)
-	Blanche Combs Trailer Court	40-3-32	1050	6	1967	60	6	1.33	45	Bonnetterre-Lamotte (Group 5)
-	Jefferson County Memorial Hospital	40-6-17bdc	750	8	1955	88	24	0.44	176	Cotter-Lower part of Gasconade (Group 4)
-	Mississippi River Fuel Corp. River Cement	40-6-22adc	1000	8	-	82	8	0.44	187	St. Peter-Upper part of Gasconade (Groups 3 & 4)
-	Dow Chemical Co.	41-6-18dac	390	-	1956	140	12	0.98	143	St. Peter-Everton (Group 3)
City of Cedar Hill		42-3-25abb	902	8	May 1933	50	-	0.26	212	Cotter-Eminence (Groups 4 & 5)
-	Jefferson County Water District No. 9	42-5-31bcc	1200	8	1967	130	24	1.63	80	Powell-Roubidoux (Group 4)
-	Beaumont Boy Scout Reservation	43-4-2bca	540	8	1950	50	24	0.44	113	Plattin-St. Peter (Groups 2 & 3)
Brier-Cliff Estates	Leonard Small Realty Co.	43-4-17hdc	675	6	Sept. 1959	23	24	0.21	107	Kimmswick-Everton (Groups 2 & 3)
-	Babier State Park	45-3-28bbd	1072	10	Aug. 1940	182	24	1.61	113	Joachim-St. Peter (Groups 2 & 3)
-	C. Kaiman	46-7-20	655	8	Feb. 1936	120	4	0.89	135	St. Genevieve-Burlington (Group 1)
-	Atlas Powder Co.	46-3-28ddd	811	8	Feb. 1941	13	3	0.07	200	Kimmswick-St. Peter (Groups 2 & 3)
Lake St. Louis	-	47-2-27	1375	8	Mar. 1970	140	4	0.76	193	Plattin-Roubidoux (Groups 2, 3, & 4)
City of O'Fallon	Well No. 3	47-3-20eda	1500	8	Oct. 1960	132	2	2.64	50	Kimmswick-Upper part of Gasconade (Groups 2, 3, & 4)
-	Monsanto Chemical Co.	47-3-23ccc	1397	10	April 1967	183	24	0.53	348	Kimmswick-Roubidoux (Groups 2, 3, & 4)
City of O'Fallon	Well No. 1	47-3-29aaa	933	8	Sept. 1940	55	24	0.25	221	Kimmswick-St. Peter (Groups 2 & 3)
Portage des Sioux	Portage des Sioux	48-6-15cbf	116	8	Mississippi River alluvium	500	4½	48	10.5	10 screen
-	Blue Wing	47-4-7cbd	100	16		2000				
-	Whistling Wing	47-4-11dba	80			1230		85	14.6	
-	Lindberg & Kenney	48-3-35cbd	106	16		2249		80	28	
-	Oro Farm	47-3-4adc	92			1690		105	16	
-	Hermitage Club	47-3-12ada	106	16		1750		175	10	
-	Webfoot Club	47-3-12cdd	95	14		1900		83	23	32-ft screen
St. Charles	St. Charles	47-4-24	107							T=36,180 cubic feet per day per foot S=0.004
-	Portage Farm	48-5-23ded	107	26	Sept. 1963	1160		102	11.4	
-	Mr. Ambo	46-4-25bbd	102	16	Missouri River alluvium 1963	840	2	168	5	32-ft screen. Well not pumped at steady rate.
-	Mr. Smittle	46-5-17	96	12		600				32-ft screen
-	Mr. Twillman	46-4-28	83	12		900		69	13	
-	Weldon Springs Ordnance Plant	45-3-18bcc	107	15	1967	2650	47			Aquifer test. T=36,180 cubic feet per day per foot S=0.2
Valley Park	Valley Park	44-5-18dda ₁	63	18	Maramec River alluvium Aug. 1949	504	24	72	7	15 ft of 18-inch screen
Valley Park	Valley Park	44-5-18dda ₂	63	18	July 1949	504	24	36	14	15 ft of 18-inch screen. Yield has increased to 47 gpm/ft after treatment for capacity loss.
Valley Park	Absorbent cotton	44-5-17cdb	63	16	May 1957	500	12	83	6	15 ft of 16-inch screen gravel pack.
Valley Park	Ashland Chemical	44-5-17cbd	59	16	Oct. 1959 June 1964	503 554	-	102 111	5 5	15 ft of 16-inch screen gravel pack.
Kirkwood	Kirkwood No. 1	44-5-15	37	18	Dec. 1926	300	10	60	5	18 ft of 18-inch screen
	Kirkwood No. 2	44-5-15	42	18	Nov. 1927	250	10	83	3	20 ft of 18-inch concrete screen.

CHEMICAL QUALITY OF GROUND WATER

Most bedrock wells are constructed with several aquifers open to the well and, for this reason, it is not feasible to sample water from individual aquifers to determine their representative water-quality characteristics. Therefore, the discussion of chemical quality of water from bedrock will be by the five aquifer groups shown on figure 7. Quality of water from alluvial deposits will be discussed as Meramec River alluvium and as Mississippi-Missouri River alluvium. Only analyses of water from wells depicted on logs in the Missouri Geological Survey files were used in this study.

The chemical quality of ground water in the study area is quite variable, ranging in dissolved-solids content from 122 to 17,500 mg/l (milligrams per liter), with the water varying from a calcium-magnesium bicarbonate to a sodium chloride, sodium sulfate, or a sodium bicarbonate type. At lower concentrations of dissolved solids, the calcium-magnesium-bicarbonate type of water generally is predominant and, as the dissolved-solids content of the water increases, the type of water is variable depending upon the source. At higher concentrations of dissolved solids the water is a sodium-chloride type.

The source and significance of dissolved mineral constituents and properties of water are summarized in table 3. The values that were equal to or less than found in 75 and 50 percent of the samples from each aquifer group and from the alluvial deposits of the major streams are given in tables 4 and 5. Differences in the concentrations of various constituents are apparent, indicating certain factors which control water quality in the study area.

The principal factors affecting groundwater quality in the area are the complex interrelations imposed by the lithology of the rock units; permeability of the rock units; the controls on water movement exerted by the geologic structure; the length of time water has been in the aquifer and the distance it has moved from the recharge area; the degree of flushing of entrapped saline water (connate water) from the rock units; and, in local areas, the works of man.

The structural attitude of rock units in the St. Louis area exerts a pronounced effect on ground water recharge, discharge, and quality. Anticlinal features such as the Eureka-House Springs anticline

shown on figure 6 tend to be areas of recharge due to secondary permeability developed at their crests by fracturing and jointing. The synclines probably act as traps for mineralized water, and flushing progresses more slowly than elsewhere. Waters in these synclinal areas tend to be of poorer quality than waters from areas where more complete flushing has taken place. Structure contour maps and cross-sections of the area seem to substantiate the presence of synclinal traps in the Valley Park area and in T. 42 and 43 N., R. 6 E., in southeastern St. Louis County and northeastern Jefferson County. Also, movement of highly mineralized water from deeper horizons up into shallower zones through old abandoned wells is probably occurring in the Valley Park area.

Faults (fractures along which there has been movement of the two sides relative to one another) can act either as barriers to groundwater flow, when aquifers are faulted against impervious beds or the rocks have been recemented, or as open conduits for water if the rock is broken and fractured adjacent to the fault. When the fault zone is impervious, complete flushing of connate water in the aquifer might not be accomplished. If the fault zone is open, complete flushing of connate water takes place, and the more rapid circulation of water removes much of the soluble material. Fault zones which are accompanied by intense rock deformation, such as the area in southwestern Jefferson County in T. 39 N., R. 3 E., and 4, are locally important recharge areas. The Maxville fault in T. 43 N., R. 5 E., (fig. 6) acts as a barrier to the movement of water and retards flushing in the aquifer.

In addition to the physical constraints that affect groundwater quality, man unfortunately creates many of his own problems. Effluents from improperly constructed septic tanks or from areas where the concentration of septic tanks is too great for the absorptive capabilities of the soil cover, and leakage from improperly constructed or improperly located sewage lagoons moves into the groundwater reservoir and contaminates the ground water. Drainage from improperly operated or improperly located sanitary landfills may also add large quantities of contaminants to the groundwater reservoir.

The generalized groundwater-quality areas shown in plate 2, are based on a dissolved-solids content of less than 500 mg/l in or above the

Table 3

SOURCE AND SIGNIFICANCE OF DISSOLVED MINERAL CONSTITUENTS AND PROPERTIES OF WATER

Constituent or property	Source or cause	Significance
Silica (SiO_2)	Dissolved from practically all rocks and soils, commonly less than 30 mg/l. High concentrations, as much as 100 mg/l, generally occur in highly alkaline waters.	Forms hard scale in pipes and boilers. Carried over in steam of high-pressure boilers to form deposits on blades of turbines. Inhibits deterioration of zeolite-type water softeners.
Iron (Fe)	Dissolved from practically all rocks and soils. May also be derived from iron pipes, pumps, and other equipment. More than 1 or 2 mg/l of soluble iron in surface waters generally indicates acid wastes from mine drainage or other sources.	More than about 0.3 mg/l stains laundry and utensils reddish brown. Objectionable for food processing, textile processing, beverages, ice manufacture, brewing, and other processes. USPHS (1962) drinking-water standards state that iron should not exceed 0.3 mg/l. Larger quantities cause unpleasant taste and favor growth of iron bacteria.
Manganese (Mn)	Dissolved from some rocks and soils. Not so common as iron. Large quantities often associated with high iron content and acid waters.	Same objectionable features as iron. Causes dark brown or black stain. USPHS (1962) drinking-water standards state that manganese should not exceed 0.05 mg/l.
Calcium (Ca) and magnesium (Mg)	Dissolved from practically all rocks and soils, but especially from limestone, dolomite, and gypsum. Calcium and magnesium are found in large quantities in some brines. Magnesium is present in large quantities in sea water.	Cause most of the hardness and scale-forming properties of water; soap consuming (see Hardness). Waters low in calcium and magnesium desired in electroplating, tanning, and dyeing and in textile manufacturing.
Sodium (Na) and potassium (K).	Dissolved from practically all rocks and soils. Found also in ancient brines, sea water, industrial brines, and sewage.	Large amounts, in combination with chloride, give a salty taste. Moderate quantities have little effect on the usefulness of water for most purposes. Sodium salts may cause foaming in steam boilers, and a high sodium content may limit the use of water for irrigation.
Bicarbonate (HCO_3) and carbonate (CO_3)	Action of carbon dioxide in water on carbonate rocks such as limestone and dolomite.	Bicarbonate and carbonate produce alkalinity. Bicarbonates of calcium and magnesium decompose in steam boilers and hot-water facilities to form scale and release corrosive carbon dioxide gas. In combination with calcium and magnesium they cause carbonate hardness.
Sulfate (SO_4)	Dissolved from rocks and soils containing gypsum, iron sulfides, and other sulfur compounds. Commonly present in mine waters and some industrial wastes.	Sulfate in water containing calcium forms hard scale in steam boilers. In large amounts, sulfate in combination with other ions gives a bitter taste to water. Some calcium sulfate is considered beneficial in the brewing process. USPHS (1962) drinking-water standards recommend that the sulfate content should not exceed 250 mg/l.
Chloride (Cl)	Dissolved from rocks and soils. Present in sewage and found in large amounts in ancient brines, sea water, and industrial wastes.	In large amounts in combination with sodium gives salty taste to water. In large quantities increases the corrosiveness of water. USPHS (1962) drinking-water standards recommend that the chloride content not exceed 250 mg/l.
Fluoride (F)	Dissolved in small to minute quantities from most rocks and soils. Added to many waters by fluoridation of municipal supplies.	Fluoride in drinking water reduces the incidence of tooth decay when the water is consumed during the period of enamel calcification. However, it may cause mottling of the teeth depending on the concentration of fluoride, the age of the child, the amount of water consumed, and the susceptibility of the individual. The maximum concentration of fluoride recommended by the USPHS (1962) varies with the annual average of maximum daily air temperatures and ranges downward from 1.7 mg/l for an average maximum daily temperature of 10.0°C to 0.8 mg/l for an average maximum daily temperature of 32.5°C . Optimum concentrations for these ranges are from 1.2 to 0.7 mg/l.

Table 3 (continued)

Constituent or property	Source or cause	Significance
Nitrate (NO_3)	Decaying organic matter, legume plants, sewage, nitrate fertilizers and nitrates in soils.	Concentration much greater than the local average may suggest pollution. USPHS (1962) drinking-water standards suggest a limit of 45 mg/l. Waters of high nitrate content have been reported to be the cause of methemoglobinemia (an often fatal disease in infants) and therefore should not be used in infant feeding. Nitrate has been shown to be helpful in reducing the intercrystalline cracking of boiler steel. It encourages the growth of algae and other organisms which may cause odor problems in water supplies.
Dissolved solids	Chiefly mineral constituents dissolved from rocks and soils.	USPHS (1962) drinking-water standards recommend that the dissolved solids should not exceed 500 mg/l. However, 1,000 mg/l is permitted under certain circumstances. Waters containing more than 1,000 mg/l of dissolved solids are unsuitable for many purposes. Consumes soap before a lather will form. Deposits soap curd on bathtubs. Hard water forms scale in boilers, water heaters, and pipes. Hardness equivalent to the bicarbonate and carbonate is called carbonate hardness. Any hardness in excess of this is called noncarbonate hardness. Waters of hardness up to 60 mg/l are considered soft; 61-120 mg/l moderately hard; 121-180 mg/l hard; more than 180 mg/l very hard.
Hardness as CaCO_3	In most waters, nearly all the hardness is due to calcium and magnesium. All the metallic cations other than the alkali metals also cause hardness.	Indicates degree of mineralization. Specific conductance is a measure of the capacity of the water to conduct an electric current. It varies with the concentrations and degree of ionization of the constituents, and with temperature.
Specific conductance (micromhos at 25°C).	Mineral content of the water.	A pH of 7.0 indicates neutrality of a solution. Values higher than 7.0 denote increasing alkalinity; values lower than 7.0 denote increasing acidity. pH is a measure of the activity of hydrogen ions. Corrosiveness of water generally increases with decreasing pH. However, excessively alkaline water may also attack metals.
Hydrogen-ion concentration (pH)	Acids, acid-generating salts, and free carbon dioxide lower the pH. Carbonates, bicarbonates, hydroxides, phosphates, silicates, and borates raise the pH.	Water for domestic and some industrial uses should be free from perceptible color. Color in water is objectionable in food and beverage processing and many manufacturing processes.
Color	Yellow-to-brown color of some water usually is caused by organic matter extracted from leaves, roots, and other organic substances. Color in water also results from industrial wastes and sewage.	Affects usefulness of water for many purposes. Most users desire water of uniformly low temperature. Seasonal fluctuations in temperature of surface waters are comparatively large depending on the volume of water.
Temperature	Climatic conditions, use of water as a cooling agent, industrial pollution.	Sediment must generally be removed by flocculation and filtration before water is used by industry or municipalities. Sediment deposits reduce the storage capacity of reservoirs and lakes and clog navigable stream channels and harbors. Particle-size distribution is a factor controlling the density of deposited sediment and is considered in the design of filtration plants. Sediment data are of value in designing river-development projects, in the study of biological conditions and fish propagation, and in programs of soil conservation and watershed management.
Suspended sediment	Erosion of land and stream channels. Quantity and particle-size gradation affected by many factors such as form and intensity of precipitation, rate of runoff, stream channel and flow characteristics, vegetal cover, topography, type and characteristics of soils in drainage basin, agricultural practices, and some industrial and mining activities. Largest concentrations and loads occur during periods of storm runoff.	

¹"Public Health Service Drinking Water Standards," revised 1962, apply to drinking water and water-supply systems used by carriers and others subject to Federal quarantine regulations.

Table 4
Comparison of 75 percentile values of chemical
constituents dissolved in water from each aquifer group

[data in milligrams per liter, or as indicated]							
Constituent	Aquifers					Alluvium Meramec River	Alluvium Mississippi and Missouri Rivers
	Group 1	Group 2	Group 3	Group 4	Group 5		
Silica (SiO ₂)-----	12	8.5	9.4	8.9	9.6	12	30
Iron (Fe)-----	.22	.52	.50	.25	.31	2.2	9.4
Manganese (Mn)-----	----	----	----	----	----	.85	.95
Calcium (Ca)-----	97	105	94	95	120	86	133
Magnesium (Mg)-----	49	51	40	51	58	25	34
Sodium (Na)-----	350	80	35	40	166	34	16
Potassium (K)-----	----	----	----	7.8	----	2.8	5.0
Bicarbonate plus carbonate (HCO ₃ +CO ₃).	515	397	380	420	396	266	528
Sulfate (SO ₄)-----	92	88	36	71	48	65	71
Chloride (Cl)-----	49	32	38	45	370	56	7.5
Fluoride (F)-----	3.0	1.4	.7	.7	.1	.1	.4
Nitrate (NO ₃)-----	2.5	1.9	2.8	1.5	.3	2.3	1.1
Dissolved solids (residue at 180°C).	820	621	475	610	770	476	596
Hardness as CaCO ₃ ---	435	430	345	440	450	324	513
Specific conductance (micromhos at 25°C).	----	----	----	----	----	806	884
pH-----	----	----	----	----	----	7.7	8.0

aquifer group indicated by the number designation of the area. For example, a well drilled in area 3 could expect potable water in all aquifers through the St. Peter Sandstone and Everton Formation.

BEDROCK AQUIFERS

GROUP 1 (POST-MAQUOKETA) AQUIFERS

Water from Group 1 aquifers varies from a calcium-magnesium-bicarbonate type to a sodium-sulfate, sodium-bicarbonate, or a sodium-chloride type. The dissolved-solids content is quite variable, ranging from 246 to 6,880 mg/l. The water is generally low in iron and very hard (Hem, 1970, p. 225). Slightly more than 75 percent of the wells sampled yielded water containing less than 0.3 mg/l of iron. Hardness of water from most of the wells was greater than 180 mg/l. Fluoride content of the water is rela-

tively high. In 50 percent of the samples, the fluoride content was greater than 1.4 mg/l. The analyses of water from 99 wells are summarized in table 6, and selected analyses of water from Group 1 aquifers are given in appendix 2. Locations of the wells are shown on plate 1 and some analyses are shown graphically on plate 2.

The data given in table 6 indicate that just over 50 percent of the wells sampled yielded potable water. These wells are, for the most part, near the outcrop line of Meramecian Series rocks (St. Louis, Salem, and Warsaw Formations) of Mississippian age, and, based upon the 25 percentile values, they yield predominantly calcium-magnesium-bicarbonate type of water. The higher dissolved-solids contents in water from Group 1 aquifers are from an area just north and northwest of the city of St. Louis in St.

Louis County, and in extreme southeastern St. Louis County. Water in these areas generally is a sodium-chloride type, but it may also contain large amounts of calcium and sulfate. Variations in the predominant chemical characteristics between the calcium-magnesium bicarbonate type and the sodium-chloride type are presumably related to the effects of geologic structure, the movement of water from overlying or underlying formations into Group 1 aquifers, and to the presence of certain minerals in the parent rock.

Waters having a high sulfate content are, for the most part, limited to the area underlain by rocks of Pennsylvanian age. These rocks comprise shales, sandstones, and siltstones that locally have minor amounts of pyrite and gypsum. These fine-grained rocks are relatively impermeable; however, over a

large area, they could yield enough seepage to explain some of the sulfate anomalies in the study area. In northeastern St. Louis County, high concentrations of sulfate coincide with the Cheltenham syncline (Fenneman, 1911, fig. 5), and, according to Trapp (1961), the sulfate/chloride ratios indicate that water with a higher sulfate content is moving upward from lower stratigraphic horizons. A persistent zone at the base of the St. Louis Limestone has thin stringers of gypsum that could contribute minor amounts of sulfate to the ground water in this part of the study area (Owens, 1960).

In southeastern St. Louis County, the chemical character of the water changes from a predominantly calcium-magnesium-bicarbonate type to a sodium-bicarbonate type, and, farther downdip, to a sodium-chloride type. The sodium-bicarbonate type of water

Table 5

Comparison of 50 percentile values of chemical constituents dissolved in water from each aquifer group

[data in milligrams per liter, or as indicated]

Constituent	Aquifers					Alluvium Meramec River	Alluvium Mississippi and Missouri Rivers
	Group 1	Group 2	Group 3	Group 4	Group 5		
Silica (SiO ₂)-----	8.6	6.2	8.4	7.2	8.0	11	26
Iron (Fe)-----	.15	.15	.17	.11	.19	.75	5.2
Manganese (Mn)-----	----	----	----	----	----	.76	.75
Calcium (Ca)-----	71	66	74	78	68	66	106
Magnesium (Mg)-----	37	36	30	39	38	20	26
Sodium (Na)-----	80	27	15	15	7.6	21	11
Potassium (K)-----	----	----	----	4.1	----	1.8	3.9
Bicarbonate plus carbonate (HCO ₃ +CO ₃).	440	352	347	350	342	212	449
Sulfate (SO ₄)-----	30	38	20	37	23	45	26
Chloride (Cl)-----	12	11	9.0	10	6.7	29	4.1
Fluoride (F)-----	1.4	.7	.4	.2	.1	.0	.2
Nitrate (NO ₃)-----	.9	.6	.6	.4	.2	.4	.2
Dissolved solids (residue at 180°C).	480	418	390	430	392	351	476
Hardness as CaCO ₃ --	360	313	302	350	353	247	402
Specific conductance (micromhos at 25°C).	----	----	----	----	----	593	773
pH-----	----	----	----	----	----	7.8	7.6

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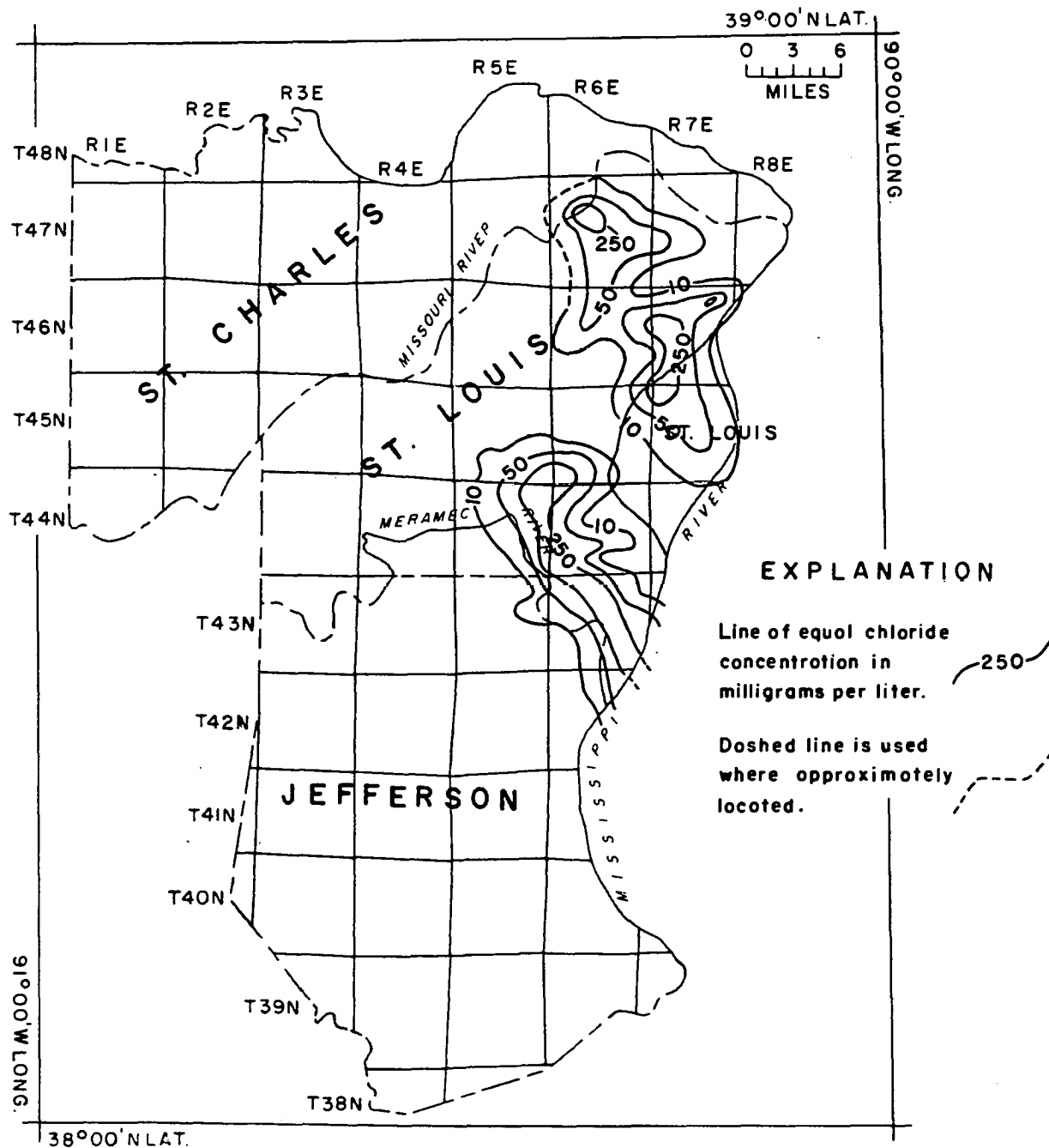


Figure 12
Distribution of chloride in Group 1 (Post-Maquoketa) aquifers.

evidently is a result of base-exchange — a process in which calcium and magnesium ions in the water are replaced by sodium ions. The minimum values shown on table 6 for calcium and magnesium are for analyses of water from this area.

Both of these areas of high dissolved solids coincide with synclinal or anticlinal structures developed in the rocks. The area in eastern St. Louis County coincides with the northern part of the Cheltenham syncline, the Florissant dome and the Twelfth Street anticline, and the area in southeastern St. Louis County coincides with a troughlike depression which is apparent on structural maps prepared by Trapp (1961). Figure 12 is a map showing the generalized distribution of chloride in Group 1 aquifers. It is possible that groundwater circulation is extremely poor in these areas and the high chloride water has not been flushed from the aquifers. However, it is more probable that mineralized water has moved into some of the structures from deeper horizons or from adjacent gas- and oil-bearing rocks.

High concentrations of iron were found in water from many areas (fig. 13). Although the reasons for the high iron content are not known, the

same form of geochemical control is probably responsible for all of the high values in the study area.

The high fluoride values in water from this group could result from solution of fluorite in the aquifers. However, increases in fluoride concentration have been noted in other parts of the State accompanying encroachment of saline water.

GROUP 2 (KIMMSWICK-JOACHIM) AQUIFERS

Water from wells that bottom in Group 2 aquifers range in dissolved-solids content from 207 to 17,500 mg/l, with 75 percent of the samples containing less than 621 mg/l (table 7). At the higher levels of dissolved solids, the waters are a sodium-chloride type. The waters generally are low in iron content; 68 percent of the samples analyzed contained less than 0.3 mg/l. Hardness of the water ranges from 128 to 1,270 mg/l. The fluoride content of 75 percent of the samples analyzed was less than 1.4 mg/l. The analyses of water from 57 wells are summarized in table 7. Twenty of these analyses were from wells that are open only to Group 2 aquifers. The remainder of the analyses are from wells open to Group 1 and Group 2 aquifers. Selected analyses of water from Group 2 aquifers are given in

Table 6

Maximum, minimum, and 25, 50, 75 percentile values for constituents in water from Group 1 (post-Maquoketa) aquifers^{a/}

Constituent	Maximum	Percent of Samples			Minimum
		75	50	25	
Silica (SiO ₂)-----	38	12	8.6	5.8	0.1
Iron (Fe)-----	13	0.22	0.15	0.12	0.02
Calcium (Ca)-----	1,380	97	71	42	3.6
Magnesium (Mg)-----	131	49	37	25	1.1
Sodium (Na)-----	2,400	350	80	22	7.6
Bicarbonate plus carbonate (HCO ₃ +CO ₃).	857	515	440	350	220
Sulfate (SO ₄)-----	1,290	92	30	18	0.2
Chloride (Cl)-----	3,420	49	12	5.5	0.5
Fluoride (F)-----	13	3.0	1.4	.3	.0
Nitrate (NO ₃)-----	77	2.5	.9	.0	.0
Dissolved solids (residue at 180°C).	6,880	820	480	395	246
Hardness as CaCO ₃ --	3,950	435	360	220	14

^{a/} Data based on analyses from 99 wells.

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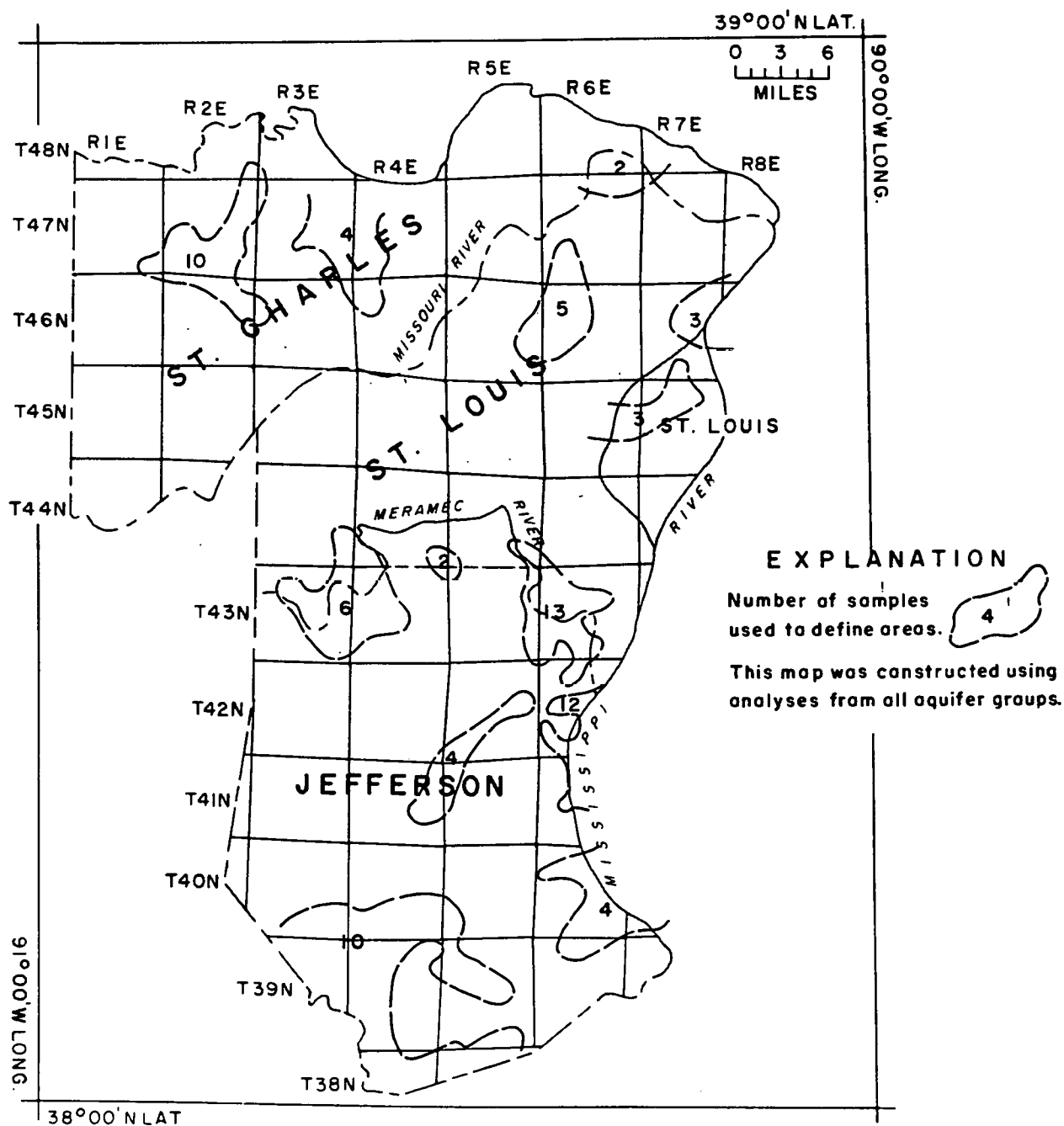


Figure 13

Areas in which iron concentrations in ground water from bedrock aquifers are in excess of 0.3 milligrams per liter.

Table 7

Maximum, minimum, and 25, 50, 75 percentile values for constituents in water from Group 2 (Kimmswick-Joachim) aquifers^{a/}

Constituent	Maximum	Percent of Samples			Minimum
		75	50	25	
Silica (SiO ₂)-----	27	8.5	6.2	4.4	1.2
Iron (Fe)-----	34	.52	.15	.09	.01
Calcium (Ca)-----	279	105	66	46	12
Magnesium (Mg)-----	188	51	36	30	12
Sodium (Na)-----	5,960	80	27	12	4.4
Bicarbonate plus carbonate (HCO ₃ +CO ₃).	523	397	352	310	141
Sulfate (SO ₄)-----	1,320	88	38	21	1.6
Chloride (Cl)-----	10,000	32	11	4.6	2.2
Fluoride (F)-----	3.5	1.4	.7	.3	0
Nitrate (NO ₃)-----	13	1.9	.6	.1	0
Dissolved solids (residue at 180°C).	17,000	621	418	344	207
Hardness as CaCO ₃ --	1,270	430	313	255	128

^{a/} Data based on analyses from 57 wells.

appendix 2. Locations of the wells sampled are shown on plate 1, and a few analyses are shown graphically on plate 2.

Approximately 64 percent of the wells sampled in Group 2 aquifers yielded potable water. These potable waters generally are a calcium-magnesium-bicarbonate type, but a comparison of the 50 and 75 percentile values in table 7 shows significant increases in sodium, sulfate, and chloride with higher dissolved-solids content, indicating that the chemical character of the water is changing to a sodium-sulfate or sodium-chloride type.

Water from wells adjacent to the Meramec River in T. 44 N., R. 4 and 5 E., in the Valley Park area, and in T. 42 N., R. 6 E., in Jefferson County, had a higher dissolved-solids content. The wells in the Valley Park area are in a synclinal structure that may still contain connate water. Some of the mineralized water is moving from deeper horizons, either through natural fractures or through abandoned well bores. The area in Jefferson County is in the vicinity of the Maxville fault and it may not be completely flushed of connate water. Wells in areas to the north and northeast where Group 2 aquifers

are more deeply buried undoubtedly yield saline water. Figure 14 shows the generalized distribution of chloride in Group 2 aquifers.

GROUP 3 (ST. PETER-EVERTON) AQUIFERS

The chemical characteristics of water given here represent a composite of waters from the St. Peter Sandstone and Everton Formation and from the overlying aquifer groups. Of the 63 analyses of water from wells bottoming in aquifer Group 3, one well derived its water solely from this group. The location of the wells sampled are shown on plate 1, and selected analyses are shown graphically on plate 2. Because of the mixing of water from the different aquifer groups, the chemical characteristics shown for Group 3 water are similar in many respects to those for the overlying groups. However, some differences do exist. The summary of analytical data in table 8 shows the water to be generally a calcium-magnesium-bicarbonate type. Dissolved-solids content ranges from 264 to 7,270 mg/l, with 75 percent of the samples containing less than 475 mg/l. Hardness of the water ranges from 30 to 1,420 mg/l, and the iron and fluoride contents

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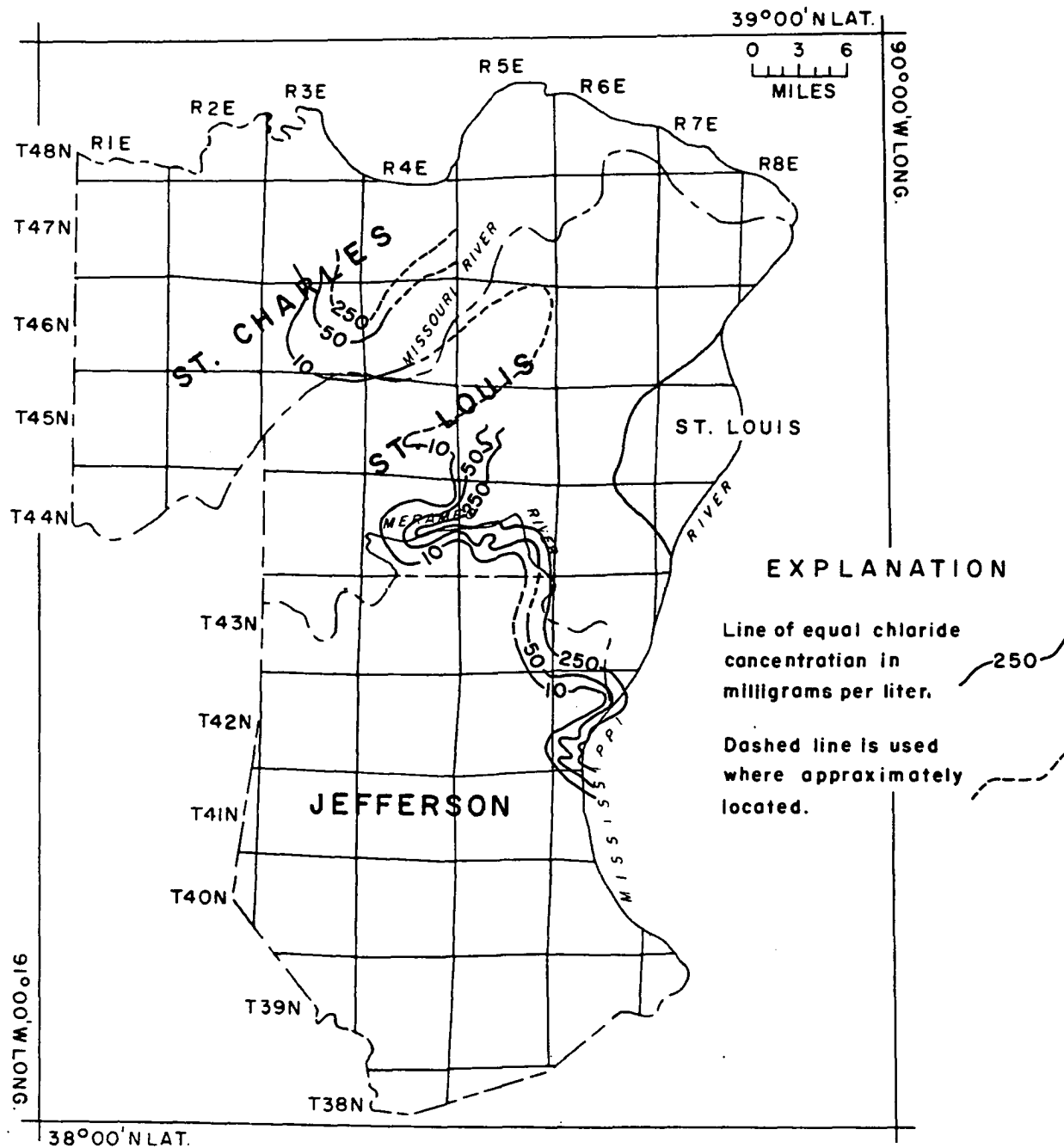


Figure 14
Distribution of chloride in Group 2 (Kimmswick-Joachim) aquifers.

Table 8

Maximum, minimum, and 25, 50, 75 percentile values for constituents in water from Group 3 (St. Peter-Everton) aquifers^{a/}

Constituent	Maximum	Percent of Samples			Minimum
		75	50	25	
Silica (SiO ₂)-----	13	9.4	8.4	6.8	2.0
Iron (Fe)-----	18	.50	.17	.09	.04
Calcium (Ca)-----	325	94	74	59	6.5
Magnesium (Mg)-----	290	40	30	26	6.3
Sodium (Na)-----	1,810	35	15	7.8	1.6
Bicarbonate plus carbonate (HCO ₃ +CO ₃)	536	380	347	314	217
Sulfate (SO ₄)-----	442	36	20	13	4.1
Chloride (Cl)-----	5,050	38	9.0	3.0	1.4
Fluoride (F)-----	2.5	.7	.4	.3	0
Nitrate (NO ₃)-----	17	2.8	.6	.1	0
Dissolved solids (residue at 180°C).	7,270	475	390	335	264
Hardness as CaCO ₃ ----	1,420	345	302	279	30

^{a/} Data based on analyses from 63 wells.

generally are moderate. A comparison of the 75 percentile values of water from Group 1, 2, and 3 (tables 6, 7, and 8) shows that water from Group 3 generally is less mineralized than water from Groups 1 and 2 indicating that most of the wells bottoming in Group 3 aquifers derive their water from the St. Peter Sandstone and Everton Formation.

Most of the wells that yielded water with a high dissolved-solids content are located in or near the water-quality problem areas discussed for Groups 1 and 2. Distribution of chloride concentrations in water from Group 3 (Everton-St. Peter) aquifers is shown on figure 15. These chloride values are not as high as would be expected from connate water and they evidently are a result of leakage of more mineralized water from underlying or overlying formations.

GROUP 4 (POWELL-GASCONADE) AQUIFERS

Water from Group 4 aquifers generally is a moderately mineralized, calcium-magnesium-bicarbonate type in and near areas of outcrop. In eastern St. Charles, eastern St. Louis, and northeastern Jefferson Counties, where the rocks are deeply

buried, the aquifers yield a highly mineralized, sodium-chloride type of water. The dissolved-solids content ranges from 256 to 9,970 mg/l. The water is generally low in iron and very hard. More than 75 percent of the wells sampled yielded water containing less than 0.3 mg/l of iron. The fluoride content of the water from Group 4 aquifers is relatively low; however, 25 percent of the samples analyzed contained more than 1.5 mg/l. Analyses of water from 48 wells are summarized in table 9. Many of these analyses are for water from Group 4 aquifers only; however, several of the wells are also open to the aquifer groups previously discussed. Selected analyses of water from Group 4 aquifers are given in appendix 2. Locations of the wells sampled are shown on plate 1 and selected analyses are shown graphically on plate 2.

Areas where Group 4 aquifers yield potable water are limited to the southern and western parts of the study area (pl. 2). Within this area, the water is predominantly a calcium-magnesium-bicarbonate type. In the vicinity of De Soto, however, water from this aquifer group has a higher dissolved-solids content and contains significant quantities of sulfate.

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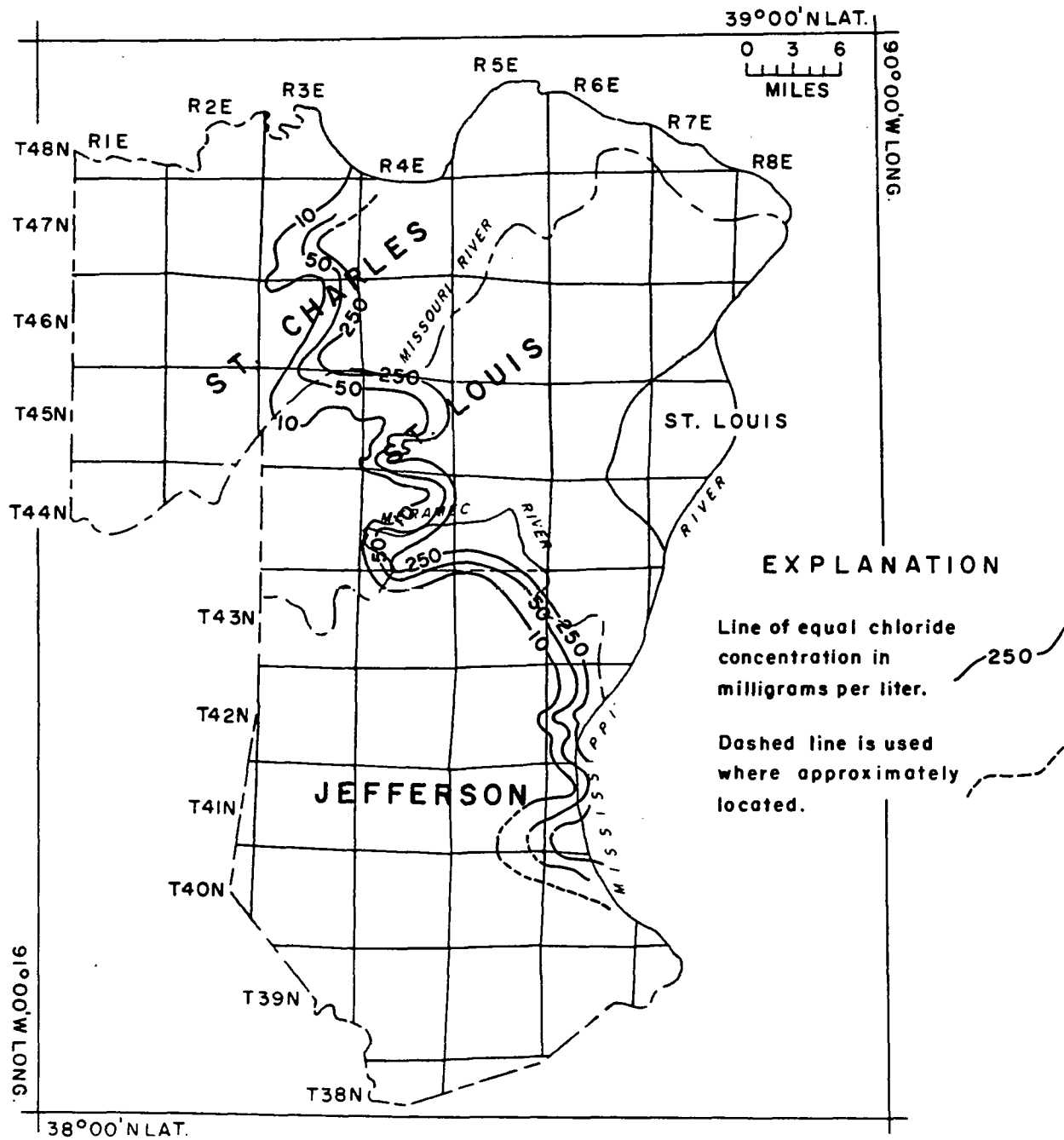


Figure 15

Distribution of chloride in Group 3 (St. Peter-Everton) aquifers.

The reason for the higher sulfate content in this area may be the oxidation and subsequent solution of sulfide minerals occurring locally.

Wells yielding water with a high chloride content are located just north of Herculaneum, adjacent to the Mississippi River in Jefferson County and in the Valley Park area in St. Louis County (fig. 16). The wells north of Herculaneum are located on the downthrown side of a fault, and it is probable that connate water has not been flushed from the aquifers here. In the Valley Park area, these aquifers contain highly mineralized water and they are presumed to be the source of mineralized water in the overlying formations. Wells in Valley Park that were drilled into these aquifers flowed at the surface. Some of these wells were abandoned. One of the wells is still flowing, indicating that the hydrostatic pressure is sufficient to move the mineralized water upward into the other formations.

GROUP 5 (EMINENCE-LAMOTTE) AQUIFERS

Potable water in Group 5 aquifers is limited to the southern third of the study area. Farther to the

north and northeast these rocks are deeply buried and contain highly mineralized water (pl. 2). The results of chemical analyses of water from 24 wells are summarized on table 10, and selected analyses are given in appendix 2. Locations of the wells sampled are on plate 1, and selected analyses are shown graphically on plate 2. The dissolved-solids content of water from wells in Group 5 aquifers ranged from 279 to 13,500 mg/l, the lower values characteristic of water from wells near the outcrop and the higher values characteristic of water down dip.

The water is very hard and generally is low in both iron and fluoride content. Values given for the 50 and 25 percentiles on table 10 indicate the calcium-magnesium-bicarbonate character of the water at the lower dissolved-solids contents. A comparison of the 50 and 75 percentile values shows that increases in dissolved-solids content in excess of about 400 mg/l are due principally to increases in the sodium and chloride contents. Although the 50 and 25 percentile values emphasize the calcium-magnesium-bicarbonate character of the water, minor variations in the concentrations of other constituents can be expected because of the influence of water from overlying aquifers which may be open to the well.

Table 9

Maximum, minimum, and 25, 50, 75 percentile values for constituents in water from Group 4 (Powell-Gasconade) aquifers^{a/}

Constituent	Maximum	Percent of Samples			Minimum
		75	50	25	
Silica (SiO ₂)-----	20	8.9	7.2	5.6	2.3
Iron (Fe)-----	4.0	.25	.11	.06	.01
Calcium (Ca)-----	479	95	78	68	18
Magnesium (Mg)-----	201	51	39	32	22
Sodium (Na)-----	2,570	40	15	7.0	2.5
Potassium (K)-----	13	7.8	4.1	2.2	1.3
Bicarbonate plus carbonate (HCO ₃ +CO ₃)	597	420	350	310	134
Sulfate (SO ₄)-----	564	71	37	21	3.1
Chloride (Cl)-----	4,550	45	10	4.2	2.0
Fluoride (F)-----	3.0	.71	.2	.1	.0
Nitrate (NO ₃)-----	55	1.5	.4	.1	0
Dissolved solids (residue at 180°C).	9,970	610	430	360	256
Hardness as CaCO ₃ ----	2,020	440	350	300	68

^{a/} Data based on analyses from 48 wells.

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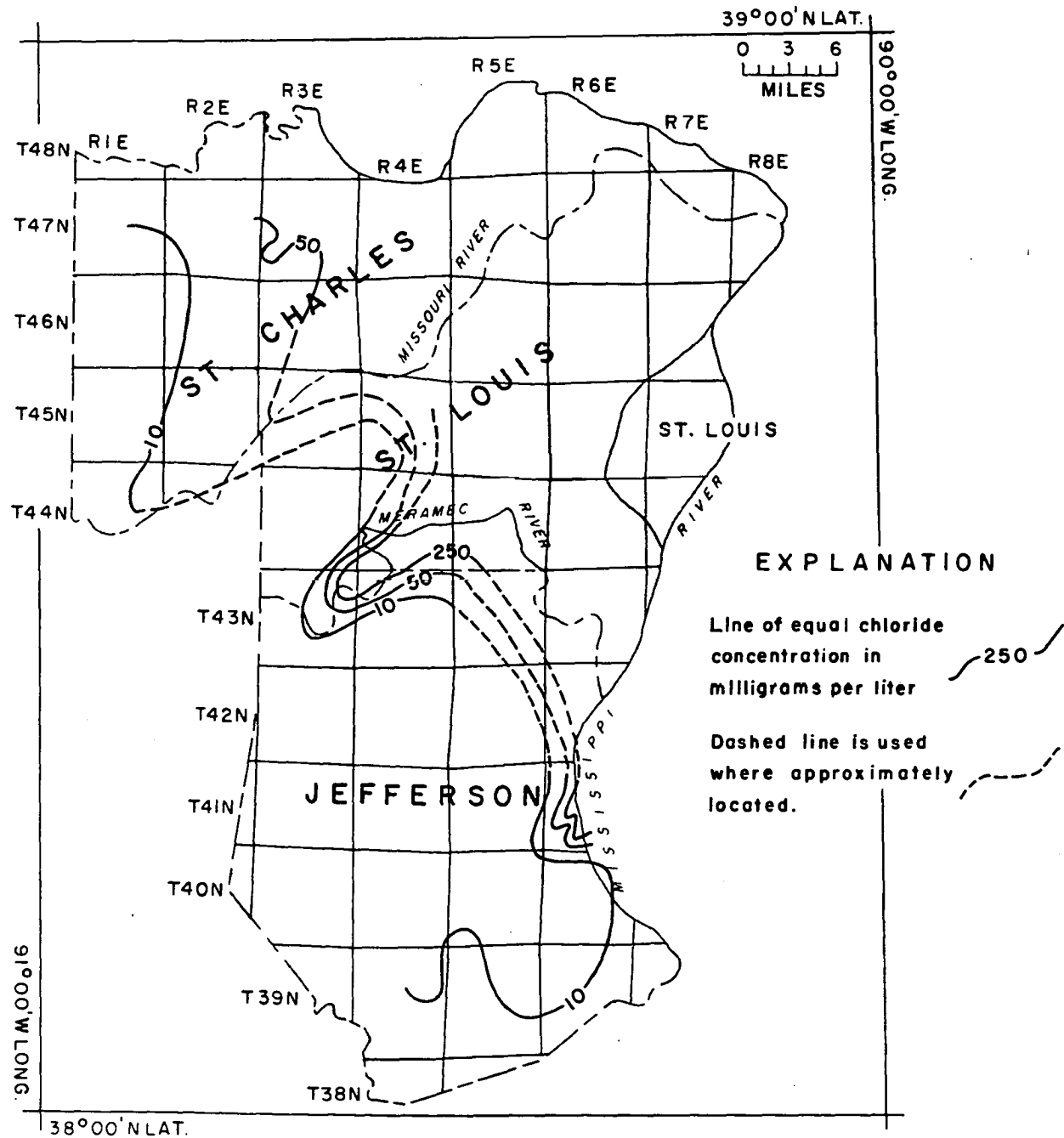


Figure 16
Distribution of chloride in Group 4 (Powell-Gasconade) aquifers.

ALLUVIAL AQUIFERS

MISSISSIPPI AND MISSOURI RIVER ALLUVIUM

Water from alluvial deposits along the Mississippi and Missouri Rivers has fairly uniform chemical characteristics, except that it varies widely in dissolved-solids content. The water generally is a calcium-magnesium-bicarbonate type and locally may contain significant quantities of sulfate. The iron and manganese contents commonly are high, and the water is very hard. Complete analyses are given in table 2, appendix 2. Locations of the wells are shown on plate 1 and selected analyses are shown graphically on plate 2. The maximum and minimum values and the values which were equal to or less than that found in 75, 50, and 25 percent of the samples analyzed are given in table 11. These data emphasize the calcium-magnesium-bicarbonate character of the water. A comparison of the 75 percentile values with the maximum values shows that the near-maximum values for sodium, chloride, and nitrate are unusual. The maximum value for nitrate probably is a result of contamination from a surface waste source. The maximum values for sodium and chloride are thought

to result from the infiltration of saline water from a nearby flowing deep well.

Areal variations in the chemical character and dissolved-solids content of the water are indicated by the graphical representation of selected analyses in plate 2. These bar diagrams emphasize the predominant calcium-magnesium-bicarbonate character of water in most of the area. Except for wells 47-4-30b and 48-7-33d, variations in the chemical character and dissolved-solids content of the water appear to be random and are probably caused by variations in the chemical composition of the aquifer material, by the length of time the water has been in contact with the aquifer material, and by the differences in permeability of the aquifer.

MERAMEC RIVER ALLUVIUM

Water from alluvial deposits along the Meramec River generally is a calcium-magnesium-bicarbonate type. However, in local areas, principally Valley Park and Times Beach, some wells yield a sodium-chloride type of water. For the most part the water is moderately mineralized. Dissolved-solids content

Table 10

Maximum, minimum, and 25, 50, 75 percentile values for constituents in water from Group 5 (Eminence-Lamotte) aquifers^{a/}

Constituent	Maximum	Percent of Samples			Minimum
		75	50	100	
Silica (SiO ₂)-----	1.8	9.6	8.0	5.5	1.0
Iron (Fe)-----	2.0	.31	.19	.06	.02
Calcium (Ca)-----	639	120	68	60	49
Magnesium (Mg)-----	602	58	38	34	26
Sodium (Na)-----	5,420	166	7.6	2.9	1.6
Bicarbonate plus carbonate (HCO ₃ +CO ₃).	469	396	342	301	269
Sulfate (SO ₄)-----	547	48	23	18	13
Chloride (Cl)-----	6,900	370	6.7	4.2	2.3
Fluoride (F)-----	3.2	.1	.1	.1	.0
Nitrate (NO ₃)-----	16	.3	.2	.1	.0
Dissolved solids (residue at 180°C).	13,500	770	392	341	279
Hardness as CaCO ₃ ---	4,060	450	353	305	247

^{a/} Data based on analyses from 24 wells.

Table 11

Maximum, minimum, and 25, 50, 75 percentile values for constituents in water from Mississippi and Missouri River alluvium

[Data in milligrams per liter, or as indicated]					
Constituent	Maximum	Percent of Samples			Minimum
		75	50	25	
Temperature (°C)-----	19	15	13.5	13	12
Silica (SiO ₂)-----	37	30	26	22	12
Iron (Fe)-----	48	9.4	5.2	2.9	.06
Manganese (Mn)-----	4.3	.95	.75	.39	.15
Calcium (Ca)-----	172	133	106	81	46
Magnesium (Mg)-----	48	34	26	19	10
Sodium (Na)-----	224	16	11	7.6	1.1
Potassium (K)-----	6.2	5.0	3.9	1.4	.8
Bicarbonate (HCO ₃)---	784	528	449	332	184
Sulfate (SO ₄)-----	132	71	26	8.9	.4
Chloride (Cl)-----	334	7.5	4.1	2.0	.5
Fluoride (F)-----	.5	.4	.2	.2	.0
Nitrate (NO ₃)-----	15	1.1	.2	.0	.0
Dissolved solids (residue at 180°C).	1,030	596	476	385	205
Hardness as CaCO ₃ ---	820	513	402	312	156
Specific Conductance (Micromhos at 25°C).	1,760	884	773	625	316
pH (units)-----	8.2	8.0	7.6	7.3	7.0
Color (units)-----	35	6	4	2	0

ranges from 122 to 1,070 mg/l and 75 percent of the samples contained less than 476 mg/l. Hardness of the water ranges from 88 to 456 mg/l, with most of the water being very hard. The water also contains significant quantities of iron and manganese. Sixty-six percent of the samples exceeded the U.S. Public Health Service (1962) drinking water standards of 0.3 mg/l for iron. The ranges in concentration and the 75, 50, and 25 percentiles of the principal constituents and properties of the water are given in table 12. A comparison of the maximum values with those equal to or less than that found in 75 percent of the samples indicates that near-maximum values are, for the most part, unusual. Selected analyses are given in table 2, appendix 2. Locations

of the wells are shown on plate 1, and selected analyses are shown graphically on plate 2.

Areal differences in the chemical character of the water are caused by variations in the lithology and permeability of the alluvial deposits, by intrusion of saline water from bedrock formations, and locally by effluents from septic tanks or other waste-disposal systems. Water-quality characteristics vary in most parts of the alluvial area because of the variability of the character and composition of aquifer materials, principally the amount of clays and degree of sorting. In general, the dissolved-solids content is lower along the bluffs or outer edge of the alluvium and increases gradually as the water moves toward the river. The high nitrate content of water from a

Table 12

Maximum, minimum, and 25, 50, 75 percentile values for constituents in water from Meramec River alluvium

Constituent	Maximum	Percent of Samples			Minimum
		75	50	25	
Temperature (°C)-----	16	14	14	13	12
Silica (SiO ₂)-----	20	12	11	9.6	8.8
Iron (Fe)-----	21	2.2	.75	.17	.00
Manganese (Mn)-----	4.6	.85	.76	.28	.00
Calcium (Ca)-----	150	86	66	57	20
Magnesium (Mg)-----	34	25	20	16	9.0
Sodium (Na)-----	230	34	21	8.4	4.0
Potassium (K)-----	8.0	2.8	1.8	1.4	.8
Bicarbonate (HCO ₃)---	478	266	212	158	100
Sulfate (SO ₄)-----	280	65	45	34	10
Chloride (Cl)-----	480	56	29	9.2	2.7
Fluoride (F)-----	.3	.1	.0	.0	.0
Nitrate (NO ₃)-----	17	2.3	.4	.0	.0
Dissolved solids (residue at 180°C).	1,070	476	351	299	122
Hardness as CaCO ₃ ---	456	324	247	212	88
Specific conduct- ance (Micromhos at 25°C)-----	1,790	806	593	488	210
pH (units)-----	8.1	7.7	7.8	7.3	6.5
Color (units)-----	75	5	5	2	1

few of the wells is presumably caused by waste-disposal practices.

Anomalous areas of higher dissolved-solids content are in the Valley Park and Times Beach areas. Available data indicate that the higher dissolved-solids content is due to the increased sodium and chloride content and that the more highly mineralized water is the result of natural upward leakage of saline water from the bedrock formations. Leakage also occurs through nonplugged abandoned wells which were drilled into the Roubidoux Formation.

The area of greatest impact of increased mineralization of water in the alluvium is in the western side of Valley Park in the vicinity of well 17 cbd and well 17 cdb. The distribution of chloride

in the alluvium in Valley Park for periods of high and low water levels is shown in figure 17. The chloride content at approximately monthly intervals is shown in table 13 for the two industrial wells and the two Valley Park municipal wells (18 dda₁ and 18 dda₂).

Although the chloride content of water from these wells varies considerably with time, the patterns of chloride distribution are similar. The isochlors apparently shift slightly in response to the relative pumping rates and duration of pumping of the production wells in the area; that is, if well 17 cbd is being pumped at a greater rate than well 17 cdb, higher concentrations of chloride will be nearer well 17 cbd, but if both wells are shut down and

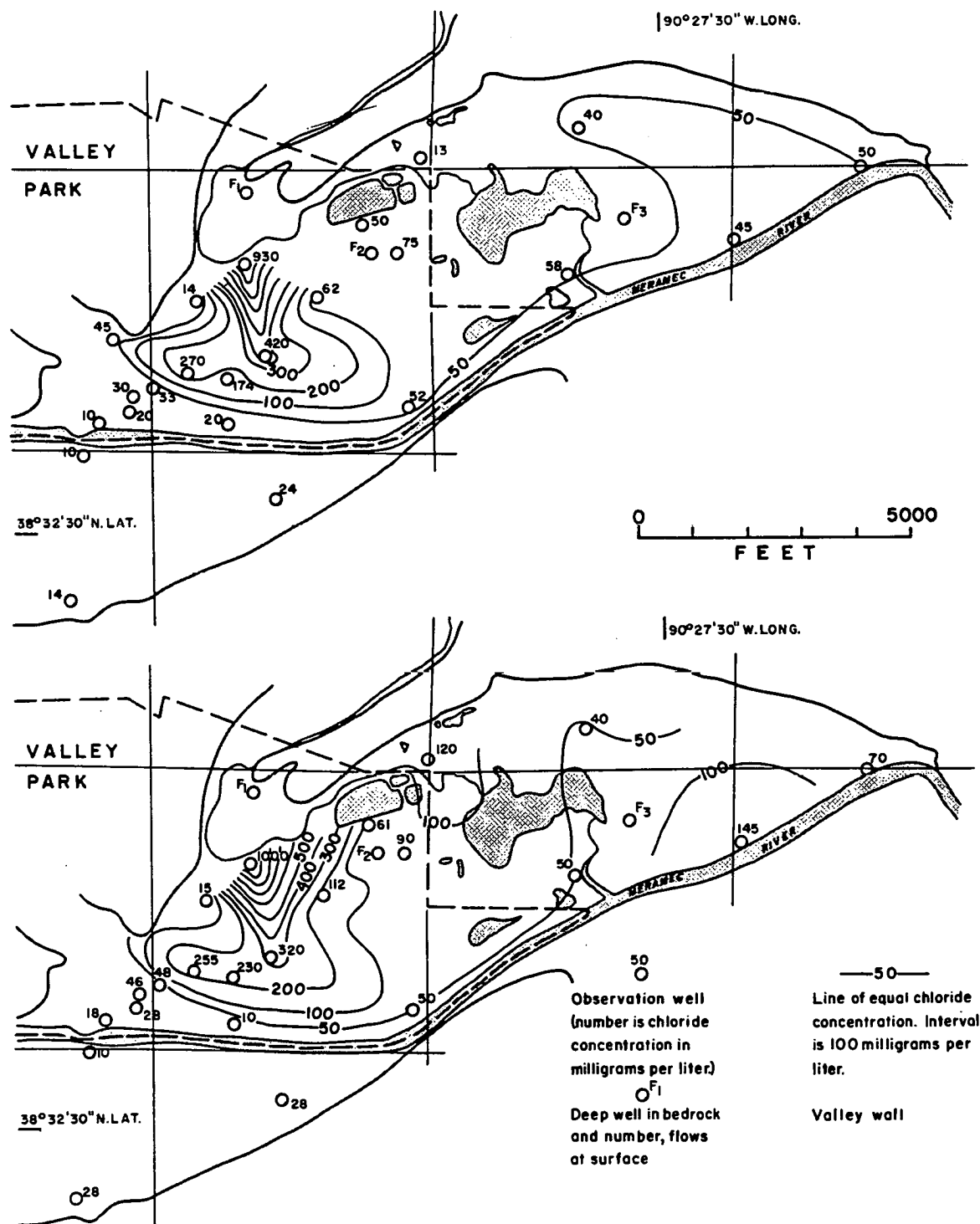


Figure 17

Distribution of chloride in alluvial deposits in the Valley Park-Kirkwood area. In May 1970 (top), the

water levels were relatively high. In July 1970 (bottom), the water levels were relatively low.

only municipal wells 18dda₁ and 18dda₂ are pumping, the high chloride water will migrate toward the municipal wells.

The principal source of mineralized water is presumed to be abandoned or leaky deep wells.

Well F₁ has been plugged and cannot be sampled, but the chemical quality of its water should be similar to that from wells F₂ and F₃. Partial analyses of water samples from these two wells are given below:

Dissolved constituents are expressed in milligrams per liter

Well	Date	Calcium	Magne- sium	Sodium	Bicar- bonate	Sulfate	Chloride	Dissolved solids
F ₂	6-4-68	465	190	2,380	257	280	4,640	9,210
F ₃	6-4-68	450	180	2,350	256	253	4,680	8,930

A graphical comparison of analyses of water from well F₂, wells 17 cbd and 17 cdb at Ashland Chemical Co. and Absorbent Cotton Co., and Valley Park municipal well no. 1 (fig. 18) shows the similarity of the type of water from the deep well and from wells 17 cbd and 17 cdb. The pattern for Valley Park no. 1 well does not show the effect of more mineralized water, but a tabulation of this well's chloride data (tbl. 13) does show an increase in chloride content beginning with samples collected in December 1970. This indicates that more mineralized water was moving into this well at that time.

Water in alluvial deposits in the Times Beach area, particularly in T. 44 N., has a higher dissolved-solids content and is similar in chemical character to that in the Valley Park area. The chloride content of water from selected wells in the Times Beach area

is shown in table 14. These data show a considerable range in concentration of chloride; however, public supply well 44-4-32bdd is consistently high, probably because the pumping of this well draws water with a higher chloride content into the well. Areal variation in chloride content for two periods are shown in figure 19. Chloride values on these illustrations indicate that the maximum concentration of chloride shifts about midway from the bluffs to the river. However, all of the water in this area is affected by the intrusion of mineralized water. Water from well 44-4-31dca adjacent to the bluff has a higher chloride content than that in wells just south of this area. For the most part, the origin of the more mineralized water in the Times Beach area is presumed to be from an underlying bedrock formation. However, the ways in which the more mineralized water reaches the alluvium are not known.

SPRINGS

Discharge measurements in the three-county area indicate that the springs are small and quite variable, reacting quickly to precipitation and having little or no flow during dry weather. This variability severely limits their economic significance because most enterprises utilizing springflow require a stable, dependable source. In fact, only one small commercial

operation using springs (watercress production) exists in the area at this time. As reported by Lutzen of the Missouri Geological Survey (oral commun., 1971) some of the springs are affected by effluent from septic tanks, lagoons, and sanitary landfills, making them esthetically undesirable and further limiting their small economic potential.

SURFACE WATER

A tremendous surface-water resource is one of the principal reasons for the continuing economic growth and development of this three-county area. The Mississippi, Missouri and Meramec Rivers furnish water for most of the population and industries, provide navigable waterways for commerce and recreation, and are a means for disposal of industrial wastes and sewage. The combined flow of the Mississippi and Missouri Rivers at St. Louis averages 112,000 mgd and the Meramec River near Eureka averages 1,930 mgd. Of the vast amount of available surface water, an average of only about 1,120 mgd is withdrawn for all uses.

It is quite evident that there is no shortage of surface water supplies for the major users who can tap the large rivers of the area. However, users who are interested in smaller supplies from tributary streams (those streams which originate in or have much of their drainage basin in the project area) face more difficult problems. The frequency data and interpretations presented in the remainder of this section of the report can be used as a guide toward the optimum utilization of these valuable resources. The information used for surface water computations was compiled from an extensive network of streamflow data sites, as shown in figure 2.

Table 13

Chloride content of water from
selected wells in the Valley Park area, Mo.

Date	[in milligrams per liter]			
	Well Number			
	44-5-17chd	44-5-17odb	44-5-18dda	44-5-18dda ₂
7-22-69	249	---	33	27
8-27-69	247	277	32	--
9-24-69	245	265	30	25
10-24-69	212	160	28	28
11-20-69	248	200	25	25
12-18-69	245	210	28	18
1-28-70	262	208	32	24
2-27-70	286	186	46	22
3-27-70	322	---	25	17
4-30-70	290	214	32	22
5-20-70	270	174	30	20
6-24-70	250	133	26	34
7-24-70	255	230	46	28
8-27-70	252	202	39	31
10-2-70	232	---	49	23
12-3-70	152	302	65	33
1-29-71	152	278	82	36
3-3-71	162	242	75	30
4-5-71	152	258	87	34

MILLIEQUIVALENTS PER LITER

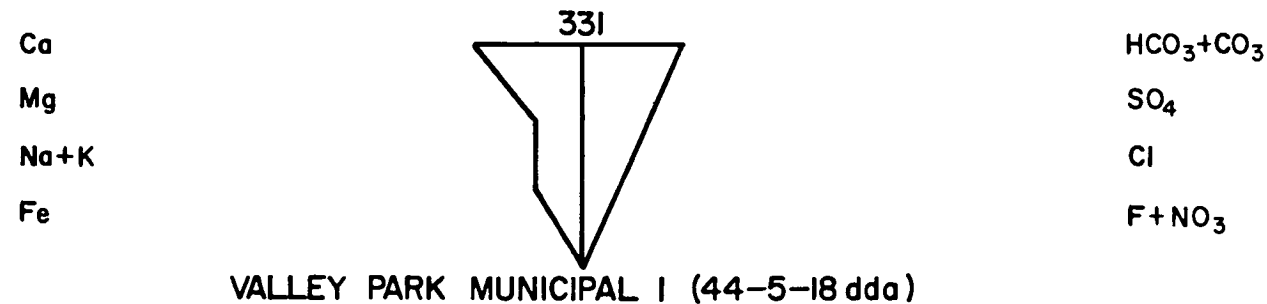
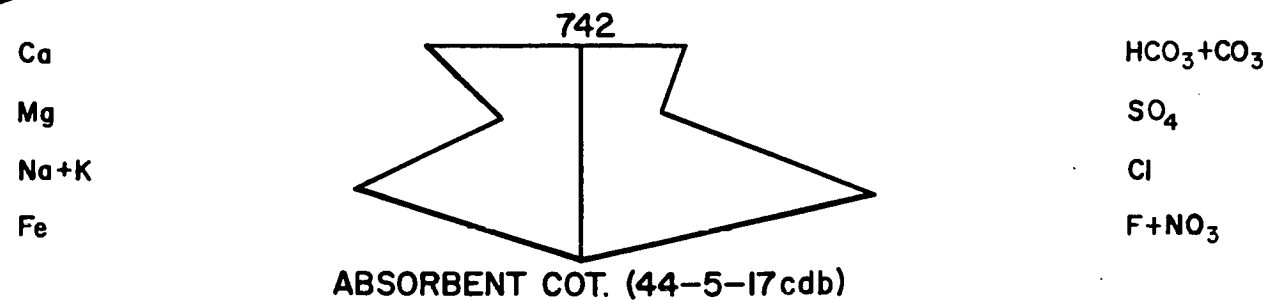
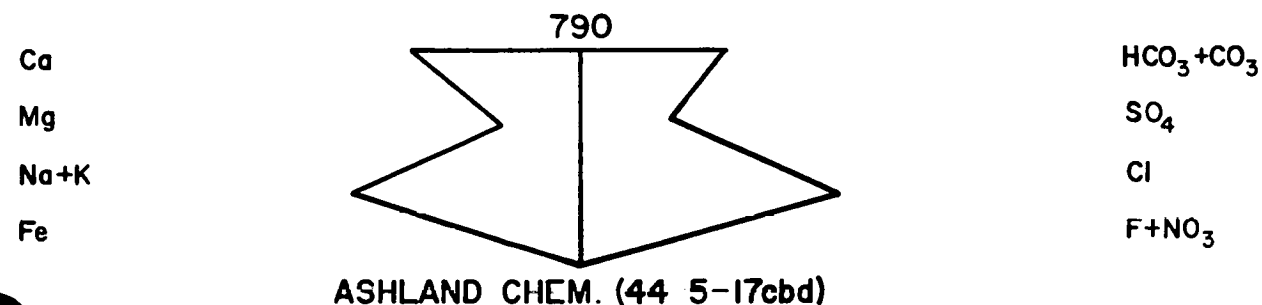
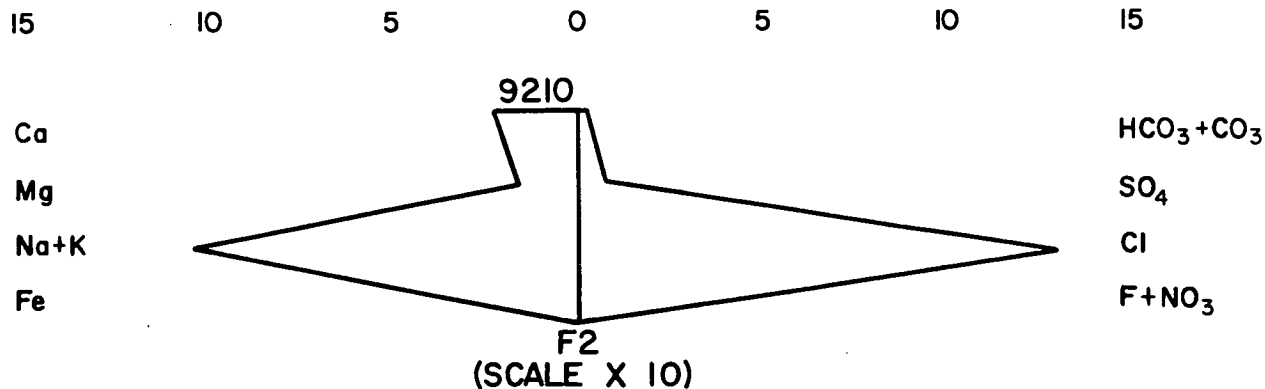


Figure 18

Comparison of chemical analyses of water from well F₂, Ashland Chemical Co. well, Absorbent Cotton Co. well, and Valley Park municipal well no. 1.

MISSISSIPPI AND MISSOURI RIVERS

The Mississippi and Missouri Rivers are treated separately in this report because their flow characteristics are significantly different from those of other streams in the project area. They are the principal reason for the present location of the City of St. Louis and are increasingly important as national arteries of commerce. Developments having large water-supply or waste-dilution requirements naturally tend to concentrate along these great rivers.

The Missouri River is almost completely controlled by an extensive reservoir system in the headwater areas. Summer flows are maintained at levels which insure adequate depths for navigation purposes, and the flooding potential has been greatly reduced. The Mississippi River, on the other hand, is not significantly controlled at medium and high stages above the confluence with the Missouri. Navigation depths are maintained by a system of locks and dams which alter mean and high flows very little; thus, flooding is a more frequent problem on this river.

In order to fully analyze the streamflow data for the gaging stations on the two rivers, a complete systems analysis of the basins upstream from the stations would be required. This would involve the development of flow-storage models of reservoirs and channels and generation of natural-flow data for model input. These procedures are beyond the scope of this study because of their cost and complexity and must be deferred until methodology is developed. However, the available statistical and flow variability data are relevant to many current and future studies; these data are presented in appendix 3.

DURATION OF FLOWS

The slope and shape of the flow duration curve indicate the variability of streamflow and hydrologic characteristics of a drainage basin, thus providing an excellent comparison of the flow characteristics of streams (fig. 20). A curve with steep slope denotes a

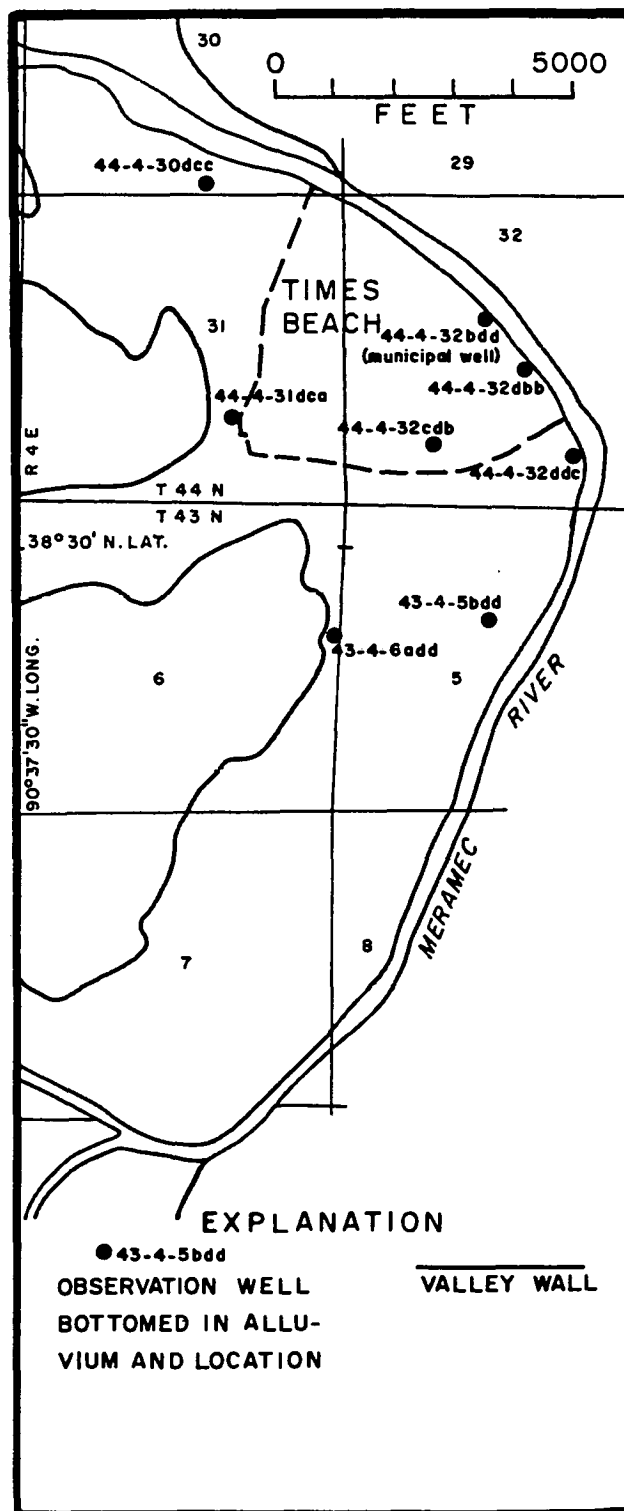


Figure 19
Location of wells in the Times Beach area.

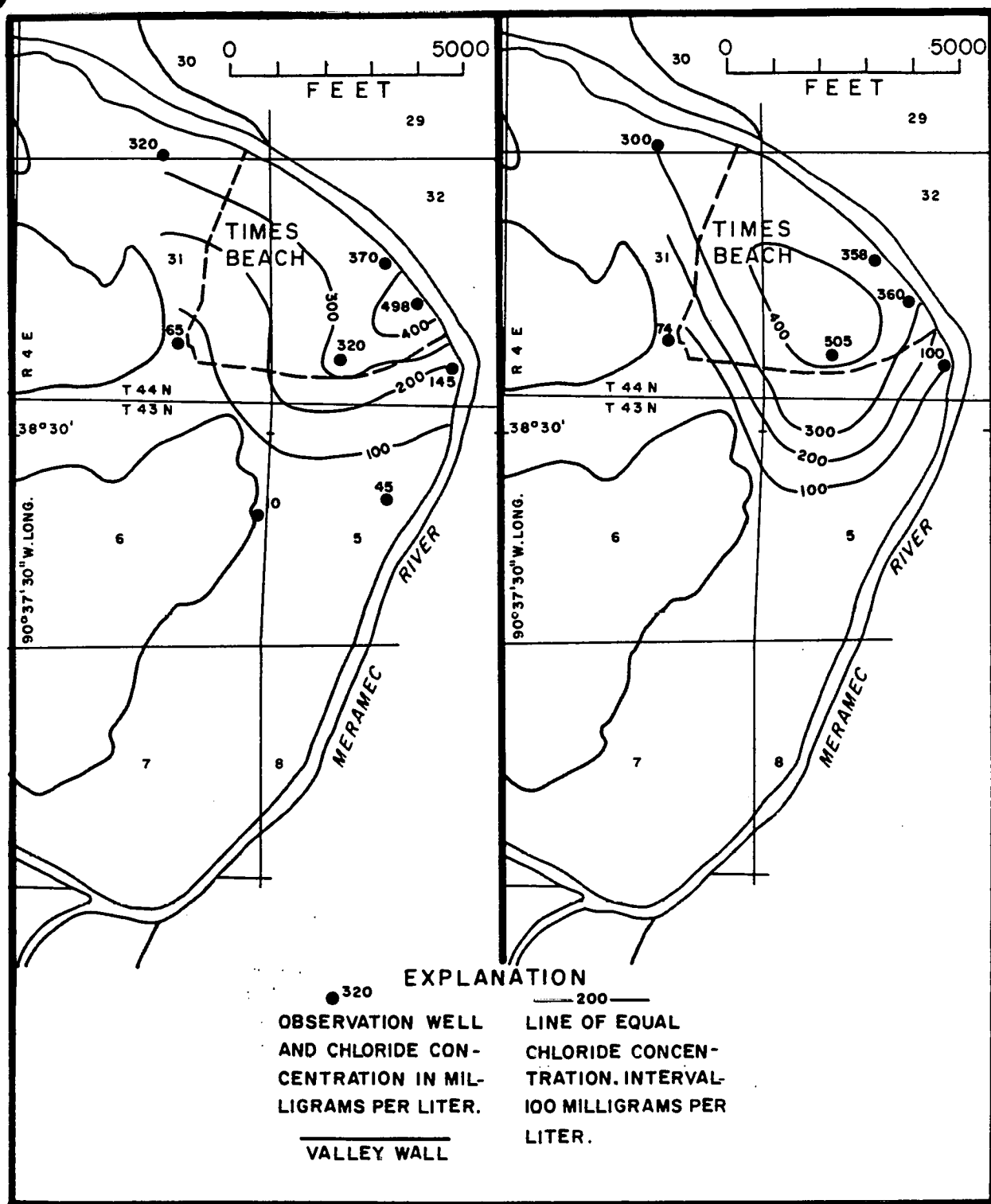


Figure 19 (continued)

Chloride distribution in alluvial deposits in the Times Beach area, October 1969.

Chloride distribution in alluvial deposits in the Times Beach area, February 1970.

Table 14

Chloride content of water from selected wells in the Times Beach area, Mo.

Date	[In milligrams per liter]					
	Well Number					
	44-4-30dcc	44-4-31dca	44-4-32bdd	44-4-32cdb	44-4-32ddb	44-4-32ddc
7-17-69	335	71	---	131	493	---
8-25-69	310	72	413	130	590	323
9-24-69	309	72	395	230	555	220
10-22-69	320	65	370	320	498	145
11-19-69	320	70	380	425	430	132
12-16-69	295	70	355	465	408	115
1-29-70	304	78	352	485	362	110
2-27-70	300	74	358	505	360	100
3-27-70	340	76	336	476	362	91
4-30-70	345	66	344	298	324	83
5-19-70	340	56	360	210	282	118
6-25-70	310	70	370	172	300	148
8-28-70	288	62	412	228	412	168
10-2-70	308	58	388	153	418	102
12-1-70	298	78	442	212	458	102
2-1-71	278	72	418	412	468	112
3-4-71	318	71	442	362	428	92
4-5-71	312	61	428	232	448	105
5-3-71	278	71	408	318	482	101
6-2-71	288	61	412	268	458	97

basin where flow is mostly from direct runoff whereas a curve with flat slope denotes a basin with large surface or groundwater storage.

The curves of figure 20 are indicative of the two types of tributary streams found in the three-county area. The Cuivre River curve represents a highly variable stream which derives much of its flow from direct runoff. This curve is characteristic of all curves plotted for small tributary streams in St. Charles, St. Louis and northern Jefferson Counties. The Big River curve is characteristic of the large

tributary streams and the small, but well-sustained streams in southern Jefferson County.

The flow-duration data presented in table 15 may be considered representative of the future distribution of flows at the gaging sites, provided there are no significant future man-made developments. In many basins in the St. Louis area, developments are already planned that will completely alter the duration data presented in this report. However, these data may be valuable as a reconnaissance tool to locate areas that are desirable for future developments.

FLOODS

Major floods have occurred during all months in the St. Louis area, but are most common in the spring and summer. While heavy general spring rains cause most of the floods, some of the greatest

floods on record have occurred in the summer (tbl. 16). This is due to intense local thunderstorms that cause flash-flood conditions on small tributary streams and consequently affect the larger streams.

A tabulation of yearly flood peaks for streams in the three-county area indicates the following flood distribution pattern:

Size of Stream	Months when floods are most likely
Thousands of square miles (for example: Mississippi and Missouri Rivers)	April through July
Hundreds of square miles (for example: Big and Cuivre Rivers)	March through May
Less than 100 square miles (for example: Platin Creek, Murphy Branch)	May and June

Detailed flood data (such as flood profiles) for specific streams are not shown in this report. These

data have been previously published and are available from the following sources:

1. Flood inundation maps and flood profiles are available in publications of the U.S. Corps of Engineers (1964, 1965, 1966) for the following streams in Jefferson and St. Louis Counties:

In Jefferson County — Bourne, Dry, Glaize, Heads, Joachim, Platin, Rock, Saline, and Sandy Creeks; Big, Meramec, and Mississippi Rivers.

In western St. Louis County — Meramec River, Brush and Fox Creeks in the vicinity of Pacific.

Searcy and others (1952) also presented selected flood profiles for the Mississippi, Missouri, and Meramec Rivers.

Table 15
Flow-duration data for
continuous-record stations on tributary streams

[Numbers refer to stations as shown on map, Fig. 2]

Percentage of time during period of record	Flow, in cfs, which was exceeded for indicated percentage of time			
	Cuivre River near Troy (No. 1)	Big River near De Soto (No. 42)	Big River at Byrnesville (No. 50)	Meramec River near Eureka (No. 52)
99.5	0.2	39	51	265
99	.3	44	59	290
98	.9	52	67	330
95	2.3	65	84	405
90	5.0	82	106	490
80	13	111	145	640
70	25	145	188	800
60	45	182	240	1,000
50	78	235	312	1,300
40	130	305	425	1,700
30	235	425	598	2,400
20	460	640	900	3,650
10	1,760	1,180	1,650	6,700
5	2,530	2,050	2,950	11,500
2	5,880	4,500	5,980	20,000
1	9,100	6,900	9,630	28,000
0.1	21,000	16,000	18,000	55,000

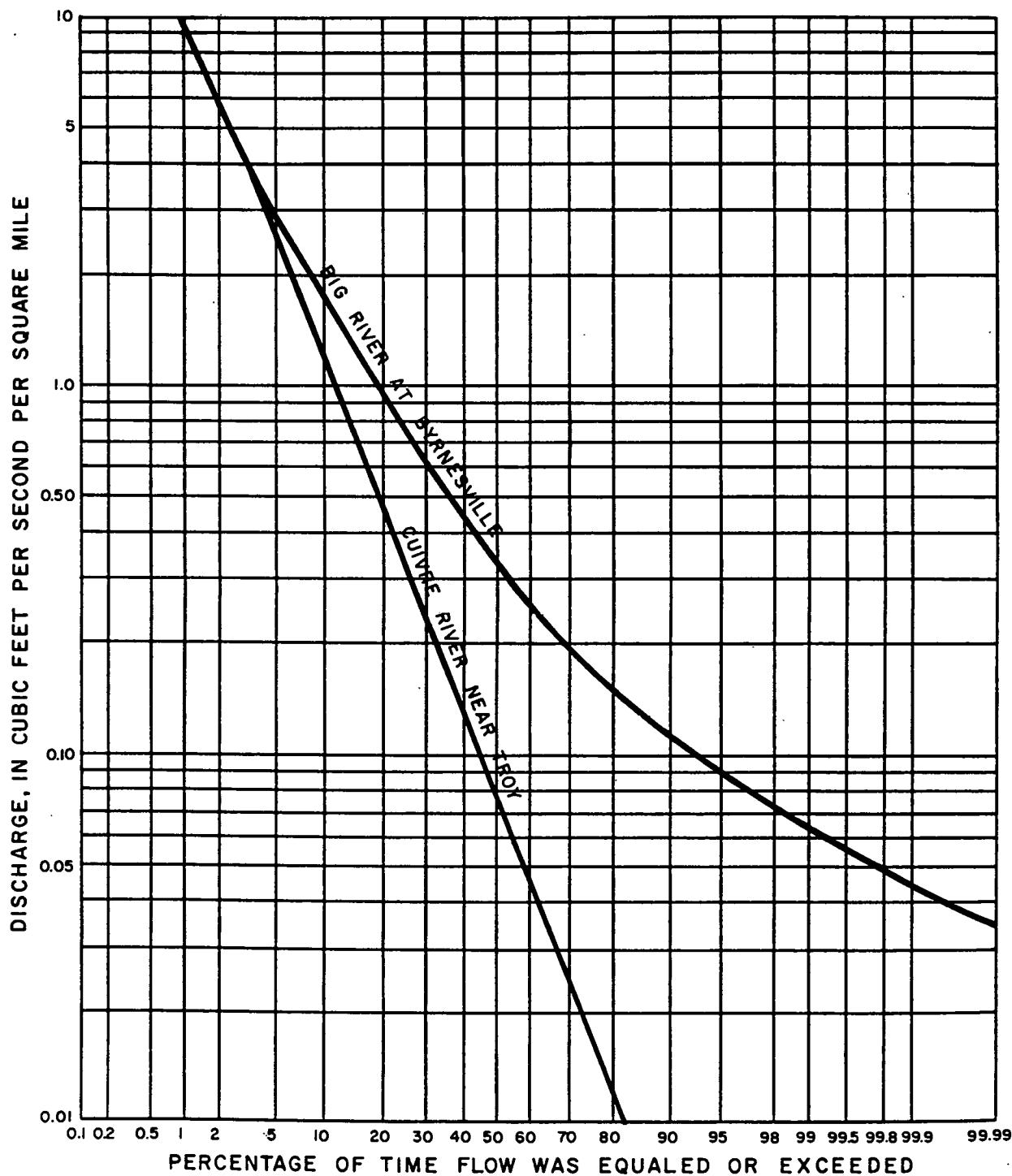


Figure 20
Duration curves of Big and Cuivre Rivers are indicative of the differences
in flow characteristics of tributary streams in the region.

2. The outstanding Jefferson County flood of June 1964 has been documented in a report by Peterson (1965). Flood-frequency and profile data are presented for Platin and Isle du Bois Creeks.

3. The estimated 100-year flood stages for the Mississippi and Missouri Rivers have been delineated for St. Louis and St. Charles Counties on 7½-minute topographic maps which are available from the District Chief, U.S. Geological Survey, P.O. Box 340, Rolla, Mo., 65401. Indirect flood-peak determinations on Gravois, Fox, and Sandy Creeks in St. Louis and

Jefferson Counties, plus peak-stage data on a number of small Jefferson County streams, are also available from this source.

4. The U.S. Geological Survey, in cooperation with the Metropolitan St. Louis Sewer District, is conducting a study of flood characteristics in five small drainage basins in the metropolitan area. Reports on several of the basins, showing stage and inundation data are now available (Spencer and Hauth, 1968; Hauth and Spencer, 1969, 1971; Spencer, 1971).

MAGNITUDE AND FREQUENCY OF FLOODS

The proper design and location of drainage structures and water facilities depend to some degree on information about the magnitude and frequency of flooding. These data are also important in floodplain zoning and other related activities. In the St. Louis area, flood problems will probably become

more severe on the tributary streams as industrial and domestic development on the floodplains becomes more intense.

The basic tool used in the analysis of floods for this report is the gaging-station flood-frequency

Table 16

Summary of maximum recorded floods and stages

Map No. (Fig. 2)	Station name	Drainage area (sq mi)	Date of maximum discharge	Maximum gage height ^{1/} (ft above mean sea level)	Discharge (cfs)
1	Cuivre River near Troy	903	Oct. 5, 1941	483.7	120,000
18	Mississippi River at Alton	171,500	Apr. 29, 1973	432.1	535,000
[Outside study area]	Missouri River at Hermann ^{2/}	528,200	Jun. 1844	517.0	892,000
34	Mississippi River at St. Louis	701,000	Jun. 27, 1844	423.17	1,300,000
42	Big River near De Soto	718	Aug. 1915	568.2	70,500
50	Big River at Byrnesville	917	Aug. 1915	463.9	80,000
52	Meramec River near Eureka	3,788	Aug. 22, 1915	446.4	175,000
77	Platin Creek near Crystal City	83.4	Jun. 17, 1964	<u>3/</u> 24.06	30,100
80	Isle du Bois Creek near Ste. Genevieve	16.4	Jun. 17, 1964	<u>3/</u> 31.08	28,400

^{1/} Did not necessarily occur at same time as maximum discharge.

^{2/} Inflow between Hermann and the mouth of the Missouri River is insignificant.

^{3/} Arbitrary datum.

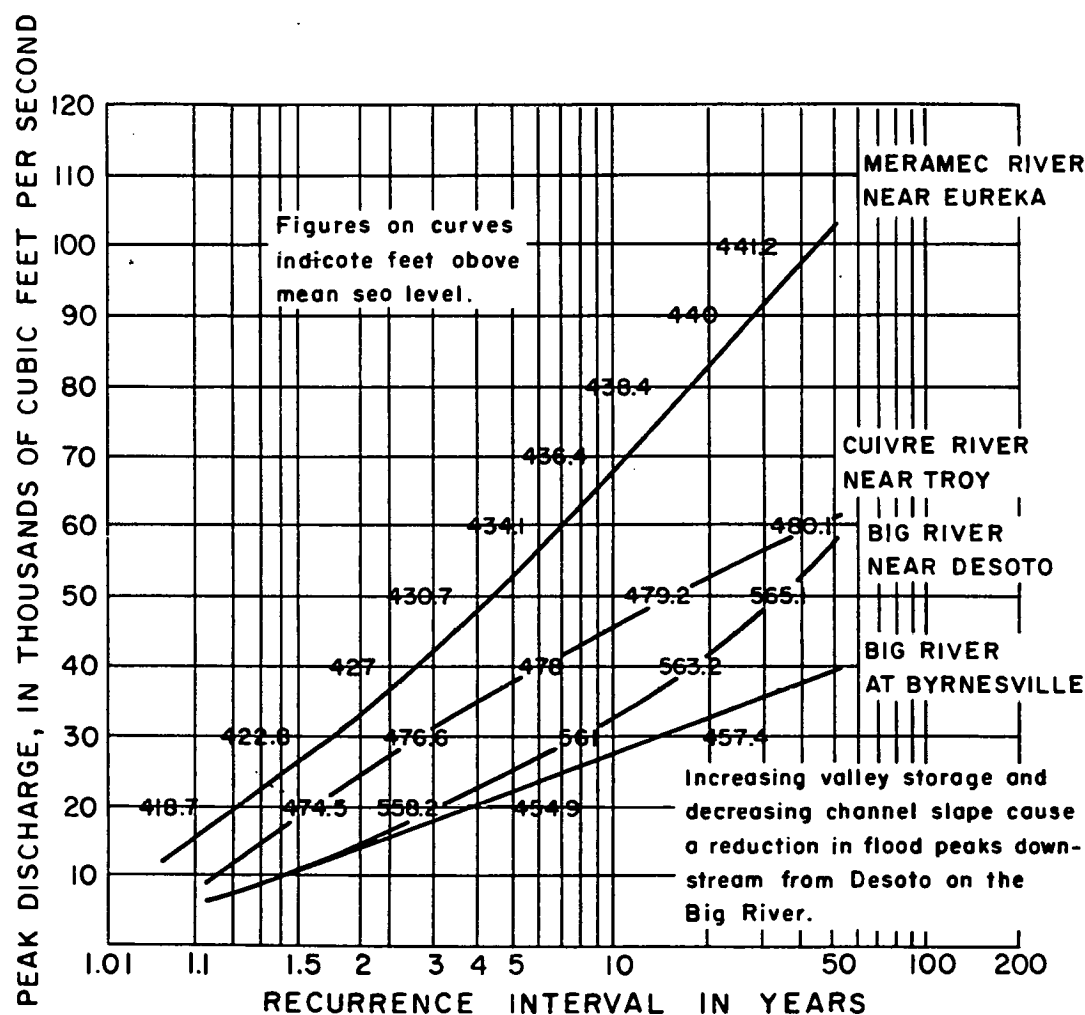


Figure 21

Flood-frequency curves for tributary streams in the St. Louis area.

curve. Examples of these curves for some of the large tributary streams in the St. Louis area are shown in figure 21. Flood-peak discharges at selected recurrence intervals from the station flood-frequency curves are shown in table 17 for selected stations. All flood-frequency curves were prepared using methods described by the U.S. Water Resources Council (1967).

Skelton and Homyk (1970) presented flood-frequency equations applicable to ungaged rural

basins in each of Missouri's physiographic regions. Data used in computation of the equations are derived from the gaging-station frequency curves and represent an average of the flood experiences for different-size drainage areas in the region.

An analysis of residual errors (actual values divided by computed values) was made to determine the usefulness of the equations in the St. Louis area. Residuals were computed and plotted on maps to determine if any geographic patterns existed in the

Table 17

Flood-frequency data at selected continuous and partial-record stations

Map No. (Figure 2)	Station name	Record used in analysis	Drainage area (sq mi)	Flood frequency				
				Magnitude of flood, in cfs, for indicated recurrence interval, in years				
				2	5	10	25	50
1	Cuivre River near Troy	1924-69	903	23,700	38,300	46,900	56,200	62,100
18	Mississippi River at Alton ^{1/}	1927-69	171,500	245,000	320,000	375,000	445,000	495,000
--	Missouri River at Hermann ^{1/}	1929-69	528,200	250,000	390,000	490,000	620,000	720,000
32	Coldwater Creek near St. Louis ^{2/}	1960-61, 1963-65, 1968-69	43.6	3,100	4,600	6,000	8,200	-----
34	Mississippi River at St. Louis ^{1/}	1928-69	701,000	480,000	700,000	800,000	895,000	940,000
42	Big River near De Soto	1950-69	718	15,500	24,900	33,100	45,800	57,400
50	Big River at Byrnesville	1923-69	917	14,600	22,400	27,800	34,900	40,400
52	Meramec River near Eureka	1922-69	3,788	34,000	55,000	69,600	88,700	103,000
78	Murphy Branch near Crystal City	1955-68	0.44	135	280	430	720	-----

^{1/} See Appendix 3 for low-flow, flood-volume, and flow-duration data.^{2/} Stream is significantly affected by urbanization.

study area. The resulting plots showed a random distribution pattern, and the equations are thus considered valid in the St. Louis area.

The grouping of the equations according to size of upstream drainage area and physiographic region was found to be the most meaningful method of presenting the data for two reasons: (a) the considerable variation in risks among regions and drainage-area sizes (as shown by the standard error of estimate) can be better defined and, (b) the effective independent variables remaining in the final regression equations are indicative of basin characteristics most significant in each region for each drainage-area class.

There are two limitations that must be considered before using the equations. First, appropriate adjustments to the equations must be made to account for increased storm runoff during and after urbanization (see the following section, "Effects of Urbanization on Storm Runoff" for a discussion of these adjustments). Secondly, the equations are based on data from rural Missouri streams and thus do not apply to the Mississippi and Missouri Rivers.

Tables 18 and 19 present the flood-frequency equations which are applicable to rural basins in the Dissected Till Plains and Ozarks portions of the

study area (fig. 1). In the case of streams that cross the Ozarks-Plains boundary, a weighted average (based on drainage area) of results from both Plains and Ozarks equations should be used.

Drainage basin characteristics are defined for the equations as follows:

1. Drainage area, A, in square miles, was determined from most recent U.S. Geological Survey topographic maps.

2. Main-channel slope, S, in feet per mile, was determined from altitudes at points 10 percent and 85 percent of the distance along the channel from the gaging station to the divide. This index was described and used by Benson (1962, 1964).

3. Mean basin altitude, E, in feet above mean sea level, was measured on 1:62,500- and 1:24,000-scale U.S. Geological Survey topographic maps for small drainage basins and on 1:250,000-scale Army Map Service maps for large basins. The altitude was computed by laying a grid over the map, determining the altitude at each grid intersection, and averaging these altitudes. The grid spacing was selected to give at least 20 intersections within the basin boundary.

4. The maximum 24-hour rainfall, $I_{24,2}$, in inches, having a recurrence interval of 2 years (2-year 24-hour rainfall) was determined for each basin from

Table 18

Flood-frequency equations applicable to rural Dissected Till Plains basins

$$\text{Model is } Y = aA^{b_1}S^{b_2}(Ex10^{-3})^{b_3}I_{24,2}^{b_4}S_i^{b_5}R^{b_6}$$

Flow characteristic, Y	Regression constant, a	Exponents of basin characteristics						Standard error of estimate (percent)
		b ₁	b ₂	b ₃	b ₄	b ₅	b ₆	
		Drainage area, A (sq mi)	Main-channel slope, S (ft per mi)	Mean basin altitude E (ftx10 ⁻³)	2-year, 24-hour rainfall, I _{24,2} (inches) ^{1/}	Soils index, S _i (inches)	Mean annual runoff, R (inches)	
2-year peak ₂ /	728	0.64	----	----	----	-0.93	----	38
2-year peak ₃ /	24.6	0.80	0.61	----	----	----	----	28
5-year peak ₂ /	1,540	0.64	----	1.29	----	-0.85	----	33
5-year peak ₃ /	0.20	0.83	0.87	----	4.69	-1.03	----	29
10-year peak ₂ /	1,890	0.65	----	1.52	----	-0.74	----	35
10-year peak ₃ /	0.19	0.81	0.83	----	5.09	-1.07	----	34
25-year peak ₂ /	1,220	0.66	----	1.34	----	----	----	40
25-year peak ₃ /	0.20	0.76	0.73	----	5.62	-1.13	----	41
50-year peak ₂ /	35	1.00	0.95	2.68	----	----	----	43
50-year peak ₃ /	1.23	0.75	0.77	----	----	----	2.06	41

Table 19

Flood-frequency equations applicable to rural Ozark Plateaus basins

$$\text{Model is } Y = aA^{b_1}S^{b_2}I_{24,2}^{b_3}R^{b_4}$$

Flow Characteristic, Y	Regression constant, a	Exponents of basin characteristics				Standard error of estimate (percent)
		b ₁	b ₂	b ₃	b ₄	
		Drainage area, A (sq mi)	Main-channel slope, S (ft per mi)	2-year 24-hour rainfall, I _{24,2} (inches) ^{1/}	Mean annual runoff, R (inches)	
2-year peak ₂ /	280x10 ⁴	0.71	----	-7.16	----	57
2-year peak ₃ /	223	0.64	----	----	----	29
5-year peak ₂ /	587x10 ³	0.70	----	-5.48	----	50
5-year peak ₃ /	405	0.63	----	----	----	26
10-year peak ₂ /	288x10 ³	0.71	----	-4.69	----	50
10-year peak ₃ /	585	0.62	----	----	----	28
25-year peak ₂ /	916x10 ²	0.80	0.27	-4.44	----	50
25-year peak ₃ /	840	0.61	----	----	----	31
50-year peak ₂ /	935	0.80	----	----	----	59
50-year peak ₃ /	631	0.48	----	----	0.52	29

^{1/} For the St. Louis area, use a value of 3.5 for I_{24,2}.^{2/} Use this equation for drainage areas of 50 square miles or less.^{3/} Use this equation for drainage areas greater than 50 square miles.

U.S. Weather Bureau Technical Paper 40 (1961).

A value of 3.5 inches can be used throughout the study area.

5. Soil infiltration index, S_i, in inches, was determined for subbasins within the state by the Soil Conservation Service (written commun., 1970).

Weighted averages of these values were used for each gaged drainage basin. Figure 23 shows the values for the St. Louis area.

6. Mean annual runoff, R , in inches, was determined from long-term gaging-station records in eastern Missouri. Figure 24 illustrates the variation in natural runoff for tributary streams in the St. Louis area.

EFFECTS OF URBANIZATION ON STORM RUNOFF

For the three-county study area, definitive ratios showing the effects of urbanization on storm runoff will be available within three years as a result of current urban-hydrology studies in cooperation with the St. Louis Metropolitan Sewer District and St. Louis County. Presently, however, there are

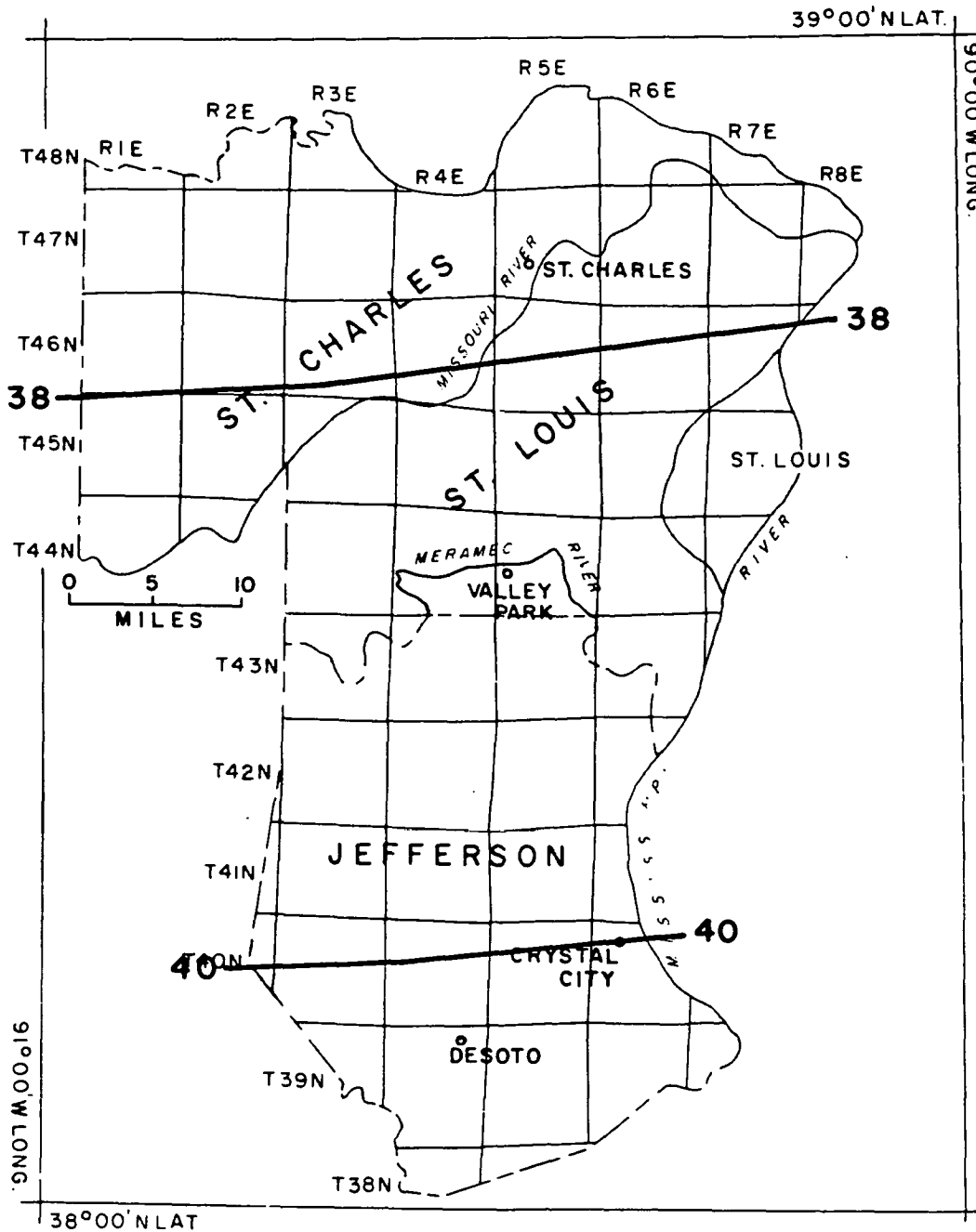


Figure 22

Average annual precipitation, in inches, for the St. Louis area. Isohyets are based on 1931-60 data from the National Weather Service - NOAA.

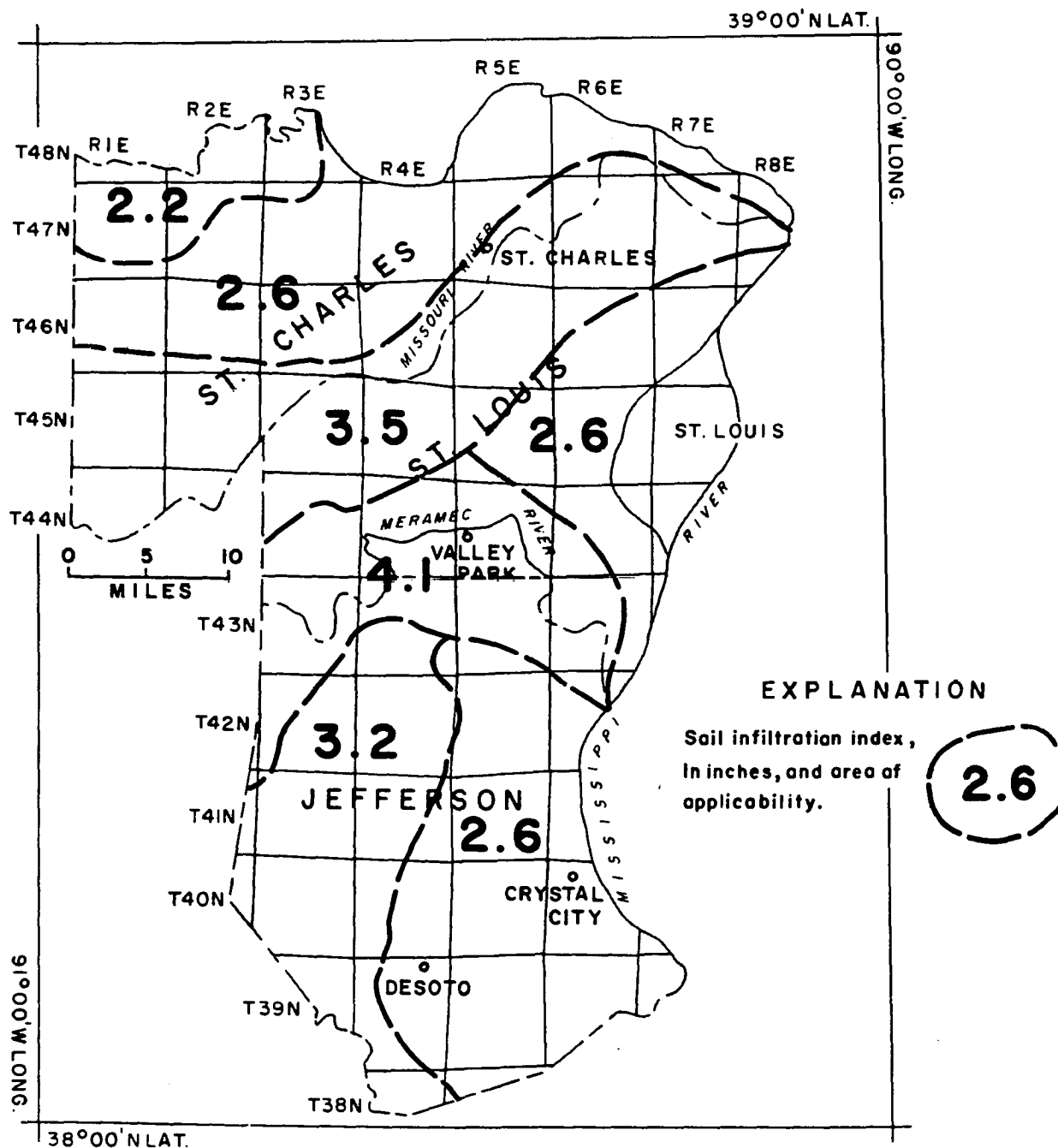


Figure 23

Soil infiltration index values, in inches, for the St. Louis area. Data furnished by the Soil Conservation Service.

inadequate hydrologic data to make precise evaluations of the effects of increasing urbanization on storm runoff.

For a generalized method of estimating increases in flood-peak discharge due to varying degrees of

urbanization in the study area, the reader is referred to Gann (1971). The methodology presented in that report will be useful to the design engineer until more comprehensive and refined data are available.

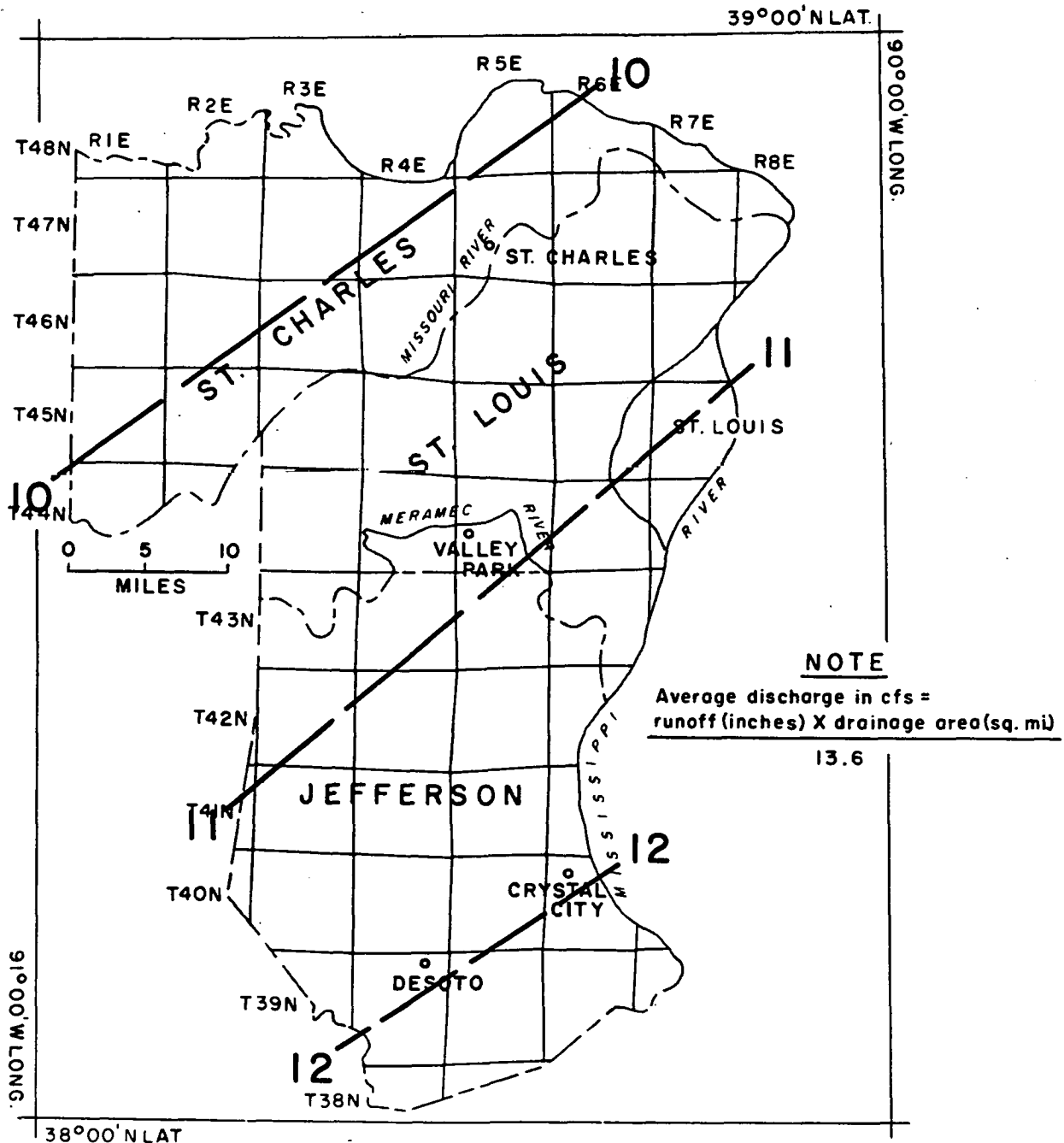


Figure 24

Mean natural annual runoff, in inches, for tributary streams in the St. Louis area.

MEAN FLOWS

The variation in mean annual runoff in the study area is shown in figure 24. The illustration is based on the results of previous runoff studies of unregulated rural basins, plus an analysis of long-term gaging-station records in the vicinity of St. Louis.

The estimation of natural mean flow for ungaged sites in the area can be made by using figure 24. The accuracy of these estimates will be sufficient for solution of the usual hydrologic problems involving mean flows; the most common of these problems is the use of the data as a parameter

in the computation of reservoir storage requirements (see subsequent section entitled "Augmentation of Dependable Flows by Storage").

EFFECTS OF URBANIZATION
ON MEAN FLOWS

In most studies in the United States, it has been observed that total runoff (amount of precipitation that appears as streamflow) is increased by urbanization. In Austin, Tex., annual runoff was increased 2.9 times in a watershed by a 21-percent-impervious cover (Espey and others, 1966). James (1965)

Table 20
Low-flow frequency data at continuous and partial-record stations

Map no. (Fig. 2)	Station name	Record used in analysis	Drainage area (sq mi)	Period (days)	Low-flow frequency				
					Annual low flow, in cfs, for indicated recurrence interval, in years				
					2	5	10	20	50
1	Cuivre River near Troy	1924-69	903	7 14 30 60 90	4.5 5.5 9.3 19 31	1.0 1.2 1.8 3.7 7.0	0.3 0.4 0.6 1.5 3.2	0.1 0.1 0.2 0.7 1.7	0 0 0.1 0.3 0.7
2	Big Creek near Moscow Mills	1962-64, 1967	----	7	0.2	----	0	----	----
7	Peruque Creek near Wentzville	1942-43, 1945-46, 1948, 1953, 1962-63, 1967	----	7	0.1	----	0	----	----
14	Dardenne Creek near Weldon Spring	1942-43, 1945-46, 1948, 1953, 1961-63, 1967	----	7	0.1	----	0	----	----
22	Femme Osage Creek near Weldon Spring	1961-63, 1967	----	7	0.2	----	0	----	----
28	Creve Coeur Creek at Creve Coeur	1961-64, 1967	----	7	0.3	----	0	----	----
31	Coldwater Creek at Shovelton ^{1/}	1961-65	----	7	10	----	5	----	----
35	Gravois Creek near Kirkwood ^{1/}	1961-65, 1967, 1969	----	7	0.2	----	0	----	----
42	Big River near De Soto	1950-69	718	7 14 30 60 90	88 100 115 125 155	50 58 68 76 95	35 42 48 55 70	27 30 35 41 52	----
43	Big River near Richwoods	1942-43, 1946-47, 1951, 1961-65, 1969	----	7	89	----	44	----	----
50	Big River at Byrnesville	1923-69	917	7 14 30 60 90	96 110 120 140 170	62 68 80 95 110	50 53 64 74 88	41 44 50 58 70	32 34 37 44 50
52	Meramec River near Eureka	1922-69	3,788	7 14 30 60 90	420 450 500 590 680	310 330 360 405 480	280 300 320 350 410	230 250 290 340 380	190 215 230 260 290
67	Joachim Creek at Hematite	1961-65, 1967-69	95.0	7	2.5	----	0.8	----	----
73	Sandy Creek near Pevely	1966-68	32.5	7	0	----	0	----	----
76	Plattin Creek at Plattin	1966-69	65.8	7	2.9	----	0.3	----	----

^{1/} Stream is significantly affected by urbanization. Natural low flows augmented by outflow from sewage disposal plants and lagoons. Low-flow estimates cannot be regarded as probability data, but are useful for comparative purposes.

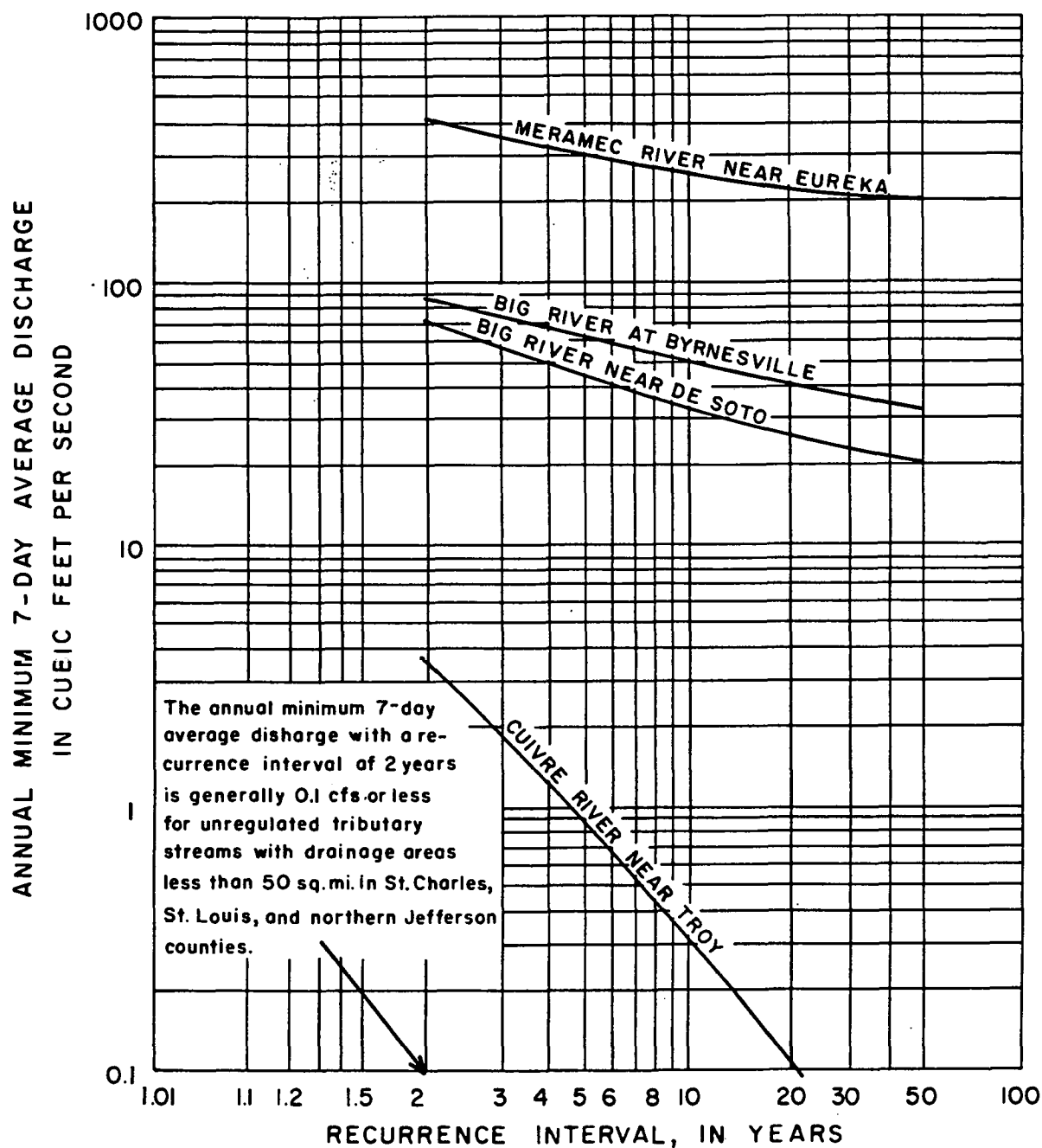


Figure 25

Low-flow frequency curves for tributary streams in the St. Louis area.

estimated that the annual runoff from a completely urbanized California stream basin was 2.3 times its natural volume. Crippen and Waananen (1969) showed that, during years of normal precipitation, the increase in annual runoff from partial urbanization

of a small California basin was about threefold. These results are logical because one of the primary controls on runoff is the basin infiltration characteristics, and these are directly related to the percentage of impervious area in a basin.

Streamflow records on Coldwater Creek (about 60-percent urbanized with an estimated 20 percent of the urbanized area impervious) represent the only runoff data of any consequence collected on an urbanized basin in the St. Louis area. These data, when adjusted for record length on the basis of nearby long-time streamflow records, indicate that the average annual runoff from the basin is about 22 inches. This is approximately twice the average for rural basins in the area (see fig. 24). A part of this increase is due to the operation of sewage treatment plants in the basin. Crippen and Waananen (1969) stated that *"Development . . . has produced a marked increase in the total runoff. Such an increase has been noted in other studies, and is probably more*

pronounced in the semi-arid California climate than in more humid regions."

Based on the studies in California and Texas, plus the data from Coldwater Creek, it is recommended that the mean flow of streams in the study area, with urban development similar to that of Coldwater Creek, be adjusted for urbanization effects by multiplying the natural runoff chosen from figure 24 by 1.5. If treatment plants are present in the basin, the mean flow could be twice as high as that shown on figure 24. Until more comprehensive urban runoff data are available, recommendations cannot be made for adjusting data from basins with varying degrees of urbanization.

LOW FLOWS

The utilization or development of a stream depends, to some extent, on its low-flow characteristics as defined by low-flow frequency data (table 20). These data are the principal tool used by hydrologists and planners to evaluate the low-flow potential of streams.

For this report, low-flow frequency data were computed by statistical methods described by Skelton (1966). Examples of low-flow frequency curves (fig. 25) are presented to indicate the variations in low-flow characteristics of some major tributary streams in the region. The Meramec and Big River curves represent streams with high, well-sustained base flows, while the Cuivre River curve indicates that this stream has a highly variable low flow that can diminish rapidly during a severe drought.

Data from low-flow partial-record stations and continuous-record stations with less than five annual minima are inadequate to define a low-flow frequency curve. These data were related to long-term gaging-station data in the area, and the resulting graphical regression was used to estimate the median annual minimum 7-day flows (7-day Q_2) and the 7-day 10-year-recurrence-interval flows shown in table 20.

Estimates of low-flow characteristics at ungaged sites in the area can be made by using a method described by Skelton (1970). Briefly, the method involves measuring low flow at the site on different recessions in several different years and graphically

relating these measurements to concurrent flows at a nearby continuous-record station. In general, the results obtained from these regressions will give reliable estimates of median values (7-day Q_2) and less reliable estimates of more extreme events.

As shown in figure 26 and table 20, there is considerable variation in the values of the 7-day Q_2 for unregulated streams in the area. In general, the 7-day Q_2 for small unregulated tributary streams ranges from 0 to 0.005 cfs per square mile in the northern two-thirds of the area and from 0.02 to 0.05 cfs per square mile in the southern third of Jefferson County. The 7-day Q_2 for the Meramec and Big River basins is a relatively high 0.1 cfs per square mile. However, data from Coldwater Creek basin indicate that median low flows can be as great as 0.3 cfs per square mile in basins where sewage treatment plants are operating, depending on plant size, water-table condition, etc.

During 1967 and 1970, hydrologic data were collected on many of the tributary streams in the three-county area to determine low-flow gains or losses and to observe the impact of various urban developments on basin environment. Table 21 presents the results of discharge and specific-conductance measurements at various sites, plus observations of the streams' appearances and other information. The reconnaissance data from 1967 is especially useful because it was made during a period of

median low-flow conditions (7-day Q_2) over most of the area. Thus the data in the table can be a valuable guide concerning actual quantities of water available

in many of the area's small surface streams during a specific drought. Water-quality information collected during these investigations is presented in appendix 4.

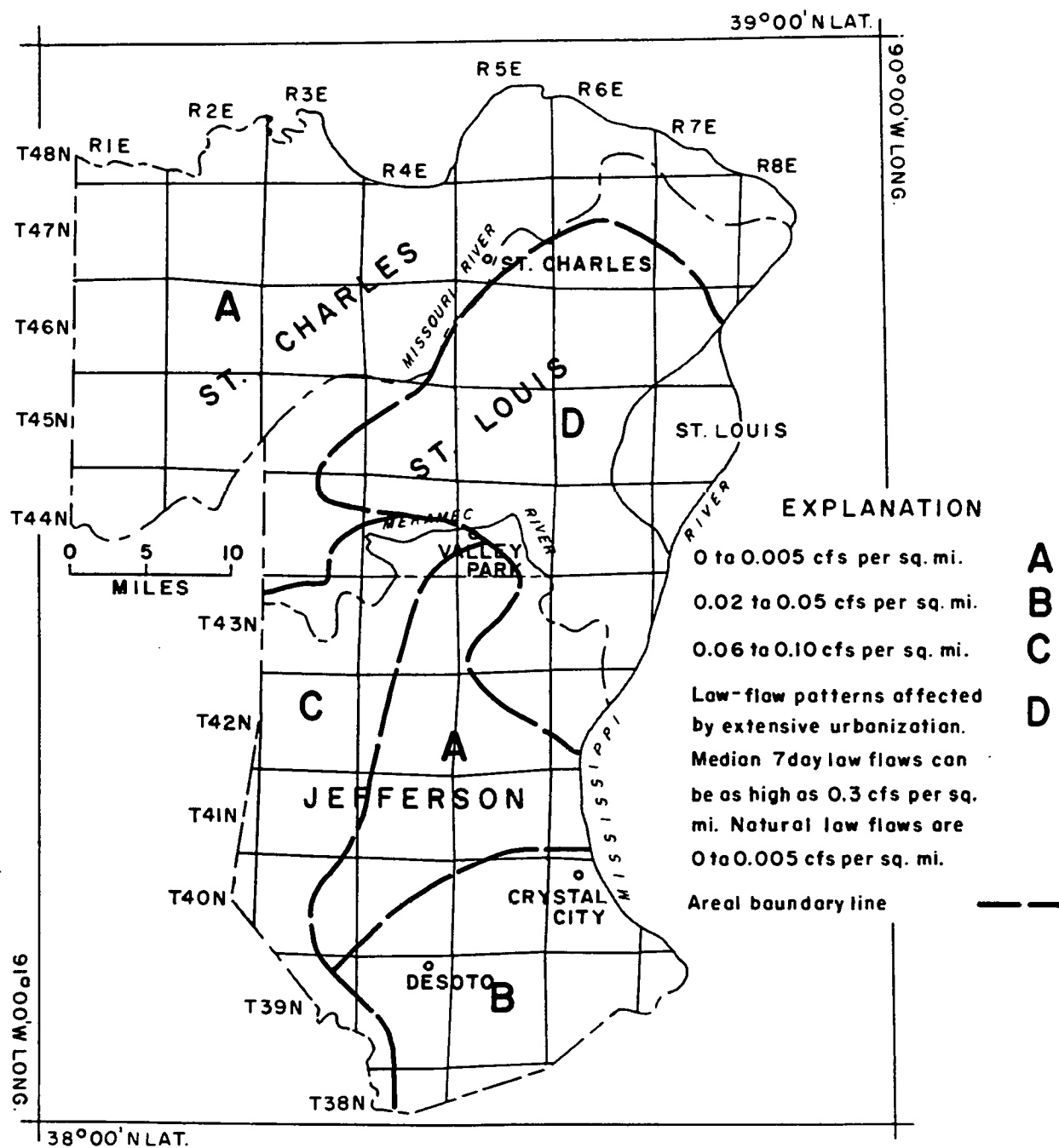


Figure 26

*Generalized patterns of median 7-day low-flow values for tributary streams.
Recurrence interval of these data is 2 years.*

The specific conductance readings and descriptions of stream appearance in table 21 can be used to identify many of the streams in the area that are affected by urbanization and have low flows of inferior-quality water. For instance, the conductance of Bonhomme Creek at Chesterfield (fig. 2, map no. 26) was 500 micromhos and the water was described as very murky, with foam on the surface. Streamflow in undeveloped parts of the region was clear at the time and natural conductances were 400 micromhos or less; thus Bonhomme Creek was evidently affected by man's activities.

EFFECTS OF URBANIZATION ON LOW FLOWS

Theoretically, urbanization will decrease the low flows of streams because of decreased soil-moisture storage, improvement of drainage, and

lowering of groundwater levels (Ringensoldus and Bauer, written commun., 1966). James (1965) made a model analysis of a California streamflow record and found that the low flow of a completely urbanized basin is about 0.7 of the natural value.

In the St. Louis area, however, low flows of many small tributary streams having drainage areas of less than 50 square miles are greatly augmented, mostly by domestic effluents (figure 26, area D), and the net result is an increase in dry-weather flow. The natural low flow of most of these streams is less than 0.5 cfs (except in middle and southern Jefferson County). Consequently, an influx of poor-quality effluent, even though in small amounts, can seriously degrade the flow of an entire stream. Studies by Lutzen of the Missouri Geological Survey and Water Resources (written commun., 1970) in the Grand Glaize, Fishpot and Romaine Creek basins, point out specific examples of these effects.

AUGMENTATION OF DEPENDABLE FLOWS BY STORAGE

In the tributary basins of the three-county study area, a lack of streams with natural sustained low flows makes it necessary to consider storage reservoirs when year-round surface-water supplies are required. The impoundments will generally serve a number of purposes such as recreation, low-flow augmentation and flood control. One of the more pressing problems involved in utilizing reservoirs in these developing areas, aside from the high cost of acquiring land, will be the pollution aspect of urban runoff during storms. It has been shown by Sheaffer and Zeisel (1966, p. 73) that the quality of initial storm runoff for some streams in urban areas is inferior to that of domestic sewage. Storage of this water would not only result in excessive treatment costs when the water is utilized, but would cause a generally unpleasant reservoir environment. Spieker (1970) stated that pollution loads may remain high in sluggish streams after several days of flooding because of accumulated sludge on the stream bottom and release of untreated sewage into the stream. Further analytical studies and continued management programs may be necessary in order to properly maintain these urban reservoirs.

For water managers and planners, there are some major points concerning impoundment of low flows in the St. Louis area that should be considered:

1. In almost all of the area, except for the larger tributary streams such as the Meramec, Big, and Cuivre Rivers, storage facilities are required to insure a dependable surface-water supply.
2. In urbanized areas of small natural flows, the quantity of low-flow may be adequate for some uses because of augmentation from treatment plants, sewers and septic tanks, but the quality of the water is very poor and thus extensive treatment is required prior to use.
3. Several miles of the lower reaches of many tributary streams are affected by backwater from the Mississippi and Missouri Rivers. In these ponded areas, water can be pumped directly from the streams with no need for impoundments to insure an adequate water level. The most important consideration in these reaches is, of course, the quality of the water, which may make it unsuitable for use without extensive treatment.

Table 21
Results of hydrologic reconnaissance on tributary streams

Map no. (Fig. 2)	Station name	Location	Date	Discharge ^a (cfs)	Conductance (micromhos @ 25°C)	Dissolved oxygen (mg/l)	Water temper- ature (°C)	Air temper- ature (°C)	Remarks
2	Big Creek near Moscow Mills	T. 48 N., R. 1 E., at bridge on U.S. Highway 61 at Lincoln-St. Charles County line, 4 miles south of Moscow Mills.	9-12-67	0.2	500	9.5	21	27	-
3	Cuivre River near Wentzville	T. 48 N., R. 2 E., 400 feet downstream from mouth of Big Creek, 4 miles north- east of Wentzville, Lincoln- St. Charles County line.	9-12-67	Pooled	460	7.5	21	31	Appears to be oil slick on water surface below mouth of Big Creek; muddy above.
4	Cuivre River near Old Monroe	NE 1/4 sec. 21, T. 48 N., R. 2 E., at fishing camp 3 miles southwest of Old Monroe, Lincoln-St. Charles County line.	9-12-67	Pooled	-	-	-	-	-
5	Cuivre River at Old Monroe	T. 48 N., R. 2 E., at bridge on State Highway 79 at Old Monroe, Lincoln-St. Charles County line.	9-12-67	Pooled	-	-	-	-	-
6	Peruque Creek at Fortistell	SE 1/4 sec. 29, T. 47 N., R. 1 E., at bridge on County Highway T, 0.5 mile south of Fortistell, St. Charles County.	9-13-67 11-4-70	0 4.4	- 460	- 10.5	- 7.0	- 4.0	Scattered shallow pools in channel.
7	Peruque Creek near Wentzville	SW 1/4 sec. 32, T. 47 N., R. 2 E., at bridge on county road 2 miles southeast of Wentzville, St. Charles County.	9-13-67 11-4-70	0 14.4	- 450	- 10.5	- 7.5	- 4.0	Shallow (less than 0.5 ft deep) pools with no flow. Scum on water surface below bridge.
8	Peruque Creek near Wentzville	SE 1/4 sec. 33, T. 47 N., R. 2 E., at bridge on U.S. Highway 61, 2.5 miles south- east of Wentzville, St. Charles County.	9-12-67	0	-	-	-	-	Pooled in vicinity of bridge. No discernible flow.
9	Peruque Creek near O'Fallon	SW 1/4 sec. 13, T. 47 N., R. 2 E., at bridge on County highway 3 miles west of O'Fallon, St. Charles County.	9-12-67	0	-	-	-	-	Shallow pools with no flow. Oil film on water upstream from bridge.
10	Peruque Creek at O'Fallon	T. 47 N., R. 3 E., at bridge on State Highway 79, one mile northeast of O'Fallon, St. Charles County.	9-12-67 11-4-70	0 11.9	- 480	- 9.3	- 7.0	- 8.0	Pooled; no discernible flow.
11	Dardenne Creek near New Melle	NE 1/4 sec. 23, T. 46 N., R. 1 E., at bridge on County Highway 2, 2 miles north of New Melle, St. Charles County.	9-13-67	Trickle (<0.05)	-	-	-	-	Mostly scattered pools. Large piles of crushed lime on right bank below bridge.
12	Little Dardenne Creek near New Melle	SW 1/4 sec. 12, T. 46 N., R. 1 E., at bridge on County Highway 2, 4 miles north of New Melle, St. Charles County.	9-13-67	0	-	-	-	-	-
13	Dardenne Creek near New Melle	NE 1/4 sec. 21, T. 46 N., R. 2 E., at bridge on County Highway 2D, 5 miles northeast of New Melle, St. Charles County.	9-13-67 11-3-70	0.1 16.5	- 360	- 10	- 9.0	- 6.0	-
14	Dardenne Creek near Weldon Spring	T. 46 N., R. 3 E., at bridge on U.S. Highway 40 and 61, 3 miles north- west of Weldon Spring, St. Charles County.	9-12-67	0.2	400	7.5	19	-	Water clear
15	Dardenne Creek near Weldon Spring	SW 1/4 sec. 16, T. 46 N., R. 3 E., at bridge on County Highway K, 2 miles north of Weldon Spring, St. Charles County.	9-12-67 11-3-70	0.2 36.9	400 340	7.5 10.3	19 9.0	- 6.0	-
16	Dardenne Creek at St. Peters	T. 47 N., R. 3 E., at bridge on County Highway C at St. Peters, St. Charles County.	9-12-67	0	-	-	-	-	Shallow pools with no flow.
19	Femme Osage Creek near Femme Osage	T. 45 N., R. 1 E., at bridge on county road 2 miles northeast of Femme Osage, St. Charles County.	9-13-67	0	370 (in pool)	6.5 (in pool)	20 (in pool)	25 (in pool)	Creek bed mostly dry but scattered pools contain small fish. The area is consider- ably more rugged from New Melle to this point than in other areas of the county, but the surface flow characteristics remain the same.

Table 21

Results of hydrologic reconnaissance on tributary streams--continued

Map no. (Fig. 2)	Station name	Location	Date	Discharge ^a (cfs)	Conductance (microhms @ 25°C)	Dissolved oxygen (mg/l)	Water temper- ature (°C)	Air temper- ature (°C)	Remarks
20	Callaway Fork near New Melle	SE¼ sec. 34, T. 46 N., R. 1 E., at bridge on County Highway F, 1.5 miles southwest of New Melle, St. Charles County.	9-13-67	0	-	-	-	-	-
21	Callaway Fork near Defiance	T. 45 N., R. 2 E., at bridge on County Highway F, 1.5 miles northwest of Defiance, St. Charles County.	9-13-67	0.3	490	7.5	19	25	Ninety-five percent of the flow originates in a small drain entering the creek 50 feet below a ford on county road in SW¼ sec. 16, T. 45 N., R. 2 E. Drain is choked with watercress with water temperature of 15°C and conductance of 490.
22	Femme Osage Creek near Weldon Spring	T. 45 N., R. 2 E., at bridge on State Highway 94, one mile north of Defiance and 7 miles southwest of Weldon Spring, St. Charles County.	9-13-67	0.6	490	9	20	26	-
23	Wild Horse Creek near Centaur	T. 45 N., R. 3 E., at bridge on Wildhorse Creek Road, 1 mile southwest of Centaur, St. Louis County.	9-13-67	Trickle (<0.05)	440	5	21	28	Water clear
24	Bonhomme Creek near Chesterfield	T. 45 N., R. 4 E., at bridge on County Highway CC, 2 miles west of Chesterfield, St. Louis County.	9-13-67	Trickle (<0.01)	-	-	-	-	Isolated pools, virtually no flow.
25	Caulks Creek near Chesterfield	T. 45 N., R. 4 E., at bridge on County Highway CC, 1.5 miles southwest of Chesterfield, St. Louis County.	9-13-67	1.4 (origin of Bonhomme Creek flow)	530	8	18	25	Small spring (0.1 cfs) 50 feet upstream from bridge has temperature of 11°C and conductance of 600 microhms. Sewage lagoon and larger spring located in headwaters of this creek.
26	Bonhomme Creek at Chesterfield	T. 45 N., R. 4 E., at bridge on Olive St. Road at Chesterfield, St. Louis County	9-13-67	1.5	500	11	23	31	Water very murky in appearance with foam on surface.
28	Creve Coeur Creek at Creve Coeur	T. 46 N., R. 5 E., at bridge on Creve Coeur mill road 1 mile southwest of Creve Coeur, St. Louis County.	9-13-67	Trickle (<0.05)	650	-	21	-	-
29	Creve Coeur Lake at Creve Coeur	T. 46 N., R. 5 E., at Creve Coeur, St. Louis County.	9-13-67	-	500 (SE shore of lake)	-	23 (SE shore of lake)	-	Foam floating on surface. Water dirty and full of debris.
30	Peefee Creek at Creve Coeur	T. 46 N., R. 5 E., at bridge on Creve Coeur mill road at Creve Coeur, St. Louis County.	9-13-67	0.3	-	-	-	-	Outflow from Creve Coeur Lake.
37	Fox Creek near Eureka	T. 43 N., R. 3 E., at bridge on U.S. Highway 66, 1.5 miles west of Eureka, St. Louis County.	6-15-57 (indirect peak flow measure- ment) 9-13-67	1,482 0	- 500 (in pool)	- -	- 20 (in pool)	-	- Isolated large, deep, clear pools are full of minnows.
38	La Barque Creek near Byrnesville	NW¼ sec. 34, T. 43 N., R. 3 E., at bridge on County Highway F, 2.5 miles northwest of Byrnesville, Jefferson County.	9-30-53 9-15-67	0 0.5	- 340	- 8.5	- 20	-	St. Peters sandstone outcrops along the stream.
39	Tiff Creek near Valles Mines (tributary to Cole Lake)	SW¼ sec. 11, T. 38 N., R. 4 E., at culvert on county road 4 miles southwest of Valles Mines, Jefferson County.	9-15-67	0	-	-	-	-	-
40	Cole Lake near Valles Mines	SE¼ sec. 10, T. 38 N., R. 4 E., 4 miles south- west of Valles Mines, Jefferson County.	9-15-67	-	80	8 to 9.5	23	23	Samples taken.
40	Cole Lake outflow	SE¼ sec. 10, T. 38 N., R. 4 E., 4 miles south- west of Valles Mines, Jefferson County.	9-15-67	0.1	240	-	19	-	Small amounts of watercress present in channel. May be part spring and part seepage from lake.

Table 21
Results of hydrologic reconnaissance on tributary streams--continued

Map no. (Fig. 2)	Station name	Location	Date	Discharge ^a / (cfs)	Conductance (micromhos @ 25°C)	Dissolved oxygen (mg/l)	Water temper- ature (°C)	Air temper- ature (°C)	Remarks
41	Unnamed creek near Valles Mines	NE¼ sec. 10, T. 38 N., R. 4 E., at bridge on County Highway E, 3½ miles southwest of Valles Mines, Jefferson County.	9-15-67	0	-	-	-	-	-
44	Dry Creek near Ware	NW¼ sec. 14, T. 40 N., R. 3 E., at bridge on County Highway Y, 1.5 miles south of Ware, Jefferson County.	9-15-67	Trickle (<0.02)	-	-	-	-	-
45	Dry Creek near Morse Hill	NW¼ sec. 26, T. 41 N., R. 3 E., at bridge on county road 1 mile southwest of Morse Hill, Jefferson County.	9-15-67	D	-	-	-	-	-
46	Belews Creek near Hillsboro	N¼ sec. 17, T. 41 N., R. 4 E., at ford on county road, 4.5 miles northwest of Hillsboro, Jefferson County.	9-15-67	0	-	-	-	-	-
47	Inflow to Lake Tishomingo	NW¼ sec. 10 and SW¼ sec. 3, T. 41 N., R. 4 E., on county road 5.5 miles north of Hillsboro, Jefferson County.	9-15-67	0	-	-	-	-	-
48	Unnamed creek near Hillsboro	NE¼ sec. 4, T. 41 N., R. 4 E., at ford on county road 6 miles north of Hillsboro, Jefferson County.	9-15-67	D	-	-	-	-	-
49	Delews Creek tributary near Cedar Hill (outflow from Lake Tishomingo)	SW¼ sec. 31, T. 41 N., R. 4 E., at bridge on County Highway BB, 2.5 miles southeast of Cedar Hill, Jefferson County.	9-15-67	0.3	320	8	20	24	-
51	Heads Creek at House Springs	NE¼ sec. 4, T. 42 N., R. 4 E., at bridge on State Highway 30 at House Springs, Jefferson County.	9-15-67	0	-	-	-	-	Dry streambed with no pools.
53	Carr Creek at Glencoe	NE¼ sec. 24, T. 44 N., R. 3 E., at bridge on State Highway 109 at Glencoe, St. Louis County.	9-13-67	D	-	-	-	-	-
54	Keifer Creek near Ellisville	NW¼ sec. 9, T. 44 N., R. 4 E., at bridge on county road 1.5 miles south of Ellisville, St. Louis County.	9-13-67	0	-	-	-	-	-
55	Unnamed spring near Valley Park	NE¼ sec. 15, T. 44 N., R. 4 E., at bridge on county road 5 miles west of Valley Park, St. Louis County.	9-13-67	0.1	520	-	13	-	Flows into Keifer Creek.
56	Unnamed spring near Valley Park	NE¼ sec. 16, T. 44 N., R. 4 E., near county road 3.5 miles west of Valley Park, St. Louis County.	9-13-67	<0.01	490	-	14	-	Flows into Spring Branch Creek.
57	Fishpot Creek at Winchester	W¼ sec. 1, T. 44 N., R. 4 E., at bridge on county road at Win- chester, St. Louis County.	9-13-67 6-16-70	0 0.5	- 380	- -	- -	- -	- Flow disappears about 400 yards downstream. Indi- cates zone of water losses.
58	Grand Glaize Creek near Kirkwood	SE¼ sec. 4, T. 44 N., R. 5 E., at bridge on Dougherty Ferry road 1.5 miles west of Kirkwood, St. Louis County.	9-13-67 6-16-70	2.0 8.3	950 650	- -	- 25	- 34	Foam on surface, smells of sewage no fish seen.
60	Romaine Creek at Paulina Hills	E¼ sec. 14, T. 43 N., R. 5 E., at bridge on State Highway 141 at Paulina Hills, Jefferson County.	11-4-70	3.7	500	10	9.0	6.5	Black precipitant on bottom of creek. Slight sewage odor.
62-	Mattese Creek near Oakville	NE¼ sec. 15, T. 43 N., R. 6 E., at bridge on Old Baumgartner Road, 1.5 miles west of Oakville, St. Louis County.	9-14-67	2.4	750	1.5	20.5	23	Foam on surface. Affected by sewage or plant effluent.

Table 21

Results of hydrologic reconnaissance on tributary streams--continued

Map no. (Fig. 2)	Station name	Location	Date	Discharge ^a (cfs)	Conductance (micromhos @ 25°C)	Dissolved oxygen (mg/l)	Water temper- ature (°C)	Air temper- ature (°C)	Remarks
63	Rock Creek at Kimmavick	T. 42 N., R. 6 E., at bridge on county highway D.5 mile west of Kimmavick, Jefferson County.	9-14-67	0.3	390	6	20	-	-
64	Claise Creek near Kohler City	T. 42 N., R. 6 E., at bridge on county highway 1.5 miles northwest of Kohler City, Jefferson County.	9-14-67	D.8	500	9	21	-	Mud bottom with small amounts of gravel.
65	Joachim Creek at De Soto	On line between secs. 10 and 11, T. 39 N., R. 4 E., at bridge on County Highway E at De Soto, Jefferson County.	9-14-67 11-5-70	1.7 14.9	430 460	9.5 10.6	24.5 7.0	30 6.5	- -
66	Cotter Creek near Hillsboro	SE¼ sec. 22, T. 40 N., R. 4 E., at bridge on State Highway 21, 3 miles south of Hillsboro, Jefferson County.	9-14-67	0	-	-	-	-	A few scattered pools.
67	Joachim Creek at Hematite ^b	NW¼ sec. 16, T. 40 N., R. 5 E., at bridge on county highway at Hematite, Jefferson County.	9-14-67 11-5-70	5.1 20.4	340 570	8.5 8.9	23 7.5	30 7.0	Water clear. Samples taken.
68	Lake Mauwanoka near Hillsboro	In secs. 1 and 2, T. 40 N., R. 4 E., 2 miles east of Hillsboro, Jefferson County.	9-14-67	outflow at dam = 0.9	-	-	-	-	Earth-fill dam was leaking at this time. Lake was about 10 percent full. Major sources of water for this lake are several springs which merge near the dam.
69	South Fork Little Creek near Hillsboro	SE¼ sec. 1, T. 40 N., R. 5 E., at bridge on county road 2.5 miles southeast of Hillsboro, Jefferson County.	9-14-67	1.8	340	9	23	30	Water clear. This stream contains the outflow from Lake Mauwanoka.
70	North Fork Little Creek near Hillsboro	S¼ sec. 31, T. 41 N., R. 5 E., at bridge on county road 2.5 miles east of Hillsboro, Jefferson County.	9-14-67	0	-	-	-	-	-
71	Little Creek near Hematite	NE¼ sec. 5, T. 40 N., R. 5 E., at bridge on county road 2 miles north of Hematite, Jefferson County.	9-14-67	2.5	350	9.5	24	32	Water clear. Samples taken.
72	Joachim Creek near Festus	NW¼ sec. 1, T. 40 N., R. 5 E., at bridge on County Highway A, 1.5 miles west of Festus, Jefferson County.	9-15-67	7.4	500	8	20	19	-
73	Sandy Creek at Pevely ^b	T. 41 N., R. 5 E., at bridge on County Highway Z, 1 mile west of Pevely, Jefferson County.	9-14-67	0.2	550	9	21	-	Sand-bottom channel. No rock outcrops visible.
74	Joachim Creek near Pevely	T. 41 N., R. 6 E., at bridge on U.S. Highway 61, 1.5 miles south of Pevely, Jefferson County.	9-14-67	Ponded	-	-	-	-	Backwater from Mississippi River.
75	West Fork Platte Creek near Papio	NE¼ sec. 25, T. 39 N., R. 5 E., at ford on county road 3 miles east of Papio, Jefferson County.	9-14-67	2.6	450	10	22	26	Water clear.
76	Platte Creek at Platte	T. 39 N., R. 6 E., at bridge on county road at Platte, Jefferson County.	11-5-70	14.9	460	11.4	13.5	7.0	-
77	Platte Creek near Crystal City	T. 40 N., R. 6 E., at bridge on U.S. Highway 61, 3 miles south of Crystal City, Jefferson County.	9-14-67	4.9	460	9.5	21	23	Samples taken.
80	Ile du Bois Creek near Festus	T. 39 N., R. 7 E., at bridge on County Highway TT, 10 miles southeast of Festus, Jefferson County.	9-14-67	0	-	-	-	-	-

^a/ 1967 data were collected during a period of median low-flow conditions (7-day Q₂).^b/ Continuous-record station.

Table 22
Draft-storage frequency data at continuous and partial-record stations

Map no. (Fig. 2)	Station name	Record used in analysis	Drainage area (sq mi)	Draft-storage frequency					
				Percent chance of deficiency ^{a/}	Amount of storage (in thousands of acre-feet) for draft rate (in cfs) indicated in column headings (not corrected for reservoir evaporation, sedi- mentation, and seepage) ^{b/}				
1	Cuivre River near Troy	1924-69	903	2 5 10	25 cfs 15 10 6	140 cfs 140 75 65	260 cfs 290 180 170	380 cfs 540 390 320	500 cfs 1,100 870 640
2	Big Creek near Moscow Mills	1962-64, 1967	-	2 5 10	12 cfs 7 5 2	24 cfs 18 11 8	48 cfs 58 38 28	60 cfs 95 66 61	72 cfs 175 134 110
7	Peruque Creek near Wentzville	1942-43, 1945-46, 1948, 1953, 1962-63, 1967	-	2 5 10	5 cfs 3 2 1	10 cfs 7 4 3	20 cfs 22 14 12	30 cfs 64 50 40	35 cfs - - 64
14	Dardenna Creek near Weldon Spring	1942-43, 1945-46, 1948, 1953, 1961-63, 1967	-	2 5 10	5 cfs 3 2 1	10 cfs 7 4 3	20 cfs 22 14 12	30 cfs 64 50 40	35 cfs - - 64
22	Fenne Osage Creek near Weldon Spring	1961-63, 1967	-	2 5 10	6 cfs 4 3 1	18 cfs 14 8 7	24 cfs 26 17 12	36 cfs 71 57 44	42 cfs - 91 72
42	Big River near De Soto	1950-69	718	2 5 10	195 cfs 70 45 35	300 cfs 260 180 120	390 cfs 480 320 260	500 cfs 830 610 510	630 cfs 2,000 1,400 1,040
43	Big River near Richwoods	1942-43, 1946-47, 1951, 1961-65, 1969	-	2 5 10	222 cfs 148 74 52	300 cfs 275 190 134	370 cfs 408 282 222	444 cfs 615 489 356	518 cfs 1,050 763 586
50	Big River at Byrnesville	1923-69	917	2 5 10	225 cfs 75 50 35	350 cfs 220 160 100	500 cfs 460 375 280	600 cfs 750 575 460	730 cfs 1,550 1,180 880
52	Meramec River near Eureka	1922-69	3,788	2 5 10	750 cfs 160 80 75	1,200 cfs 650 500 320	1,600 cfs 1,300 1,100 700	2,100 cfs 2,500 2,000 1,500	2,600 cfs 5,600 4,200 3,100
67	Joachim Creek at Hemetite	1961-65, 1967-69	95.0	2 5 10	19 cfs 10 4 3	38 cfs 33 21 12	58 cfs 70 57 41	66 cfs 108 84 66	76 cfs - 140 104

^{a/} Percent chance of deficiency indicates the percent of years in which a storage reservoir of indicated capacity would become empty.

^{b/} Amounts of storage listed are hydrologically feasible. The physical limitations of the terrain have not been analyzed.

Table 22 contains draft-storage frequency data for gaging stations in the St. Louis area. These data were computed by the mathematical technique of Markov chain analysis called probability routing, as described in a report by Skelton (1971).

Note that the frequency characteristics are expressed as percent chance of deficiency. This value indicates the percent of years in which a reservoir of indicated capacity will become empty. It also can be interpreted as the average chance of having an empty reservoir in any year over a long period of years. However, this does not mean that a deficiency is equally probable in each year, because a series of dry years will decrease the amount of water stored and increase the chance of deficiency in succeeding years.

The draft-storage data are useful primarily in making preliminary estimates of potential development and in comparing development possibilities of different streams. However, for small, multi-purpose reservoirs, the data may be adequate for final design purposes.

Regional draft-storage curves for a 2-percent chance of deficiency were developed from long-time streamflow records in eastern Missouri and are presented in figure 27. These curves can be used to estimate storage requirements at ungaged sites or gaging stations where records are short or inadequate. The standard errors of estimate for the regional curves were determined graphically and found to be 20 percent or less.

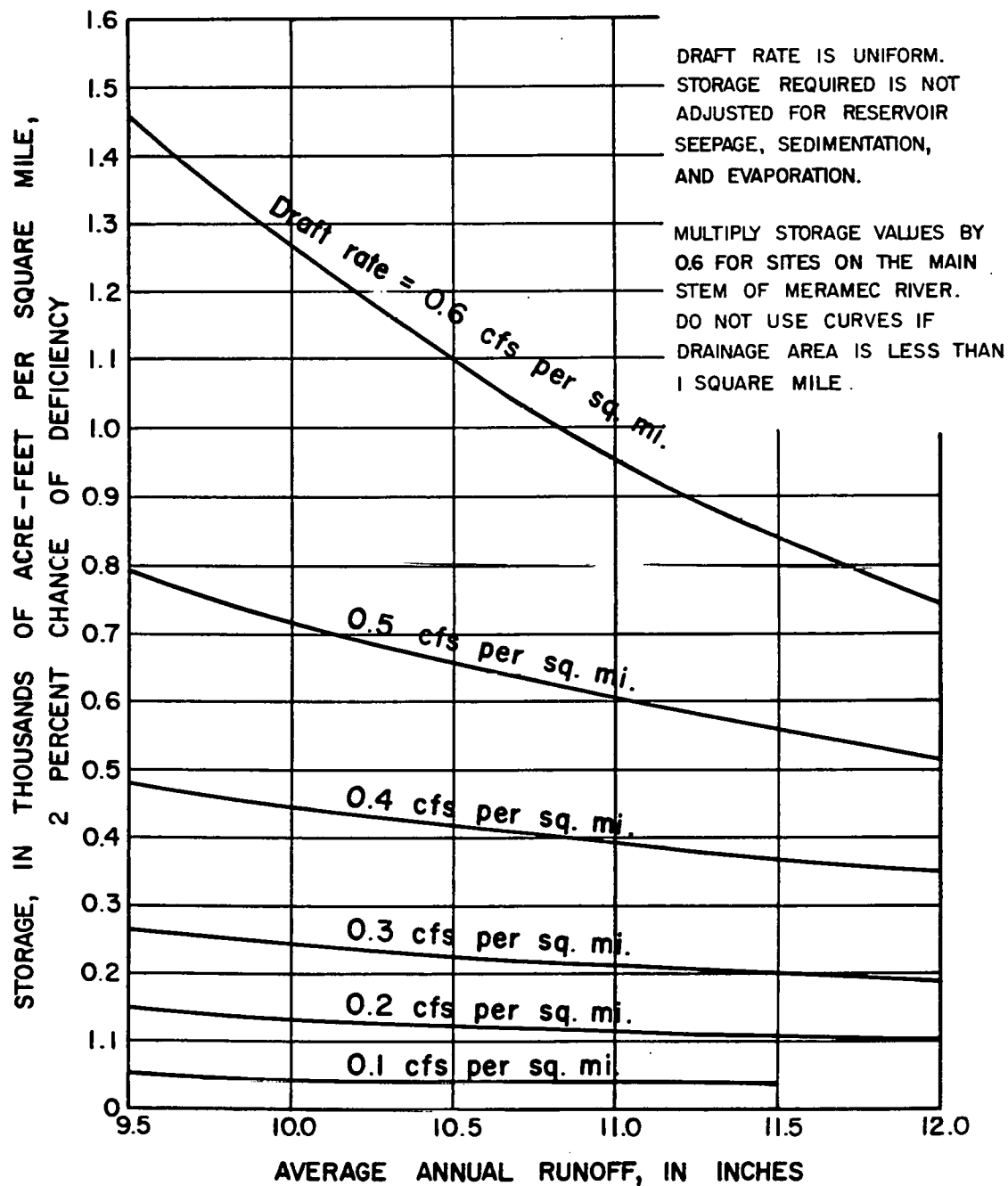


Figure 27
Regional draft-storage curves for the St. Louis area.

APPLICATION OF REGIONAL DRAFT-STORAGE CURVES

In most cases, proposed reservoir sites are located where long streamflow records are not available. Therefore, the regional draft-storage curves of figure 27 should be utilized in making estimates. The following steps are necessary in making estimates of storage requirements at ungaged sites:

1. Determine the drainage area upstream from the site, using the best available topographic map.
2. Determine average annual runoff for the basin to the nearest inch from figure 24. Use the center of the basin as the point of estimation.
3. Use the regional curves to estimate storage requirements. The estimates will be somewhat conservative; the average chance of the reservoir becoming empty in any year is 2 percent.
4. Where significant urbanization exists, the storage requirements obtained from the regional curves should be computed using adjusted values of mean flows to account for the increased runoff volumes from urbanized areas. Suggestions for these adjustments are presented in the section "Effects of Urbanization on Mean Flows."

RESERVOIR LOSSES

For this report no adjustments have been made to station data or regional curves for reservoir losses

due to evaporation, seepage or sedimentation. A detailed discussion of regional adjustments to storage requirements for these losses is presented by Skelton (1968, p. 15-23). This information will be useful in preliminary studies; however, a more detailed analysis will be necessary at the reservoir site prior to construction of major structures.

LIMITATIONS OF DATA

Before station data and regional draft-storage curves are used in project planning, the following limitations should be considered:

1. Regional curves and station data should not be extrapolated beyond the limits shown.
2. Regional curves are not applicable to streams significantly regulated by reservoirs or to the Mississippi and Missouri Rivers.
3. Regional curves should not be used for drainage areas of less than one square mile.
4. In the Ozarks part of the study area (fig. 1), field reconnaissance of potential reservoir sites is necessary to avoid gross underestimation of storage requirements. In this region, there is a possibility that small basins and reaches of some streams may have zones of significant water losses which were not discovered during hydrologic investigations of the region (see table 21). Special studies would be required to define storage requirements in water-loss areas and to determine if reservoirs are structurally feasible.

QUALITY OF SURFACE WATER

The St. Louis area is nearly surrounded by large streams. The Missouri River to the north, the Mississippi River to the east, and the Meramec River to the south make available an almost unlimited supply of surface water. Many of the water-supply and waste-disposal needs of the area are met by these streams. Because of their large flow, these streams are able to assimilate large amounts of wastes. Uses of the water, however, are limited when extensive and costly treatment is needed to obtain the desired quality.

Municipal, industrial, agricultural and other wastes entering streams anywhere in the north-central

part of the United States influence the quality of water in the Missouri and Mississippi Rivers in the St. Louis area. Not all of man's activities, however, have caused deterioration of the quality of water in these rivers. For instance, impoundments on the Missouri River main stem and tributaries over the past 20 years have resulted in a significant decrease in turbidity, an undesirable characteristic of Missouri River water.

The map of the study area, figure 2, includes locations of U.S. Geological Survey stream-sampling sites and water plants which are the source of data for this report.

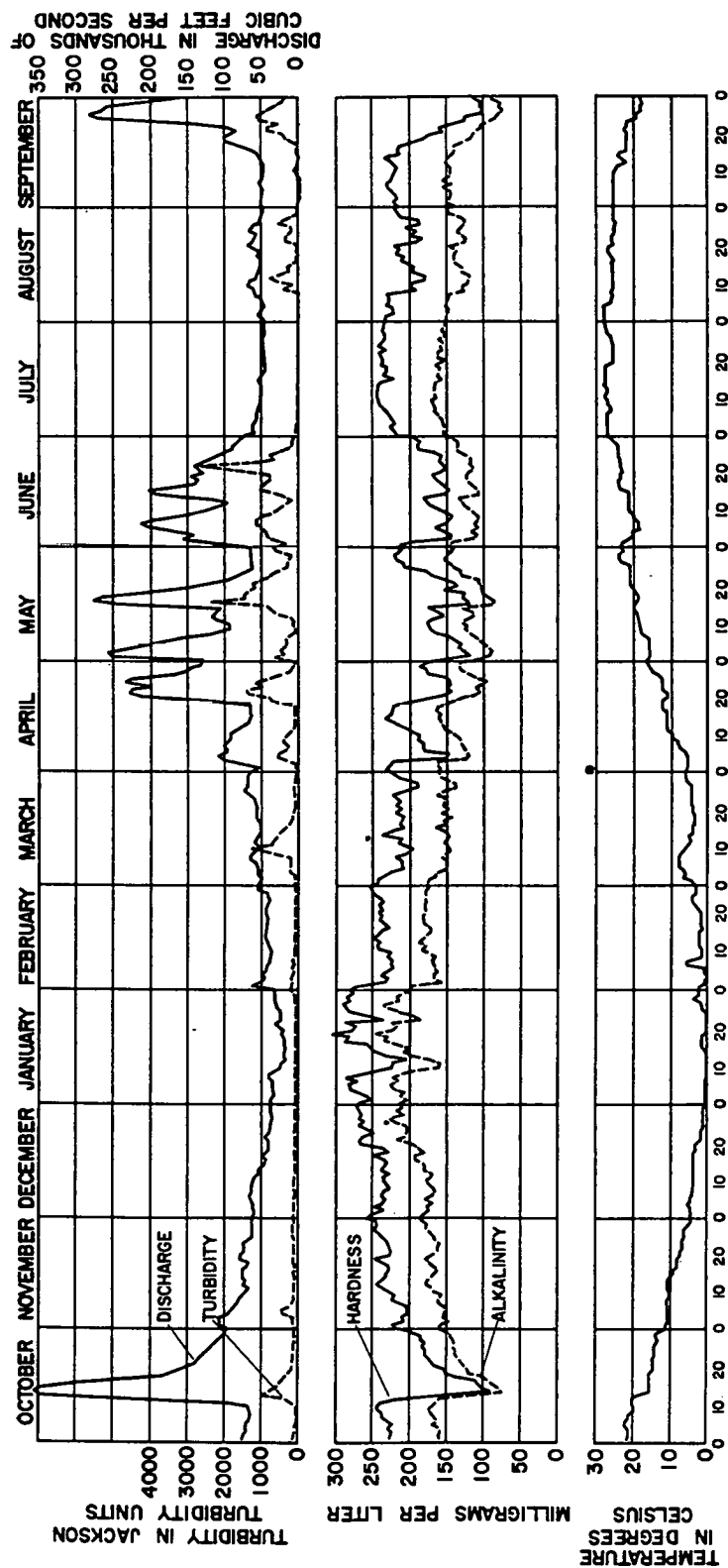


Figure 28
Relation between discharge and chemical and physical characteristics of water from the Missouri River
at Howard Bend Plant near St. Louis, Mo., 1969-70.

MISSOURI RIVER

Water in the Missouri River near St. Louis is moderately mineralized. The predominant chemical constituents are calcium, magnesium, sodium, bicarbonate and sulfate. Variations in dissolved-solids content are primarily caused by variations in the amounts of these constituents. Although a downward trend in turbidity has been observed in recent years, turbidity is still relatively high, and the water must be treated for most uses. Generally, the water is hard and this undesirable characteristic contributes to the need for treatment before use.

Daily changes in selected chemical and physical characteristics at the City of St. Louis Howard Bend Water Plant (fig. 2, map no. 27) are related to the discharge record from the gage at Hermann, Mo., for the 1970 water year in figure 28. Water temperature varied from 0.0 degrees Celsius (centigrade) in January and February to 29.0°C in July and August. Turbidity varied from 20 JTU (Jackson turbidity units) in January to 2,400 JTU in May with a median for the year of 135. Turbidity fluctuates rather closely with streamflow; therefore, turbidity is generally lower during winter when streamflow is low and higher during the spring and summer when streamflow is high. Alkalinity and hardness as CaCO_3 ranges from 76 and 89 mg/l respectively during the high water in October to high values of 243 and 303 mg/l in January.

Alkalinity and hardness vary inversely with streamflow and generally have higher values in the winter.

Ranges in chemical and physical characteristics of daily samples collected at Howard Bend for the 20-year period 1951-70 are summarized in table 23. During this period the average concentration of dissolved solids was 382 mg/l as compared to 365 mg/l reported for the 10-year period 1940-49 (Searcy, Baker and Durum, 1952).

Average monthly characteristics for the 20-year period, figure 29, include temperature variations from 2.0°C in January to 27.0°C in July. The long-term relationship in this figure follows the short-term relationship in figure 28. Dissolved solids, alkalinity and hardness were lowest in the summer when streamflow was high and highest during the winter when streamflow was low.

Annual average turbidity and annual average discharge for the period 1951-70 are plotted in figure 30. Turbidity decreased from an average of 1,002 JTU for the 5-year period 1951-55 to 361 for 1966-70. Discharge averaged the same for both periods, 77,000 cfs. Turbidity averaged 694 JTU for the 20-year period 1951-70, as compared to 1,670 JTU for the 10-year period 1940-49 (Searcy, Baker and Durum, 1952).

The double-mass curves in figure 31 show a decrease in turbidity and sediment, with the most

Table 23

Selected chemical and physical characteristics of water from the Missouri River at Howard Bend Plant near St. Louis, Mo., 1951-70
[analyses by City of St. Louis]

Characteristics	Minimum	Mean	Maximum
Temperature (°C)-----	0	14.5	31.0
pH-----	7.5	8.1	9.6
Alkalinity as CaCO_3 (mg/l)	53	150	294
Hardness as CaCO_3 (mg/l)	83	206	366
Turbidity (JTU)-----	5	694	12,000

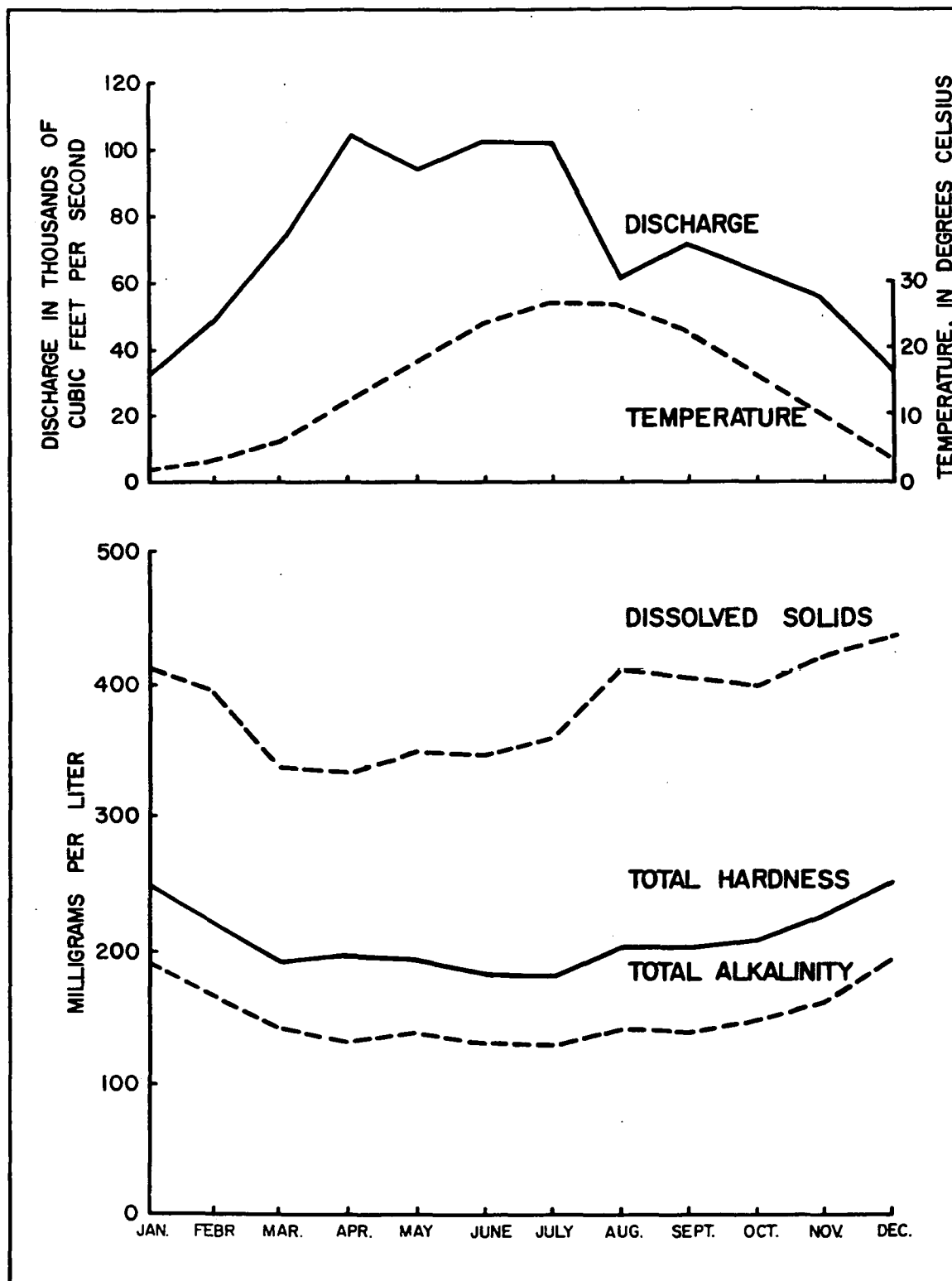


Figure 29
Average monthly chemical and physical characteristics of water from the Missouri River
at Howard Bend Plant near St. Louis, Mo., 1951-70.

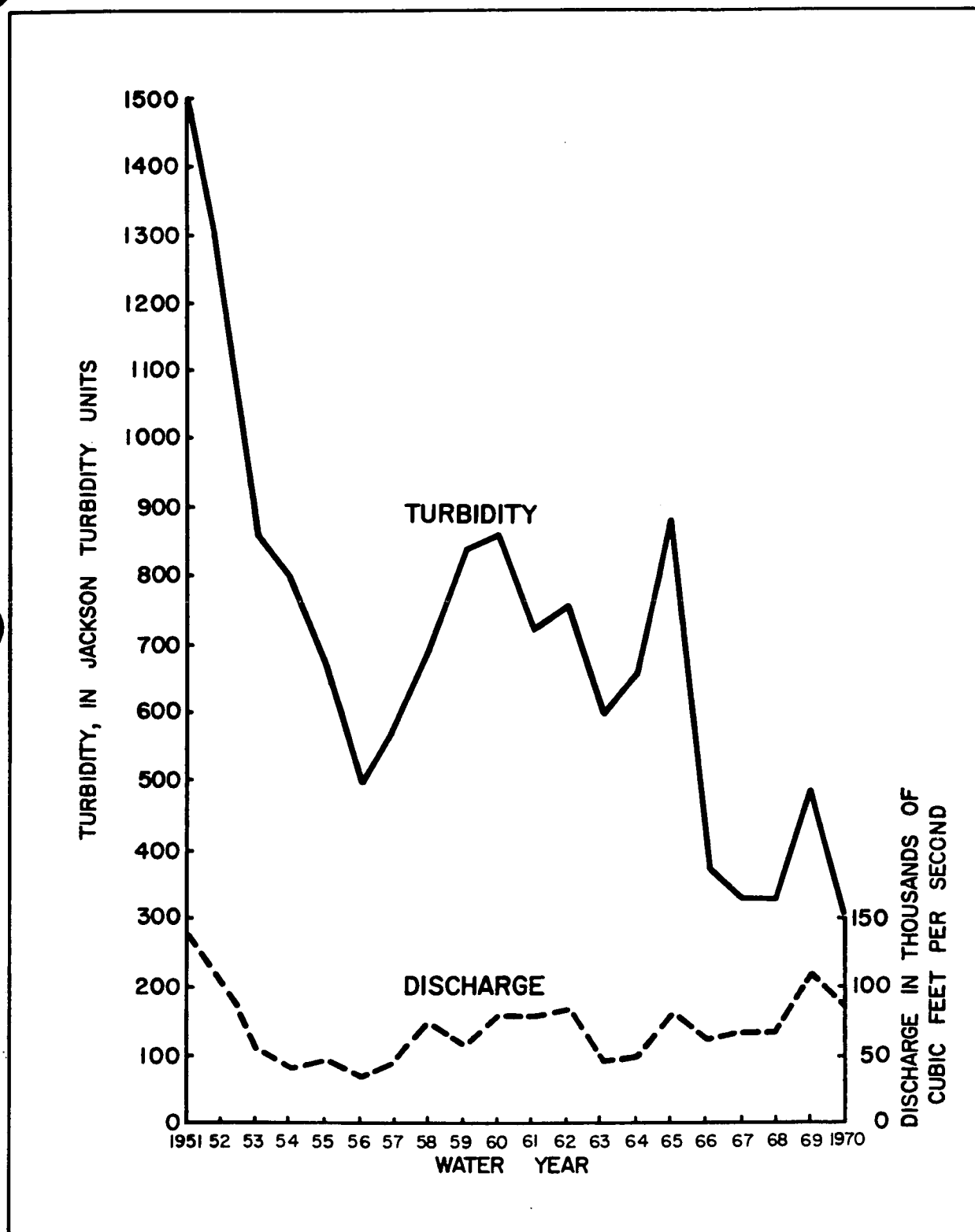


Figure 30

Annual average turbidity and discharge of the Missouri River at Howard Bend Plant near St. Louis, Mo., 1951-70.

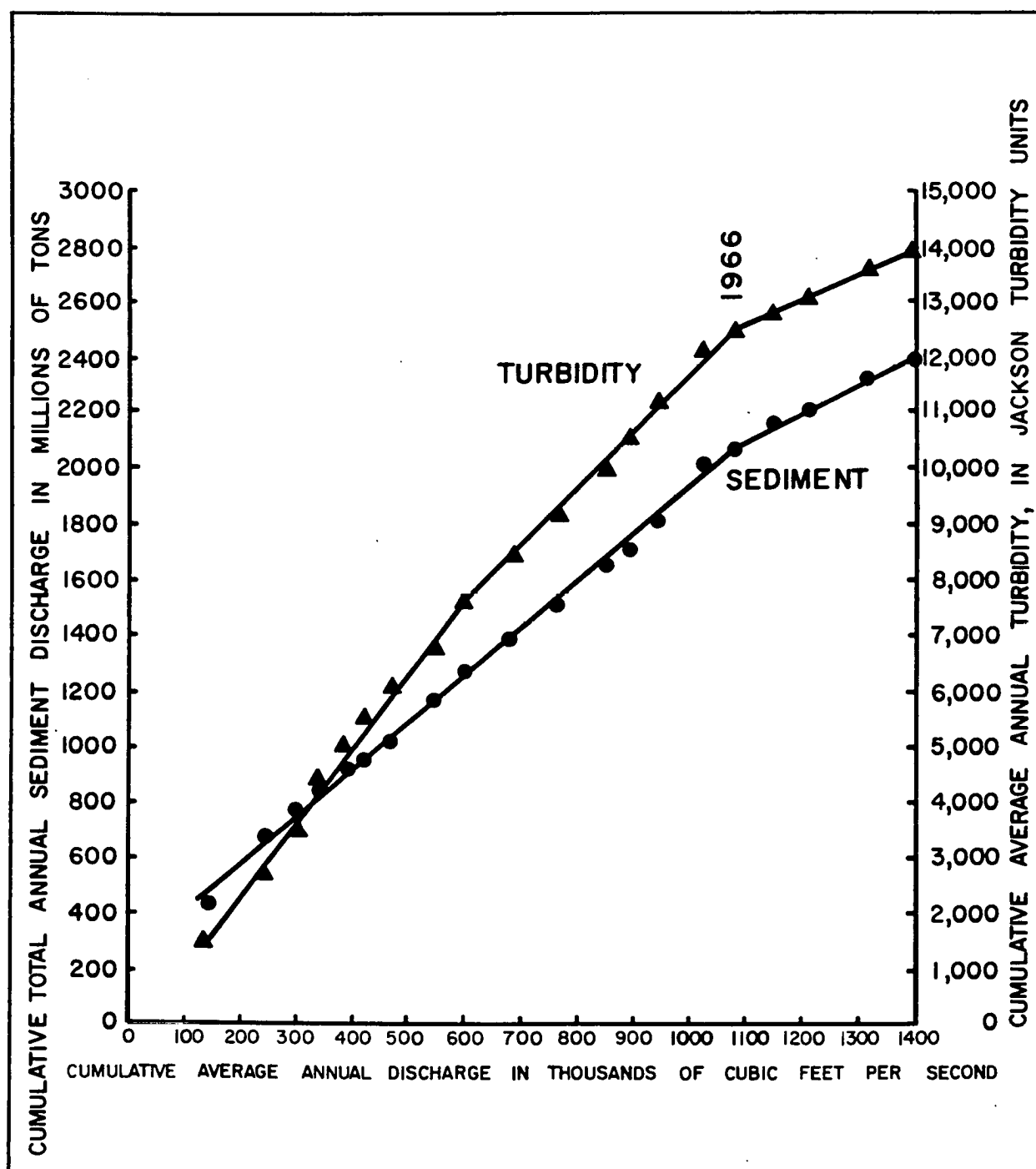


Figure 31
Double-mass curve of turbidity and sediment versus discharge for the Missouri River
at Howard Bend Plant near St. Louis, Mo., 1951-70.

Table 24

Selected chemical and physical characteristics of water
from the Mississippi River at Alton, Ill., 1970
[analyses by Alton Water Co.]

Characteristic	Minimum	Median	Maximum
Temperature (°C)-----	0	12.5	29.5
pH-----	7.7	8.1	8.6
Alkalinity as CaCO ₃ (mg/l)	87	168	205
Hardness as CaCO ₃ (mg/l)	118	235	304
Turbidity (JTU)-----	12	40	875

significant change occurring about 1966. The sediment record was collected at Hermann, Mo., by the U.S. Army Corps of Engineers, Kansas City District. Federal impoundments constructed on the Missouri River's main stem and tributaries (numbering about 50) and control structures on the Missouri River are apparently responsible for the decrease in turbidity and sediment. However, the actual effectiveness of the impoundments for sediment removal is difficult to evaluate because of the inexact relationship of sediment to streamflow. Jordan (1968) attempted to separate the effects of streamflow from those of the impoundments. The results were based on data for years prior to 1964 and indicated that impoundments caused a 25- to 30-percent reduction in sediment discharge for the Missouri River at Kansas City. The influence would be less for stations downstream from Kansas City because of fewer impoundments downstream. More impoundments have been completed since Jordan's analysis and apparently have caused further decrease in sediment discharge. As more impoundments are constructed, especially in the uncontrolled sediment-laden tributaries downstream from Kansas City, sediment and turbidity should continue to decrease in the St. Louis area.

Appendix 5 is a compilation of annual average values of several water-quality characteristics of the Missouri River at the City of St. Louis Howard Bend Water Plant for the period April 1951 to March 1970. Total coliform bacteria averaged about 5,900

col/100 ml (colonies per 100 milliliters) for the first 5 years and about 14,000 col/100 ml for the last 5 years of the period.

MISSISSIPPI RIVER

UPSTREAM FROM THE MISSOURI RIVER

Mississippi River water at the Alton Water Plant (fig. 2, map no. 17), about 9 miles upstream from the mouth of the Missouri River, is generally of good quality and suitable for most uses. The water, which is moderately mineralized, is a calcium-bicarbonate type and contains significant amounts of magnesium and sulfate in the dissolved solids. Although turbidity is relatively low upstream from the Missouri River, the water is very hard and some treatment such as softening would be desirable for municipal and some industrial uses.

The relation between discharge and some water-quality characteristics at Alton are illustrated in figure 32 for the 1970 water year. Turbidity reached undesirable levels only a few times during the high streamflow of spring and fall.

Ranges in chemical and physical characteristics of daily samples collected during the 1970 water year are listed in table 24.

Total coliform bacteria counts made by the Alton Water Company on 26 samples collected from September to December 1970 ranged from 2,000 to 64,000, with a median of 11,000 col/100 ml.

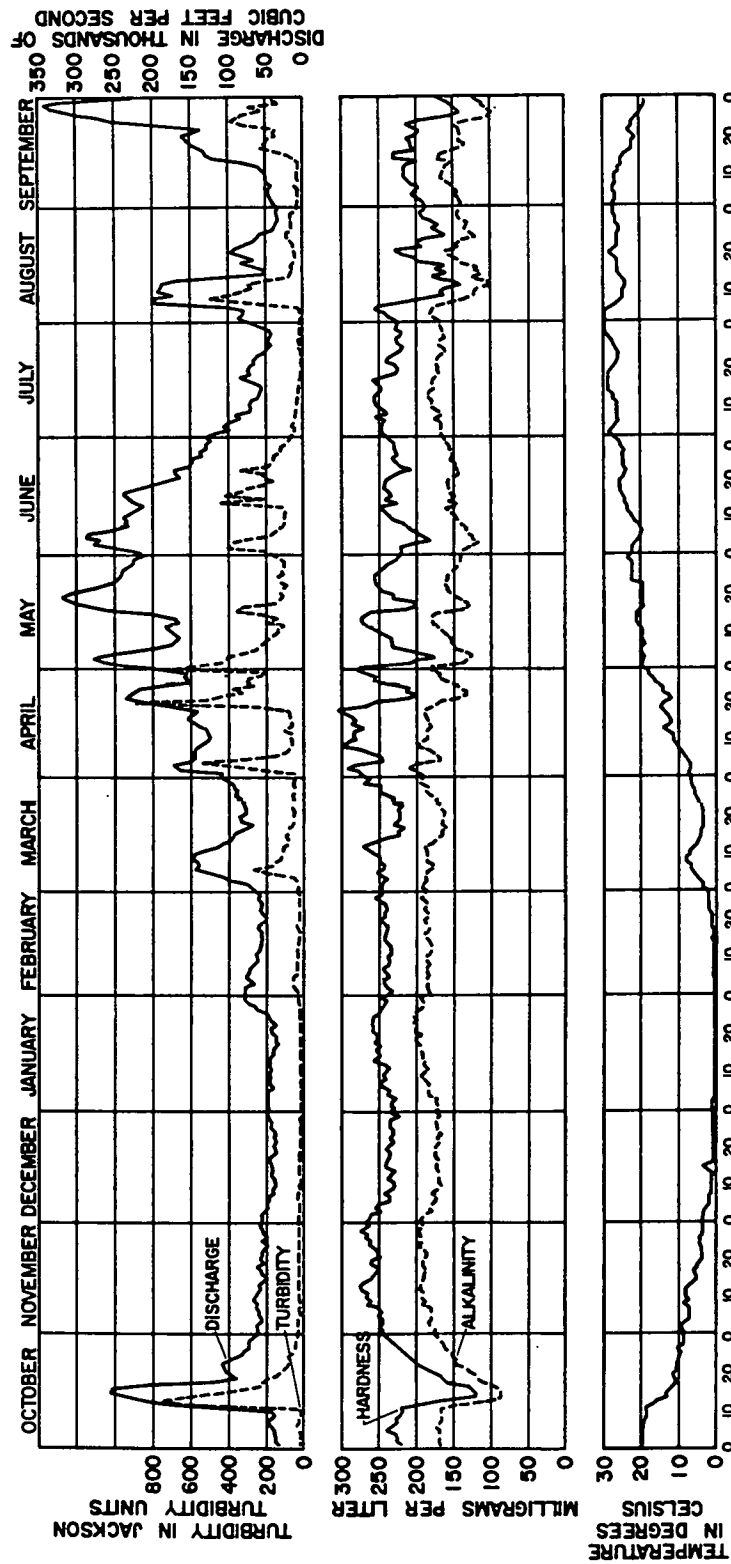


Figure 32

Relation between discharge and chemical and physical characteristics of Mississippi River at Alton, Ill., 1969-70.

Table 25

Selected chemical and physical characteristics of water from the
Mississippi River at Chain of Rocks Plant in St. Louis, Mo., 1951-70
[analyses by City of St. Louis]

Characteristic	Minimum	Mean	Maximum
Temperature (°C)-----	0	14.5	32.0
pH-----	7.2	8.0	9.0
Alkalinity as CaCO ₃ (mg/l)	72	147	290
Hardness as CaCO ₃ (mg/l)	89	204	323
Turbidity (JTU)-----	8	608	6,000

DOWNSTREAM FROM THE MISSOURI RIVER

Inflow from the Missouri River during periods of low flow does not mix completely for several miles downstream. As a result, water-quality records at the Chain of Rocks Water Plant (fig. 2, map no. 33), about 5 miles downstream from the confluence with the Missouri, are indicative of Missouri River inflow. The water on the opposite (east) side of the river is about the same quality as water in the Mississippi River upstream from the confluence.

Daily variations of selected characteristics of Mississippi River water at Chain of Rocks for the 1970 water year are illustrated in figure 33. Temperature ranged from 0.0°C in January to 29.5°C in July and August. Alkalinity as CaCO₃ varied from 83 mg/l in September and October to 241 mg/l in January. Hardness as CaCO₃ ranged from 105 mg/l in October to 296 mg/l in January. Turbidity varied from 10 JTU in January to 4,000 JTU in May. The median turbidity was 160 JTU, as compared to a median of 40 JTU for the same period at Alton. Inflow from the Missouri River is responsible for the increased turbidity in the Mississippi, especially during periods of high flow in the Missouri River.

Ranges in chemical and physical characteristics of daily samples at Chain of Rocks are summarized in table 25 for the 20-year period October 1950 to September 1970. The average dissolved-solids content for the period was 373 mg/l. This compares to an average of 340 mg/l for the 10-year period 1940-49

(Searcy, Baker and Durum, 1952). The dissolved solids are primarily composed of bicarbonates and sulfates of calcium and sodium.

Average monthly water temperature, figure 34, ranged from 2.0°C for January to 26.5°C for August. Dissolved solids, alkalinity and hardness were lowest in the summer when streamflow was high and highest during the winter when streamflow was low.

As shown in figure 35 annual average discharge was relatively uniform for the period 1951-70, while turbidity dropped from an average of 880 JTU for the first 5 years to an average of 355 JTU for the last 5 years of the period.

Double-mass curves of turbidity and sediment versus streamflow are plotted in figure 36 for the years 1951-70. A decided break in slope is noted about 1966, which indicates a significant decrease in turbidity and sediment since that time. This decrease was caused mainly by the completion of control structures in the upper Missouri River basin, as described in the previous section on the Missouri River.

Annual average values of several characteristics of Mississippi River water at Chain of Rocks for the period April 1951 to March 1970 are compiled in appendix 6. The bacteria data indicate that total coliform bacteria counts averaged about 9,500 col/100 ml for the years 1951-55, and about 27,000 col/100 ml for the years 1966-70.

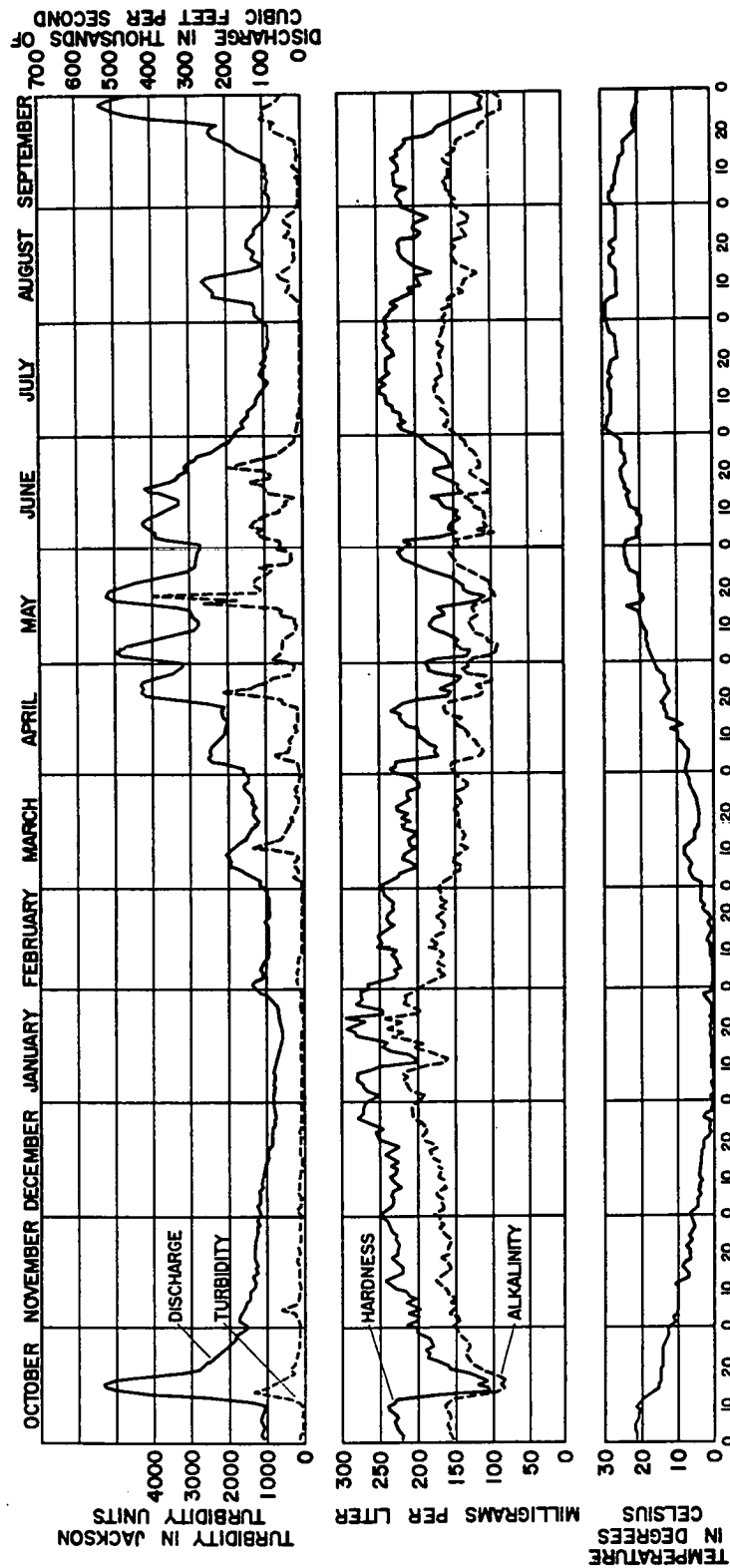


Figure 33
Relation between discharge and chemical and physical characteristics of Mississippi River water
at Chain of Rocks Plant in St. Louis, Mo., 1969-70.

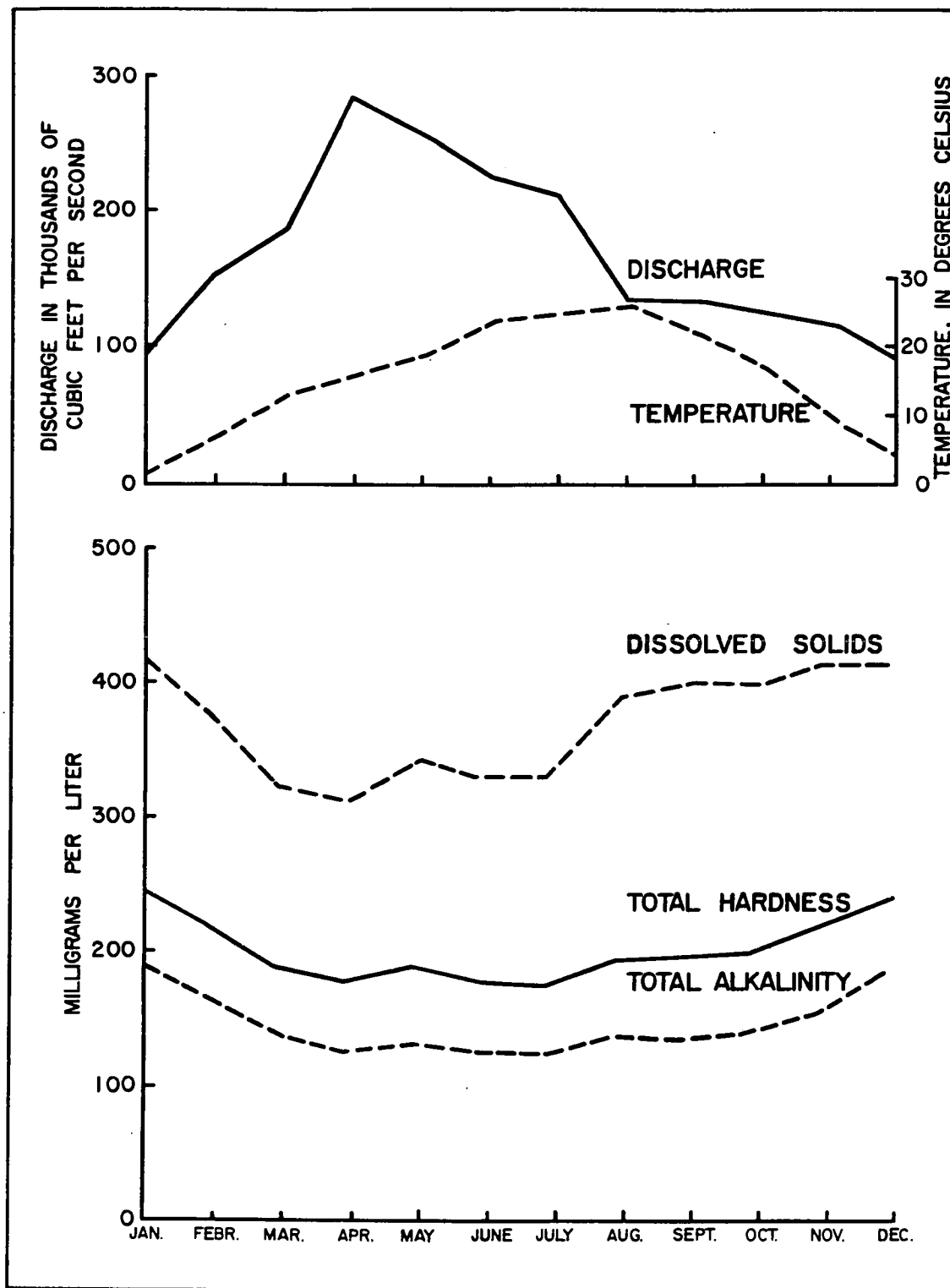


Figure 34

Average monthly chemical and physical characteristics of the Mississippi River water at Chain of Rocks Plant in St. Louis, Mo., 1951-70.

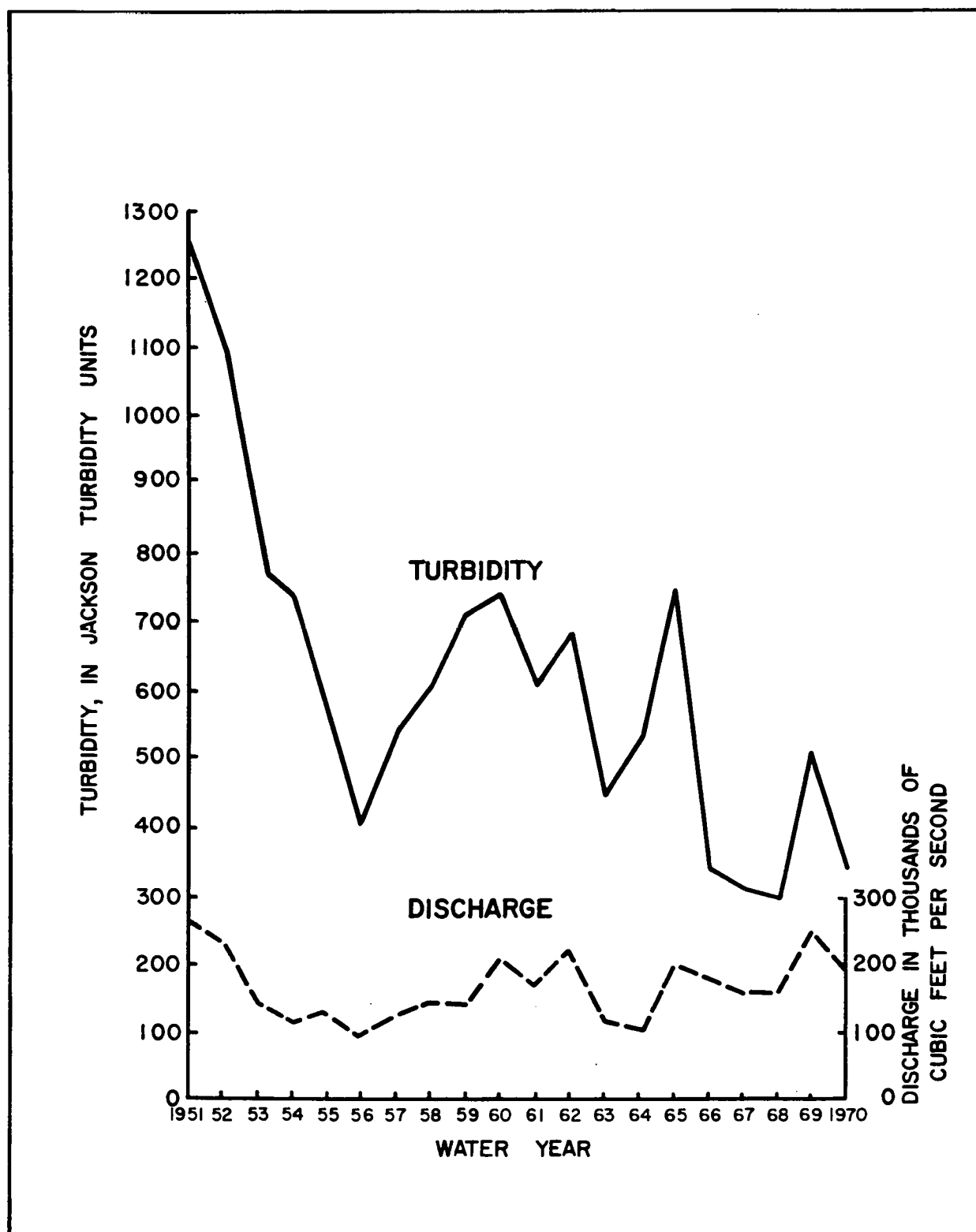


Figure 35

Annual average turbidity and discharge of the Mississippi River at Chain of Rocks Plant in St. Louis, Mo., 1951-70.

TRIBUTARY STREAMS

Streams tributary to the Missouri and Mississippi Rivers in the St. Louis area represent a small part of

the total volume of surface water available to that area. However, distribution of the smaller streams throughout the three counties makes them important.

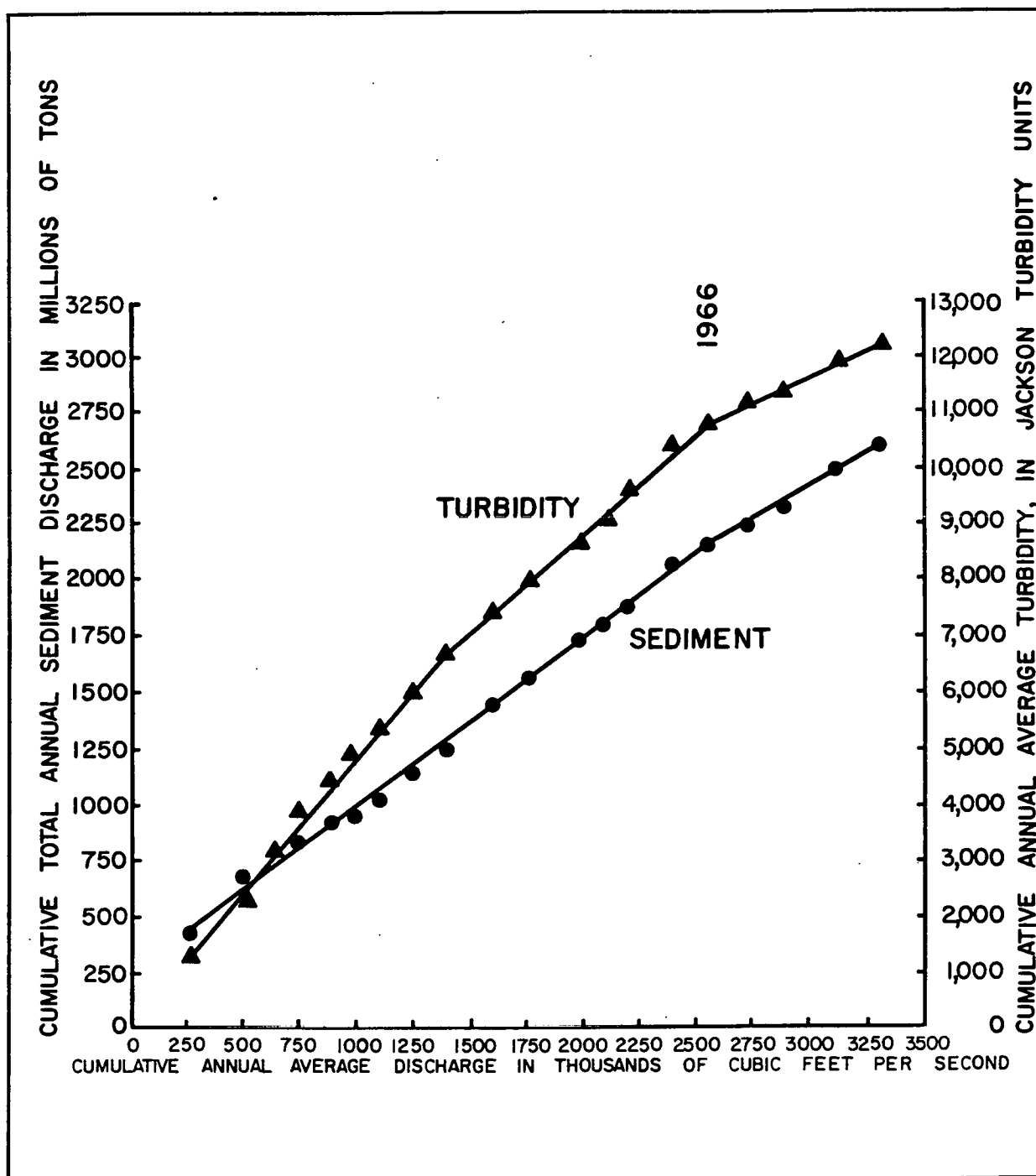


Figure 36

Double-mass curve of turbidity and sediment versus discharge for the Mississippi River at Chain of Rocks Plant in St. Louis, Mo., 1951-70.

The largest of the tributary streams are the Meramec River and the Big River, which flows into the Meramec.

The U.S. Geological Survey has a monthly sampling station at the gaging station on the Big River near De Soto, Mo. (fig. 2, map no. 42). Data covering some of the more important water-quality characteristics for the period 1966-70 are summarized in table 26. Water in the Big River is a calcium-magnesium-bicarbonate type.

Fecal coliform bacteria counts for the Big River ranged from 1 to 13,000 col/100 ml, with a median of about 70 for the monthly samples collected during the 1970 water year. Fecal streptococci varied from 12 to 45,000, with a median of about 140 col/100 ml. Fecal coliform to fecal streptococci ratios for individual samples averaged about 0.5, indicating that the pollution was derived predominantly from animal wastes.

The Meramec River flows into the Mississippi River south of St. Louis, about 34 miles downstream from the mouth of the Missouri River. Records of discharge are given for the gaging station at Eureka,

Mo., about 35 miles upstream from the mouth (fig. 2, map no. 52).

Suspended-sediment discharges for the Meramec River at Eureka, Mo., from February 1969 to September 1970, ranged from 17 to 175,000 tons per day and averaged 2,680 tons per day. Daily sediment concentrations varied from 19 to 1,430 mg/l and averaged 147 mg/l. Sediment loads and concentrations were affected at times during the period by highway construction activities upstream from the sampling site. The stream is normally clear and transports relatively small amounts of sediment. Most of the sediment discharge occurs during short periods of high streamflow.

The St. Louis County Water Company furnished data for the Meramec River at Fenton, Mo., about 16 miles upstream from the mouth (fig. 2, map no. 59). Some of the characteristics for daily samples collected during the period 1966-70 are summarized in table 27. The average hardness of 166 mg/l indicates that the water is hard. Turbidity is normally low in the Meramec River and not a problem for most uses. Monthly variations are shown in figure 37. A compilation of annual average values of several of the

Table 26

Selected chemical and physical characteristics of water from the Big River near De Soto, Mo., 1966-70

Characteristic	Minimum	Median	Maximum
Temperature (°C)-----	0	14.0	28.0
pH-----	7.4	8.1	8.5
Alkalinity as CaCO ₃ (mg/l)	92	211	246
Hardness as CaCO ₃ (mg/l)	110	245	296
Dissolved solids (mg/l)---	144	271	342
Turbidity (JTU)-----	0	6	300

more important water-quality characteristics of the Meramec River at Fenton, Mo., for the period January 1966 to December 1970, are listed in table 28. Meramec River water is also a calcium-magnesium-bicarbonate type.

The U.S. Geological Survey operates a monthly sampling station on the Meramec River at Paulina

Hills, Mo., about 10 miles upstream from the mouth (fig. 2, map no. 61). Dissolved solids, hardness and alkalinity duration curves for the period August 1963 to September 1970 are shown in figure 38. The median value, that which was equaled or exceeded 50 percent of the time, was 208 mg/l for dissolved solids, 176 mg/l as CaCO_3 for hardness, and 160 mg/l as CaCO_3 for alkalinity.

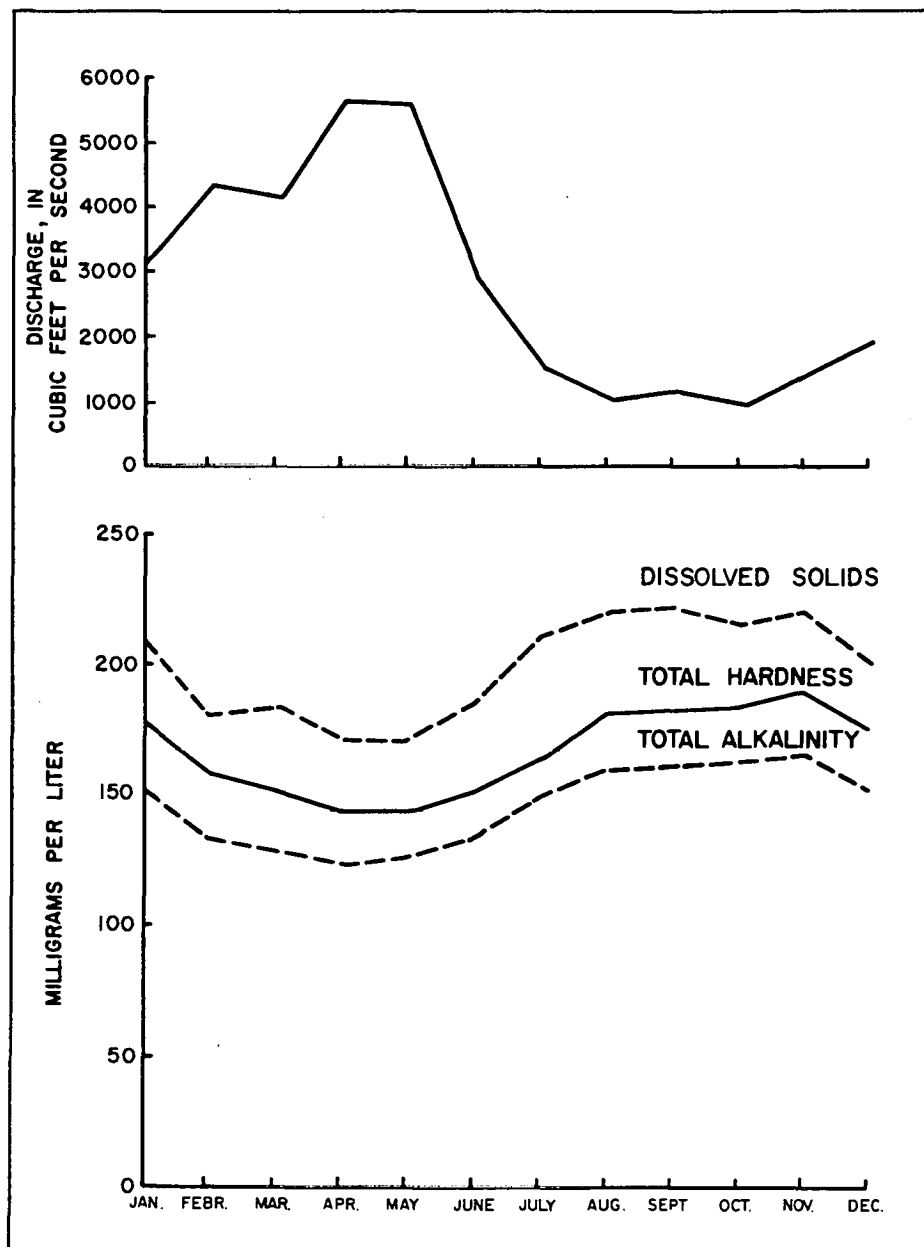


Figure 37

Average monthly chemical and physical characteristics of the Meramec River at Fenton, Mo., 1966-70.

Table 27

Selected chemical and physical characteristics of water from the Meramec River at St. Louis County South Plant in Fenton, Mo., 1966-70
[analyses by St. Louis County Water Co]

Characteristic	Minimum	Mean	Maximum
pH-----	7.8	8.2	8.6
Alkalinity as CaCO ₃ (mg/l)	29	145	210
Hardness as CaCO ₃ (mg/l)	36	166	236
Dissolved solids (mg/l)	17	198	428
Turbidity (JTU)-----	1	64	2,000

Table 28

Annual average water-quality characteristics of the Meramec River at Fenton, Mo., 1966-70
[in milligrams per liter except as indicated; analyses by St. Louis County Water Co]

Year ending December 31	1966	1967	1968	1969	1970
Silica (SiO ₂)-----	6.8	6.4	7.4	7.4	7.0
Iron (Fe)-----	0.04	0.07	0.06	0.02	0.01
Calcium (Ca)-----	34	32	33	34	34
Magnesium (Mg)-----	21	19	20	19	19
Sodium and Potassium (Na&K)	6	6	5	6	4
Carbonate (CO ₃)-----	3	2	2	2	3
Bicarbonate (HCO ₃)-----	148	138	140	140	139
Sulfate (SO ₄)-----	21	18	20	20	19
Chloride (Cl)-----	11	9	8	9	9
Fluoride (F)-----	0.1	0.1	0.1	0.1	0.1
Nitrate (NO ₃)-----	2.2	1.7	2.5	2.4	2.0
Ammonia (NH ₃)-----	0.1	0.1	0.1	0.1	0.1
Ortho Phosphate (PO ₄)-----	0.11	0.13	0.14	0.13	0.13
Dissolved solids-----	201	193	195	195	203
Alkalinity as CaCO ₃ -----	151	140	142	142	142
Hardness as CaCO ₃ -----	172	159	164	164	165
Color (units)-----	10	19	16	15	17
Turbidity (JTU)-----	40	65	56	60	85
pH (units)-----	8.2	8.2	8.2	8.2	8.2

Fecal coliform bacteria counts for the Meramec River varied from 7 to 3,800 col/100 ml and had a median of about 75 for the monthly samples collected in the 1970 water year. Fecal streptococci ranged from 16 to 18,000 and had a median of 55 col/100 ml. Fecal coliform to fecal streptococci ratios for individual samples averaged about 1.1. This indicates that the pollution is mostly derived from animal wastes.

The three-county area is experiencing a high rate of population growth, especially in St. Charles and Jefferson Counties. Much of the development is in unincorporated areas. Because of scattered development, hundreds of individually operated waste-treatment facilities are contributing substantial quantities of treated and partially treated waste effluents to the smaller streams.

Miscellaneous samples were collected from several streams outside the metropolitan St. Louis area, and results of their analysis are in appendix 4. Most of the samples were collected during times of low streamflow.

The surface water in St. Charles County flows over limestone rocks and is a calcium-bicarbonate type. Streams in Jefferson County flow over dolomitic rocks, and the water is a calcium-magnesium-bicarbonate type. The higher magnesium content in Jefferson County is accompanied by a higher hardness than in St. Charles County.

Bacteria counts for small streams in St. Charles County are generally higher than those in Jefferson County and show a higher fecal coliform to fecal streptococci ratio, which indicates that the bacteria are probably from human wastes.

Maline, Gravois, Cold Water and Watkins Creeks, and River des Peres are the principal watersheds in the metropolitan St. Louis area. They include an area of approximately 188 square miles and an estimated 1970 population of 1,009,000 persons. These streams receive residential, commercial and industrial wastes and receive runoff from highly urbanized areas to the point where they cannot assimilate all the wastes. The Metropolitan St. Louis Sewer District (MSD) is currently making a study of the area's water resources problems and needs and will make recommendations for improvement of surface-water quality.

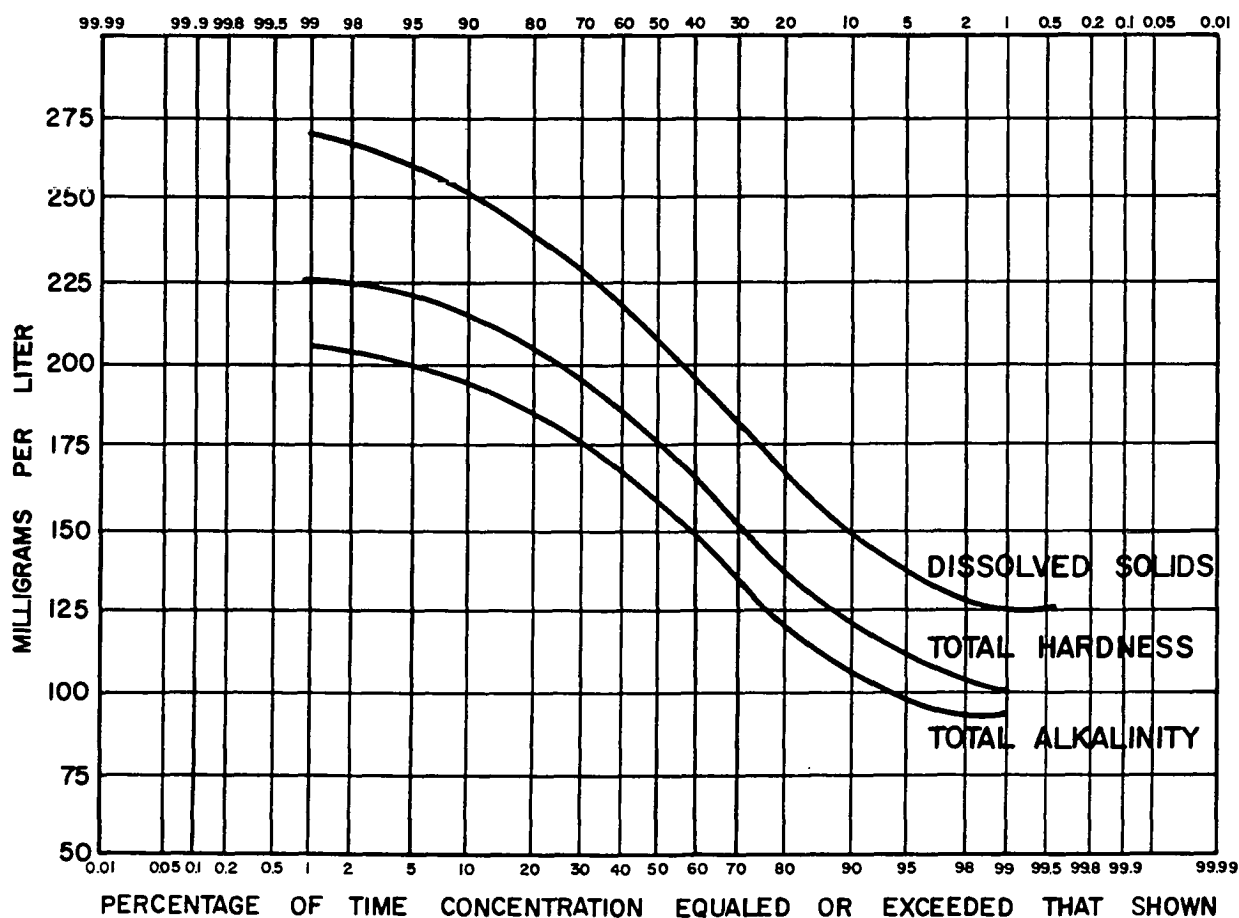


Figure 38

Duration curves of selected water-quality characteristics of the Meramec River at Paulina Hills, Mo.

WATER RESOURCES OF THE ST. LOUIS AREA, MISSOURI

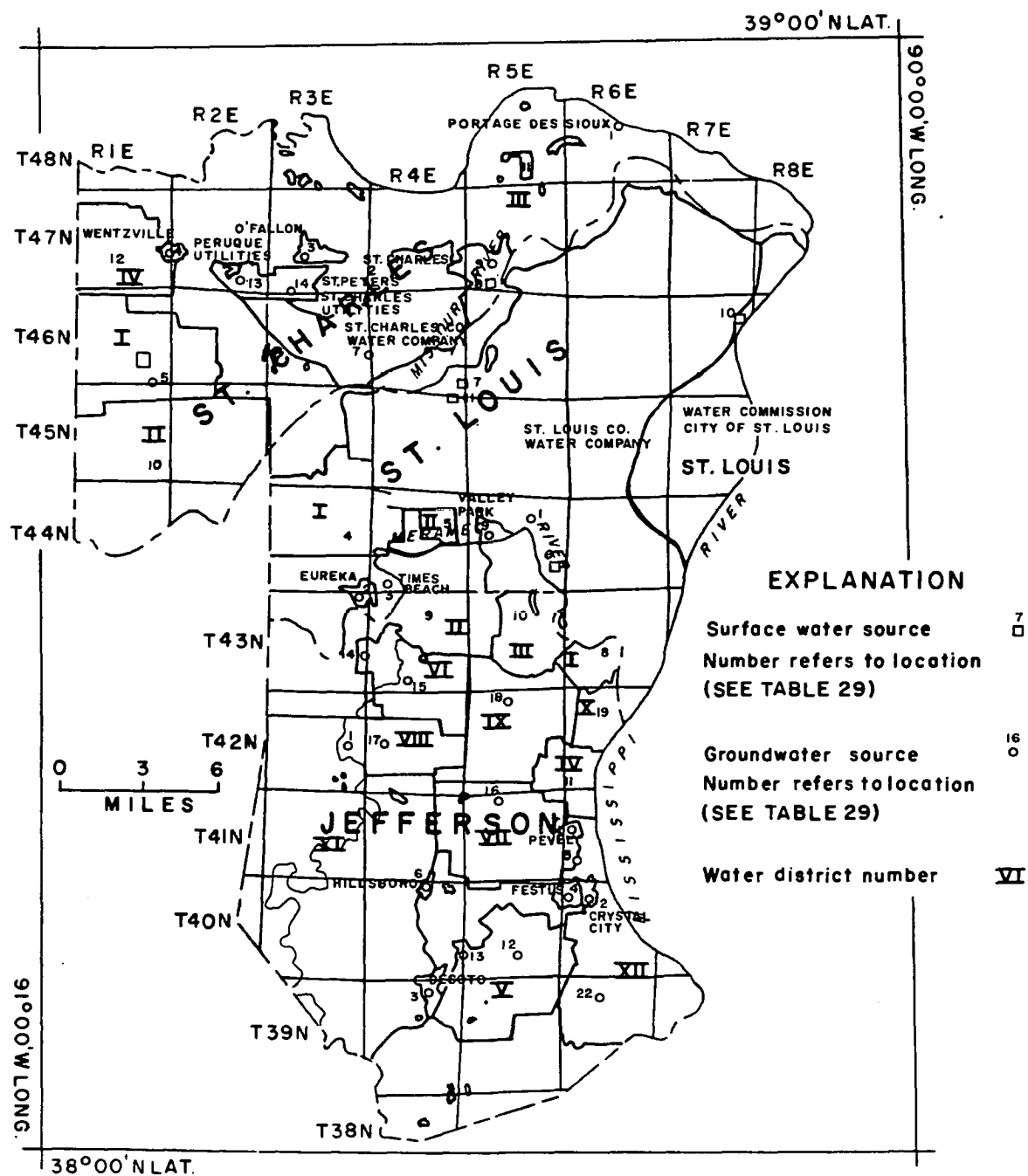


Figure 39

Areas served by a central water supply. Roman numerals indicate the water district numbers. Modified

from East-West Gateway Coordinating Council (Water Facilities Map, 1970).

WATER UTILIZATION

The principal uses of water in the three-county area, the estimated amounts used, and the source of the water are shown below:

Use	Source and amounts (mgd)	
	Surface water	Ground water
Public water supply *, +	292	10
Rural use	3	6
Irrigation	See text	
Thermoelectric power *	819	—
Self-supplied industrial *	9	15
Total	1,123	31

* Data from Missouri Water Resources Board, 1970.
Census of Public Water Supplies in Missouri, 1969.

Approximately 97 percent of the water used in the three-county area comes from a surface-water source, 2 percent of the water used is pumped from alluvial aquifers, and 1 percent is pumped from bedrock

aquifers. More than 85 percent of the surface water used is from the Mississippi River.

Figures for public supply include water used by municipalities, water-supply districts, subdivisions and trailer courts. Figure 39 and table 29 show the cities and public water-supply districts served by a central water supply. The City of St. Louis and the St. Louis County Water Company account for approximately 289 of the 292 mgd of surface water used for public water supply. Rural use is for both domestic and livestock purposes and was estimated based on census figures. The amount of water used for irrigation will vary with rainfall. In 1968 it was estimated that approximately 60 million gallons per year were used for irrigation of crops. A little over half of this amount was from wells. An undetermined, but probably small amount of water is withdrawn from wells in the Mississippi River alluvium of St. Charles County. Water from these wells is pumped into reservoirs to provide a suitable habitat for waterfowl during the hunting season. By far the largest use of water is for the generation of thermoelectric power. This is largely a nonconsumptive use, the water being used primarily for cooling.

SUMMARY AND CONCLUSIONS

SURFACE WATER

No shortage of surface-water supplies is foreseeable for major users who are able to tap the large rivers of the area. Of the large amount of available surface water (114,000 million gallons per day on the average), only about 1,120 million gallons per day is withdrawn for all uses.

Those who are interested in supplies from the smaller tributary streams face more difficult problems. The natural flows of streams in St. Charles and St. Louis Counties and the northern two-thirds of Jefferson County are generally highly variable. In these areas, as shown in figure 26, a lack of natural

sustained low flows makes it necessary to utilize storage reservoirs when year-round surface-water supplies are required. Streams in southern Jefferson County have a more consistent flow pattern and better-sustained low flows. However, major water users would probably require storage reservoirs in this region also.

Impoundments may not be necessary to insure adequate quantities of water in the lower reaches of many tributary streams. These reaches are ponded by backwater from the Mississippi and Missouri Rivers, thus maintaining a dependable supply in the channel.

WATER RESOURCES OF THE ST. LOUIS AREA, MISSOURI

Table 29
Water-Supply Facilities In The St. Louis Area

Municipality or operating agency	No. on map (Fig. 39)	Source	Average pumpage (million gallons per day)
<u>St. Louis County</u>			
Kirkwood	1	Ranney well: Aux. Meramec River and St. Louis County Water Co.	3.500
Eureka	2	3 wells	.172
Times Beach	3	1 well	.100
St. Louis County Water District No. 1	4	St. Louis County Water Co.	.041
St. Louis County Water District No. 2	5	St. Louis County Water Co.	.041
St. Louis County Water Co.			100.000
South Plant	6	Meramec River	-
Central Plant	7	Missouri River	-
North Plant	8	Missouri River	-
Valley Park	9	2 wells	.294
<u>City of St. Louis</u>			
St. Louis City Water Co.			150.000
Chain of Rocks Plant	10	Mississippi River	-
Howard Bend Plant	11	Missouri River	-
<u>St. Charles County</u>			
Portage Des Sioux	1	1 alluvial well	0.025
St. Peters	2	2 drilled wells	0.035
O'Fallon	3	3 drilled wells	0.533
Wentzville	4	4 drilled wells	0.350
St. Charles FWSD No. 1	5	1 drilled well	-
St. Charles County Water Division			
North Plant	6	3 alluvial wells	.400
South Plant	7	2 alluvial wells	0.100
St. Charles City			3.000
Plant No. 1	8	Missouri River	-
Plant No. 2	9	5 alluvial wells: Mississippi River Bottom	-
St. Charles FWSD No. 2	10	Under construction	-
St. Charles FWSD No. 3	11	Dormant	-
St. Charles FWSD No. 4	12	Dormant	-
Peruque Utilities	13	2 wells	-
St. Charles Utilities	14	1 well	-

Water-Supply Facilities In The St. Louis Area--continued

Municipality or operating agency	No. on map (Fig. 39)	Source	Average pumpage (million gallons per day)
<u>Jefferson County</u>			
Cedar Hill	1	2 wells	.043
Crystal City	2	Ranney well	.500
De Soto	3	2 wells	.650
Festus	4	5 wells	.500
Herculaneum	5	3 wells	.280
Hillsboro	6	3 wells	.130
Pevely	7	2 wells	.058
Jefferson County PWSD No. 1	8	St. Louis County Water Co.	.750
Jefferson County PWSD No. 2	9	St. Louis County Water Co.	.173
Jefferson County PWSD No. 3	10	St. Louis County Water Co.	.200
Jefferson County PWSD No. 4	11	Jefferson County PWSD No. 9	-
Jefferson County PWSD No. 5, East	12	1 well	.031
Jefferson County PWSD No. 5, West	13	1 well	.024
Jefferson County PWSD No. 6 (Hoene Springs)	14	2 wells	.010
Jefferson County PWSD No. 6 (House Springs)	15	1 well	.040
Jefferson County PWSD No. 7	16	2 wells	.055
Jefferson County PWSD No. 8	17	1 well	.024
Jefferson County PWSD No. 9	18	2 wells	.070
Jefferson County PWSD No. 10	19	St. Louis County Water Co.	-
Jefferson County PWSD No. 12	20	1 well	-

Modified from East-West Gateway Coordinating Council (Water Facilities Inventory and Evaluation, 1971).

However, extensive treatment may be required to make the water suitable for use.

When developments are planned in the tributary basins, proposed effluent loads should always be balanced against streamflow available for dilution. The low-flow potential of the stream is the principal limiting factor in effective waste disposal via the drainage network and can be evaluated by using the analysis and tabulations presented in the "Low Flows" section of this report.

The low flows of many small tributary streams are already greatly augmented by domestic effluent, with a net increase in dry-weather flow. From a water-use standpoint, augmentation of small natural

streamflows by this effluent is not desirable because of high treatment costs.

The increase of low flows by urbanization has been accompanied by an increase in average annual runoff and flood peaks. The intensity of these effects depends on the percentage of impervious area in a basin and the quantity of effluent entering the stream from sewage treatment plants, septic tanks, industry and storm sewers. During low-order floods (2-year recurrence interval), storm sewers, gutters and man-made ditches greatly increase peak flows over those that occur in comparable rural areas. During greater flood events, they function less efficiently, and the difference between urban and rural flood peaks becomes smaller. The 25-year flood for a

60-percent urbanized basin in St. Louis County with an estimated 20-percent impervious area is about 2.5 times greater than the 2-year flood, whereas the same flood from a rural basin in the area is about 3.5 times greater than the 2-year flood. The average annual runoff for the same urbanized basin is about twice that of a comparable rural stream.

Flood problems will probably become more severe on tributary streams in the area as industrial and domestic development increase on the floodplains. The time distribution of floods will remain the same, barring major climatic changes, with most floods occurring in the 5-month period, March through July.

Springs in the study area are of little economic value because of their small and highly variable discharge. Some of the springs and seeps are becoming increasingly polluted as urbanization spreads, further limiting their value as a water supply.

The predominant chemical constituents of water in the Missouri River near St. Louis are calcium, magnesium, sodium, bicarbonate and sulfate. Variations in dissolved-solids content are primarily caused by variations in the amounts of these constituents. The water is hard and turbidity is relatively high. However, impoundments on the Missouri River main stem and tributaries over the past 20 years have resulted in a significant decrease in turbidity.

Water in the Mississippi River upstream from the mouth of the Missouri River is a calcium-bicarbonate type and contains significant amounts of magnesium and sulfate in the dissolved solids. Turbidity upstream from the Missouri River is relatively low and the water is very hard.

Water from the Meramec River is a CaCO_3 type. The water is hard, and turbidity is normally low.

Water from tributary streams in St. Charles County is primarily a calcium-bicarbonate type. Water from streams in Jefferson County contains significant amounts of magnesium in addition to calcium and bicarbonate. Fecal coliform to fecal streptococci bacteria ratios were higher in St. Charles County than in Jefferson County, indicating more contamination by human wastes.

The influence of urbanization on water quality of small streams is characterized by the generally deteriorated condition of the streams in St. Louis County, particularly those in the metropolitan St. Louis area.

GROUND WATER

Alluvial aquifers having the greatest potential for development are those underlying the floodplains of the Mississippi and Missouri Rivers. Wells capable of yielding more than 2,000 gpm can be constructed in much of this area. Larger sustained yields could be obtained by locating the wells so that infiltration would be induced from the river.

Wells capable of yielding 500 to 1,500 gpm can be developed at carefully selected sites in the alluvium bordering the Meramec River. Yields exceeding 500 gpm from wells in the Meramec River alluvium probably would require the installation of a well or wells capable of inducing infiltration from the river.

Little is known about the aquifer characteristics of the alluvium bordering the smaller perennial streams in the area, but it is doubtful whether a suitable supply could be developed unless a water-supply facility capable of inducing recharge from the stream could be installed. This installation would probably have to be an infiltration gallery or radial collector well.

Water from the Mississippi, Missouri and Meramec River alluvium generally is a calcium-magnesium-bicarbonate type. The water is very hard and contains significant quantities of iron and manganese. Locally, in the Meramec River alluvium such as at Valley Park and Times Beach, some wells yield a sodium-chloride type of water.

Wells yielding more than 50 gpm of potable water can be developed from the bedrock aquifers in the western third of St. Charles County, the extreme western part of St. Louis County, and the southwestern three-fourths of Jefferson County. The most important bedrock aquifers in the area are the Potosi Dolomite (5), Gasconade Dolomite (4), Roubidoux Formation (4) and St. Peter Sandstone (3).

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APPENDIX 1

GEOLOGIC LOGS OF SELECTED TEST HOLES IN ALLUVIUM

MERAMEC RIVER ALLUVIUM

JEFFERSON COUNTY

43 - 5 - 13 cbb Surface altitude: about 398 ft. Depth to water, 15 ft., June 12, 1968	Thick ness (feet)	Depth (feet)
Clay, silty, dark brown	7	7
Clay, silty, sandy, brown	5	12
Clay, silty, sandy; contains some gravel	15	27
Gravel and sand, medium to coarse	10	37
Gravel and sand, silty, brown; contains a few boulders	41	78
Bedrock	—	78

ST. LOUIS COUNTY

43 - 4 - 5bdd Surface altitude: about 430 ft. Depth to water, 30 ft., June 6, 1968	Thick ness (feet)	Depth (feet)
Silt, sandy, brown	2	2
Clay, silty, sandy, brown	10	12
Clay, sandy; contains trace of gravel	10	22
Sand, fine to medium, clayey, light brown	5	27
Sand, medium, silty, clayey, brown; contains some gravel	10	37
Sand, medium to coarse, silty, clayey; contains some gravel	20	57
Sand, coarse to very coarse; contains much gravel	4	61
Bedrock	—	61

43 - 3 - 4cdc Surface altitude: about 455 ft. Depth to water, 8 ft., June 5, 1968	Thick ness (feet)	Depth (feet)
Clay, dark gray	2	2
Clay, sandy, light brown to gray; contains some gravel	15	17
Sand, very fine to fine, clayey, tan to gray	10	27
Sand, fine to medium, gray	10	37
Sand, very fine to fine, gray to gray-brown; contains some gravel	20	57
Sand, medium; contains some gravel	3	60
Bedrock	—	60

44 - 5 - 23bbb Surface altitude: about 410 ft. Depth to water, 24 ft., Jan. 14, 1969	Thick ness (feet)	Depth (feet)
Sand, fine to medium, silty, tan	12	12
Sand, medium, silty, brown; contains some gravel	10	22
Sand, medium to coarse, brown; contains some gravel	10	32
Sand, medium to very coarse, silty, brown; contains gravel	25	57
Bedrock	—	57

44 - 5 - 35bba Surface altitude: about 410 ft. Depth to water, 17 ft., June 4, 1968	Thick ness (feet)	Depth (feet)
Clay, silty, dark brown	2	2
Clay, sandy, silty, dark brown	5	7
Sand, medium, clayey, brown	5	12
Sand, medium, silty, brown; contains gravel	5	17
Sand, fine to medium, clayey; contains gravel	5	22
Sand, medium, clayey; contains gravel	10	32
Sand, medium to coarse, clayey; contains much gravel	26	58
Bedrock	—	58

44 - 3 - 24dad Surface altitude: about 430 ft. Depth to water, 28 ft., June 7, 1968	Thick ness (feet)	Depth (feet)
Silt, clayey, brown	2	2
Clay, silty, sandy, brown	10	12
Sand, very fine to fine, silty, brown	30	42
Sand, fine to medium, silty, brown; contains some gravel	10	52
Sand, medium, some fine, silty, clayey, brown; contains some gravel	19	71
Bedrock	—	71

MISSISSIPPI RIVER ALLUVIUM

ST. CHARLES COUNTY

47 - 7 - 11ccb Surface altitude: about 410 ft. Depth to water, 7 ft., Oct. 28, 1969		Thick ness (feet)	Depth (feet)	47 - 5 - 14bca Surface altitude: about 430 ft.		Thick ness (feet)	Depth (feet)
Sand, fine, light tan	2	2		Sand, very fine to fine, brown	7	7	
Clay, sandy, dark brown	11	13		Clay, brown	16	23	
Sand, medium, clayey, dark brown	4	17		Sand, very fine to fine, silty, gray-brown	9	32	
Sand, medium to coarse, gray-brown	15	32		Sand, fine to medium, gray-brown	5	37	
Sand, coarse to very coarse, gray-brown; contains some gravel	90	122		Sand, medium to gray-brown	5	42	
				Sand, fine to very coarse, poorly sorted, gray-brown	10	52	
				Sand, coarse, gray-brown	20	72	
				Sand, coarse to very coarse; contains some gravel	25	97	
				Sand, very coarse, gray-brown; contains some gravel	12	109	
				Bedrock	—	109	
48 - 7 - 35abd Surface altitude: about 416 ft. Depth to water 9 ft., Jan. 23, 1969		Thick ness (feet)	Depth (feet)	44 - 1 - 14cab Surface altitude: about 468 ft. Depth to water, 14 ft., Feb. 10, 1967		Thick ness (feet)	Depth (feet)
Clay, silty, brown	17	17		Silt, clayey, dark brown	1	1	
Clay, silty, sandy, gray, brown	10	27		Silt, light brown	5	6	
Sand, very fine to fine, silty, gray-brown	15	42		Sand, very fine to fine, silty, clayey, brown	10	16	
Sand, very fine to very coarse, poorly sorted, gray-brown; contains some gravel	5	47		Sand, fine to medium, gray-brown	15	31	
Sand, medium to coarse; contains gravel	45	92		Sand, medium, gray-brown, some coarse, trace of very coarse sand	10	41	
Sand, coarse to very coarse, gray-brown; contains some gravel	16	108		Sand, medium to coarse, gray-brown, some very coarse sand, some very fine gravel	10	51	
Gravel and boulders	1	109		Sand, medium, gray-brown, some coarse to very coarse sand, contains some gravel from 62-66 ft.	29	80	
Bedrock	—	109		Bedrock	—	80	
48 - 6 - 15ada Surface altitude: about 423 ft. Depth to water, 3 ft., Feb. 6, 1969		Thick ness (feet)	Depth (feet)	44 - 1 - 23cab Surface altitude: about 471 ft. Depth to water, 18 ft., Feb. 10, 1967		Thick ness (feet)	Depth (feet)
Clay, dark gray	15	15		Clay, silty, brown	1	1	
Silt, clayey, sandy, dark gray; contains gravel	12	27		Sand, fine, tan, some very fine	8	9	
Sand, fine to medium, dark gray	10	37		Clay, dark brown	2	11	
Sand, medium to coarse, gray; contains some gravel	5	42		Sand, fine to medium, light brown, trace of very coarse	15	26	
Sand, very coarse, gray; contains much gravel	5	47		Sand, medium, gray-brown, some coarse, some fine; gravel lens from 37 to 39 ft.	15	41	
Sand, coarse, silty, gray; contains some gravel	45	92		Sand, medium to coarse, some very coarse sand, some very fine gravel	15	56	
Sand, coarse to very coarse, gray-brown; contains gravel	10	102		Sand, coarse to very coarse, some medium sand, some very fine to fine gravel	5	61	
Sand and gravel	8	110		Sand, very coarse, and very fine gravel	44	105	
Bedrock	—	110		Bedrock	—	105	
48 - 6 - 22ada Surface altitude: about 440 ft. Depth to water, 21 ft., Feb. 6, 1969		Thick ness (feet)	Depth (feet)				
Clay, silty, gray	2	2					
Silt, sandy, clayey, brown	10	12					
Sand, very fine to fine, silty, brown	15	27					
Sand, fine to medium, brown	5	32					
Sand, medium to coarse, brown	5	37					
Sand, coarse to very coarse, brown; contains trace of gravel	5	42					
Sand, medium to coarse, gray-brown	10	52					
Sand, fine to medium, gray	20	72					
Sand, medium to coarse, gray; contains trace of gravel	5	77					
Sand, coarse to very coarse, gray-brown; contains gravel	25	102					
Sand, medium to coarse; contains some gravel	20	122					

ST. LOUIS COUNTY

47 - 5 - 28ddd		Thick	Depth
Surface altitude: about 437 ft.		ness	(feet)
Depth to water, 17 ft., Feb. 10, 1967		(feet)	
Clay, silty, gray-brown	4	4	
Silt, light gray-brown	6	10	
Sand, medium, light brown	16	26	
Sand, medium to coarse, gray-brown, some very coarse, trace of very fine gravel	20	46	
Sand, medium to very coarse, gray-brown, trace of very fine to fine gravel	15	61	
Sand, coarse to very coarse, gray-brown, some medium sand, some very fine to medium gravel	10	71	
Sand, very coarse, gray-brown, some medium to coarse sand, much very fine gravel, some fine to medium gravel	45	116	
Bedrock	—	116	

47 - 5 - 29 dbd		Thick	Depth
Surface altitude: about 440 ft.		ness	(feet)
Depth to water, 24 ft., Feb. 10, 1967		(feet)	
Sand, very fine to fine, silty, brown	11	11	
Sand, medium, light tan	10	21	
Sand, medium to coarse, tan, some very coarse sand from 26 to 36 feet	15	36	
Sand, coarse, some medium, some very coarse, trace of very fine gravel	20	56	
Sand, very coarse, gray-brown, some medium to coarse sand, much very fine to fine gravel	10	66	
Sand, very coarse, much very fine gravel, some medium to coarse sand, some gravel 1 inch long	30	96	
Bedrock	—	96	

Table 1

Selected analyses of water from bedrock wells in St. Louis area by aquifer group

Well number	Depth (feet)	Date of collection	Temperature (°C)	Milligrams per liter															Specific conductance (Microhmoh at 25°C)	pH	Color	
				Silica (SiO ₂)	Iron (Fe)	Manganese (Mn)	Calcium (Ca)	Magnesium (Mg)	Sodium (Na)	Potassium (K)	Bicarbonate (HCO ₃)	Carbonate (CO ₃)	Sulfate (SO ₄)	Chloride (Cl)	Fluoride (F)	Nitrate (NO ₃)	Dissolved solids (residue at 180°C)	Hardness as CaCO ₃				
																		Calcium Magnesium				Noncarbonate
Group 1 (post-Maquoketa) Aquifers																						
43-6-31 dab	301	12-19-60	--	4.8	0.23	----	81	45	11	----	466	0	11	4.0	0.3	0.0	404	387	4	--	--	
44-6-31 ccb	409	6-11-41	--	12	----	----	262	131	1310	----	339	0	262	2,360	----	----	5,050	1190	913	--	--	
45-4-12 cdd	383	5-17-35	--	10	.05	----	40	27	48	0.0	216	0	26	22	3.2	2.0	372	211	----	--	--	
46-2-1 bcb	220	3-7-61	--	4.2	.13	----	65	28	14	----	331	4	11	1.5	.1	----	311	275	0	--	--	
46-6-35 ddc	790	9-20-38	--	6.8	.14	----	211	120	1560	----	305	0	267	2,670	----	----	5,400	1020	770	--	--	
46-7-20 dbc	655	2-27-36	--	6.0	.12	----	45	25	124	----	416	3	84	36	3.0	.0	558	214	----	--	--	
47-6-34 bac	513	1-27-38	--	8.4	.12	----	30	16	246	----	396	1	296	34	3.8	3.5	916	139	----	--	--	
Group 2 (Kimmerwick-Joachim) Aquifers																						
44-5-20 adb	365	4-26-41	--	5.6	----	----	74	26	23	----	339	0	49	14	----	----	424	290	12	--	--	
46-1-15 cdb	370	3-3-61	--	4.2	.16	----	62	39	27	----	354	14	15	5.0	.7	1.2	355	313	----	--	--	
46-4-17 bcb	810	3-28-61	--	16	1.0	----	124	74	1120	----	340	0	357	1,740	2.5	.1	4,070	618	337	--	--	
46-5-2 cb	915	6-1-34	--	19	.20	----	94	41	12	----	454	13	6.4	6.2	----	7.4	459	403	----	--	--	
47-7-35 dca	1300	-----	--	4.0	4.5	----	252	188	5960	----	347	0	23	10,000	----	.4	17,500	----	----	--	--	
48-6-22 acm	619	2-16-34	--	1.2	.10	----	125	82	1220	----	131	5	376	1,900	----	.5	4,710	649	542	--	--	
Group 3 (St. Peter-Everton) Aquifers																						
39-7-6 dba	181	11-27-60	--	7.7	.11	----	106	56	25	----	376	0	124	8.3	.3	4.6	604	497	106	--	--	
42-4-5 bab	185	1-6-61	--	5.6	.14	----	83	31	3.5	----	379	6	11	2.8	----	----	335	335	14	--	--	
42-5-23 dd	150	2-3-61	--	3.3	.15	----	78	28	2.6	----	359	0	7.8	2.0	.3	0	311	309	14	--	--	
43-5-4 bdb	800	5-9-62	--	8.0	.04	----	46	25	9.8	----	252	0	19	12	.7	.1	270	216	12	--	--	
45-3-7 dbb	535	3-7-61	--	6.8	.09	----	85	35	17	----	366	14	17	13	.3	16	420	358	34	--	--	
44-4-1 add	798	2-25-37	--	8.8	.15	----	325	149	1810	----	267	--	442	3,320	----	0	7,270	1,420	----	--	--	
47-1-19 abc	770	7-30-68	--	8.0	.04	----	68	35	40	9.6	420	0	70	7.9	.7	----	478	313	0	--	--	
47-3-25 dcd	820	12-7-67	--	7.0	.85	----	66	35	200	11	349	0	56	291	1.5	0	915	307	21	--	--	
48-2-35 add	810	5-18-34	--	8.0	.60	----	6.5	3.4	290	----	456	40	150	28	----	16	777	30	----	--	--	
Group 4 (Powell-Gasconade) Aquifers																						
39-4-1 bcb	185	11-16-60	--	9.7	.08	----	161	116	22	----	597	0	386	12	0	11	1,110	881	391	--	--	
41-2-13 cdb	305	12-10-60	--	7.5	.07	----	70	43	6	----	389	7	12	3.5	----	.1	352	350	19	--	--	
42-6-30 adc	562	12-7-36	--	12	.12	----	141	92	753	----	134	0	128	1,580	.1	----	3,100	730	620	--	--	
43-3-18 ccd	585	9-5-61	--	5.0	.08	----	68	36	13	----	348	0	16	2.5	.1	0	314	316	30	--	--	
44-1-11 dcd	352	3-3-61	--	18	.20	----	104	54	37	----	516	0	48	25	.1	9.7	600	484	61	--	--	
44-3-35 daa	820	1-18-63	--	6.3	1.6	----	80	36	27	----	309	24	23	44	.2	0	422	350	56	--	--	
44-5-16 abd	1345	6-1-34	--	8.0	.20	----	464	187	2570	----	250	8	563	4,370	2.8	.1	4,650	1,930	----	--	--	
45-3-29 acc	1072	6-12-40	--	4.0	----	----	52	27	14	----	295	4	22	6.5	----	----	324	238	----	--	--	
47-2-19 cca	1337	1-7-63	--	6.0	4.0	----	63	28	37	4.0	341	--	45	24	.8	.1	406	274	----	--	--	
47-3-20 ada	1500	8-18-66	--	8.0	.01	----	47	25	100	8.8	364	0	68	43	1.1	1.2	561	220	----	--	--	
Group 5 (Emmence-Lamotte) Aquifers																						
39-3-14 baa	350	11-28-60	--	5.5	0.06	----	68	38	26	----	336	12	51	11	0.5	0.2	387	327	31	--	--	
39-5-31 caa	800	6-12-63	--	6.0	.20	----	70	41	2.3	1.2	403	0	18	4.8	.1	----	406	344	13	--	--	
40-6-6 cdb	865	-----	--	8.0	.04	----	61	32	2.9	2.0	310	--	18	3.7	----	.4	337	284	30	--	--	
41-4-27 ddb	1100	8-10-65	--	----	.30	----	68	44	7.4	1.5	403	0	--	8.1	.1	.3	----	350	20	--	--	
47-6-18 add	2755	9-23-40	--	8.4	----	----	283	112	1620	----	302	0	478	2,690	2.1	----	6,060	1170	921	--	--	

APPENDIX 2

Table 2

Selected analyses of water from wells in alluvial deposits in St. Charles, St. Louis, and Jefferson Counties, Missouri

Well number	Depth	Date of collection	Temperature (°C)	milligrams per liter														Hardness as CaCO ₃		Specific conductance (micromhos at 25°C)	pH	Color	
				Silica (SiO ₂)	Iron (Fe)	Manganese (Mn)	Calcium (Ca)	Magnesium (Mg)	Sodium (Na)	Potassium (K)	Bicarbonate (HCO ₃)	Carbonate (CO ₃)	Sulfate (SO ₄)	Chloride (Cl)	Fluoride (F)	Nitrate (NO ₃)	Dissolved solids (residue at 180°C)	Calcium Magnesium	Noncarbonate				
Meramec River Alluvium																							
43-3-10 bdc	37	6-6-68	14	11	2.2	0.50	86	16	6.5	0.8	342	C	10	6.2	0.2	0.0	321	281	0	559	7.7	7	
43-3-11 cdd	24	6-6-68	13	9.1	1.9	.32	150	20	4.0	1.4	478	C	58	5.8	.0	.4	486	456	64	765	7.8	3	
43-3-22 daa	42	6-5-68	16	11	7.5	1.6	20	9.3	5.0	1.2	100	C	13	2.7	.2	.0	122	88	6	210	7.1	7	
44-4-31 dca	40	6-6-68	14	12	1.9	1.4	77	32	50	2.5	376	C	33	72	.2	.0	476	324	16	837	7.7	3	
44-4-14 ccc	42	6-7-68	13	11	.11	.00	60	18	28	1.8	212	C	39	47	.1	9.3	337	224	50	569	7.4	5	
44-5-10 ccc	53	6-4-68	14	8.9	.70	1.3	56	15	42	3.4	185	C	72	54	.1	.0	351	201	50	593	7.4	5	
Mississippi and Missouri Rivers Alluvium																							
44-5-17 cdb	63	8-27-69	14	12	.34	.61	87	26	140	4.6	158	C	108	277	.1	.0	742	324	195	1290	7.6	2	
44-5-18 dda	62	8-27-69	13.5	13	.00	.33	57	16	26	2.2	158	C	88	32	.0	4.2	331	208	78	536	7.5	2	
44-5-27 bad	58	6-4-68	15	10	3.6	1.2	98	33	9.4	1.4	403	C	62	8.4	.3	.5	438	380	50	747	7.7	3	
43-5-13 cab	48	6-11-68	----	9.2	3.4	.80	51	14	25	1.8	212	C	32	24	.0	.3	283	185	11	467	7.4	2	
43-5-1 ccd	43	6-7-68	12	9.1	.10	.00	36	15	7.7	.9	132	C	34	18	.1	4.8	201	152	44	391	7.3	5	
Mississippi and Missouri Rivers Alluvium																							
44-1-23 cab	46	2-3-67	15	26	2.8	2.7	172	38	11	5.3	662	C	55	2.4	.2	.0	641	586	42	1020	7.1	0	
44-3-15 bbc	47	10-30-69	13	17	5.7	.82	107	20	16	1.0	386	C	46	15	.2	.0	419	349	32	689	7.6	1	
47-4-23 bdd	100	10-30-69	13	37	8.7	.39	95	37	16	2.0	508	C	54	1.7	.3	4.1	452	389	0	734	7.6	5	
47-5-2 bdd	46	10-29-69	14	24	1.0	.15	46	10	4.0	2.6	184	C	17	.5	.5	2.8	205	156	5	316	7.8	0	
47-7-13 dcc	46	10-27-69	14	24	10	.80	133	31	7.0	3.9	512	C	70	2.0	.3	.1	552	460	40	872	8.0	5	
47-8-20 aad	50	10-27-69	14	30	29	2.1	169	47	16	5.4	784	C	1.6	3.8	.2	.3	690	616	0	1070	8.1	10	
48-2-12 bbd	39	10-30-69	13.5	24	8.0	.97	90	20	11	1.0	312	C	72	7.0	.2	.0	388	307	51	618	7.3	2	
48-3-16 bd	89	10-30-69	13.5	29	14	1.1	76	17	9.2	1.3	316	C	7.2	5.9	.2	1.0	304	260	0	504	7.5	2	
48-5-23 bad	56	10-28-69	12	27	9.3	1.2	93	23	8.2	4.6	340	C	53	4.6	.4	.2	392	327	48	884	8.1	15	
48-6-15 bcb	116	10-28-69	14	27	7.6	.18	120	32	11	4.6	544	C	13	3.2	.3	2.8	489	431	0	808	8.1	5	
48-7-20 cac	47	10-28-69	13	27	4.8	.53	118	26	4.3	4.6	460	C	25	3.2	.2	1.1	441	402	24	716	8.2	5	
49-5-34 ddd	52	10-30-69	12	30	9.7	.62	82	17	8.8	1.9	325	C	28	.9	.2	.5	339	275	8	526	8.0	35	

APPENDIX 3

STREAMFLOW STATISTICS AND FLOW-VARIABILITY DATA FOR MISSISSIPPI AND MISSOURI RIVER STATIONS

Statistical and flow-variability data are presented so that water managers and planners will have values of daily streamflow in a form which is readily adaptable to their needs.

Further analysis of these data was not justified at this time. However, future research plans of the Water Resources Division include systems analyses of the Mississippi and Missouri basins.

Scientific notation (for example, $0.036 = 0.36 \times 10^{-1}$) is used in the statistics of monthly and annual means. In this format a decimal is always placed immediately to the left of the first digit in the mantissa, with the two digits immediately after the "E" indicating the exponent of 10 needed to compute the correct data value. The following examples illustrate the use of the "E" format:

$$\begin{aligned} -0.424 \text{ E } -01 &= -0.424 \times 10^{-1} = -0.0424 \\ 0.424 \text{ E } -01 &= 0.424 \times 10^{-1} = 0.0424 \\ 0.424 \text{ E } 00 &= 0.424 \times 10^0 = 0.424 \\ 0.424 \text{ E } 01 &= 0.424 \times 10^1 = 4.24 \end{aligned}$$

The lowest and highest mean discharges for each year and their ranking are shown for each of the three stations in this appendix. The order numbers are included for the convenience of the user who may want to construct frequency curves for these stations. Note that climatic year data (April 1 - March 31) used in computation of lowest mean discharges and water year data (October 1 - September 30) are used in computation of highest-mean-discharge data.

Tables of duration of daily discharges are shown for each station. A cumulative frequency curve (flow-duration curve) showing the percent of time during which specified discharges were exceeded in a given period may be plotted from these data. Logarithmic probability paper is recommended for these plots because it tends to straighten the flow-duration curve.

MISSISSIPPI RIVER AT ALTON, ILL. 06687500

STATISTICS ON NORMAL MONTHLY MEANS(ALL DAYS)

BY ROWS (MEAN, VARIANCE, STANDARD DEVIATION, SKEWNESS, COEFF. OF VARIATION, PERCENTAGE OF AVERAGE FLOW, FIRST ORDER SERIAL CORRELATION COEFF.)

DEC	NOV	DEC	JAN	FEB	MARCH	APRIL	MAY	JUNE	JULY	AUG	SEPT
0.5726F 05	0.6108F 05	0.5332F 05	0.6088F 05	0.7309F 05	0.1227E 0A	0.1726E 0A	0.1538F 0A	0.1337F 0A	0.1039F 0A	0.6108F 05	0.5700F 05
0.1402F 10	0.1375E 10	0.4394F 09	0.10A3E 10	0.9580F 09	0.2532F 10	0.4330F 10	0.4365E 10	0.4161F 10	0.2414F 10	0.5500F 09	0.7003F 09
0.3744F 05	0.3708F 05	0.2096E 05	0.3260E 05	0.3095F 05	0.5032F 05	0.6581F 05	0.6607F 05	0.6450F 05	0.4913F 05	0.2345F 05	0.2644F 05
0.1859F 01	0.1872F 01	0.8341F 00	0.1539E 01	0.2897E 00	0.6154E-01	0.4287E 00	0.5181E 00	0.9636F 00	0.8350E 00	0.6490F 00	0.1782F 01
0.6540F 00	0.6070E 00	0.3931E 00	0.5354E 00	0.4235E 00	0.4100E 00	0.3812E 00	0.4297E 00	0.4826E 00	0.4730F 00	0.3840F 00	0.4642E 00
0.5155F 01	0.5501F 01	0.4802F 01	0.5483E 01	0.6583F 01	0.1105E 02	0.1555E 02	0.1385E 02	0.1204F 02	0.9353E 01	0.5501F 01	0.5134E 01

STATISTICS ON NORMAL ANNUAL MEANS(ALL DAYS)

MEAN	VARIANCE	STANDARD DEVIATION	SKEWNESS	COEFF. OF VARIATION	SERIAL CORR
0.9252F 05	0.7858E 09	0.2803F 05	0.1993E-01	0.3030F 00	0.2388E 00

MISSOURI RIVER AT HERMANN, MO. 06934500

STATISTICS ON NORMAL MONTHLY MEANS(ALL DAYS)

BY ROWS (MEAN, VARIANCE, STANDARD DEVIATION, SKEWNESS, COEFF. OF VARIATION, PERCENTAGE OF AVERAGE FLOW, FIRST ORDER SERIAL CORRELATION COEFF.)

DEC	NOV	DEC	JAN	FEB	MARCH	APRIL	MAY	JUNE	JULY	AUG	SEPT
0.5122F 05	0.5095F 05	0.3367E 05	0.3492E 05	0.4754E 05	0.7767E 05	0.1057E 0A	0.9970E 05	0.1228E 0A	0.9624E 05	0.5586F 05	0.5631F 05
0.8594F 09	0.1028F 10	0.2456F 09	0.3191F 09	0.6272F 09	0.1538F 10	0.4076E 10	0.2716E 10	0.5363E 10	0.4885F 10	0.6737F 09	0.1334E 10
0.2932F 05	0.3206F 05	0.1567E 05	0.1786E 05	0.2504E 05	0.3921E 05	0.6384E 05	0.5212E 05	0.7323F 05	0.6989E 05	0.2596E 05	0.3653E 05
0.2254F 01	0.1687F 01	0.9223F 00	0.8141F 00	0.1337F 01	0.8428E 00	0.1222E 01	0.1017E 01	0.1281F 01	0.3376E 01	0.1512E 01	0.2774E 01
0.5724F 00	0.6293F 00	0.4654E 00	0.5115E 00	0.5267E 00	0.5049E 00	0.6039F 00	0.5227E 00	0.5964E 00	0.7262E 00	0.4646F 00	0.6488F 00
0.6151E 01	0.6119E 01	0.4044F 01	0.4194F 01	0.5710F 01	0.9328F 01	0.1270E 02	0.1197E 02	0.1475F 02	0.1154E 02	0.6710F 01	0.6763E 01

STATISTICS ON NORMAL ANNUAL MEANS(ALL DAYS)

MEAN	VARIANCE	STANDARD DEVIATION	SKEWNESS	COEFF. OF VARIATION	SERIAL CORR
0.6939F 05	0.6849E 09	0.2617E 05	0.5932E 00	0.3772F 00	0.4023E 00

MISSISSIPPI RIVER AT ST. LOUIS, MO. 07010000

STATISTICS ON NORMAL MONTHLY MEANS(ALL DAYS)

BY ROWS (MEAN, VARIANCE, STANDARD DEVIATION, SKEWNESS, COEFF. OF VARIATION, PERCENTAGE OF AVERAGE FLOW, FIRST ORDER SERIAL CORRELATION COEFF.)

DEC	NOV	DEC	JAN	FEB	MARCH	APRIL	MAY	JUNE	JULY	AUG	SEPT
0.1131F 0A	0.1121F 0A	0.8669E 05	0.9620E 05	0.1229E 06	0.2006E 06	0.2808E 06	0.2521E 06	0.2558F 0A	0.2065F 0A	0.1218F 0A	0.1182E 0A
0.3908F 10	0.4180F 10	0.1096E 10	0.2406E 10	0.2908E 10	0.6577E 10	0.1366E 11	0.1081E 11	0.1488E 11	0.1185F 11	0.1737E 10	0.3573E 10
0.6251F 05	0.6465F 05	0.3311E 05	0.4905F 05	0.5392E 05	0.8110E 05	0.1169E 06	0.1040E 06	0.1220F 0A	0.1089E 0A	0.4163E 05	0.5977E 05
0.1907F 01	0.2019F 01	0.8313E 00	0.1260E 01	0.4990E 00	0.8266E-01	0.6386E 00	0.6612E 00	0.1131E 01	0.2148E 01	0.7594E 00	0.2046E 01
0.5526F 00	0.5767E 00	0.3820E 00	0.5098E 00	0.4388E 00	0.4043E 00	0.4162E 00	0.4124E 00	0.4767F 00	0.5272F 00	0.3423F 00	0.5056F 00
0.5751F 01	0.5700F 01	0.4407E 01	0.4891E 01	0.6248F 01	0.1020E 02	0.1428E 02	0.1282E 02	0.1301E 02	0.1050F 02	0.6192F 01	0.6011F 01

STATISTICS ON NORMAL ANNUAL MEANS(ALL DAYS)

MEAN	VARIANCE	STANDARD DEVIATION	SKEWNESS	COEFF. OF VARIATION	SERIAL CORR
0.1639E 06	0.2487E 10	0.4987E 05	0.1025E 00	0.3043F 00	0.3487E 00

APPENDIX 3 (continued)

Appendix 3

APPENDIX 3 (continued)

MISSISSIPPI RIVER AT ALTON, ILL. 05587500

LOWEST MEAN DISCHARGE, IN CFS, AND RANKING, FOR THE FOLLOWING NUMBER OF CONSECUTIVE DAYS IN YEAR ENDING MARCH 31

YEAR	15000 ¹	1	15800 ³	1	19600 ⁷	1	22600 ¹⁴	4	25100 ³⁰	4	27700 ⁶⁰	5	29100 ⁹⁰	3	30000 ¹²⁰	2	30800 ¹⁸³	2	ANNUAL	7
1934	15000.0	1	15800.0	1	19600.0	1	22600.0	4	25100.0	4	27700.0	5	29100.0	3	30000.0	2	30800.0	2	70500.0	7
1935	23900.0	14	24100.0	13	25700.0	11	27700.0	13	29600.0	11	32500.0	11	33000.0	6	33600.0	6	37700.0	8	61900.0	5
1936	27200.0	19	28500.0	18	31000.0	21	32900.0	21	34800.0	19	36800.0	18	41000.0	19	46600.0	21	46100.0	16	100000.0	19
1937	21600.0	10	21600.0	9	21700.0	7	21900.0	2	22300.0	2	25300.0	1	30400.0	5	41100.0	17	42200.0	11	79000.0	11
1941	25300.0	15	25800.0	15	27200.0	15	28300.0	15	30400.0	14	30900.0	8	35900.0	14	40800.0	16	44300.0	13	56900.0	3
1942	21000.0	9	21900.0	10	26200.0	12	26600.0	11	28600.0	9	38300.0	20	58700.0	25	68300.0	27	93900.0	28	113000.0	23
1943	48100.0	31	49000.0	31	50100.0	31	54900.0	31	71500.0	31	83100.0	30	86200.0	30	89200.0	29	95000.0	29	121000.0	27
1944	30600.0	25	31100.0	24	35100.0	25	37400.0	24	40300.0	24	43500.0	23	44200.0	21	46400.0	20	49600.0	21	120000.0	26
1945	30200.0	23	30600.0	23	31700.0	23	33300.0	22	34900.0	21	37200.0	19	38800.0	17	39400.0	14	44700.0	15	114000.0	24
1946	41100.0	30	43100.0	30	45900.0	30	47300.0	29	52000.0	29	58700.0	27	59900.0	26	66600.0	25	71300.0	25	135000.0	29
1947	34400.0	26	36300.0	27	37100.0	26	42200.0	26	51900.0	28	55300.0	25	58200.0	23	65600.0	24	70100.0	23	92000.0	16
1948	28000.0	20	28300.0	17	28700.0	16	29900.0	17	34800.0	20	39500.0	21	41000.0	20	42200.0	18	44600.0	14	128000.0	28
1949	15800.0	2	17600.0	2	22500.0	9	23500.0	6	25200.0	5	26500.0	3	28500.0	2	30000.0	3	38200.0	10	80200.0	13
1950	19000.0	6	20400.0	7	21600.0	6	23500.0	7	30800.0	15	33100.0	12	35100.0	12	35100.0	8	47400.0	18	79200.0	12
1951	22500.0	11	22900.0	11	24100.0	10	26400.0	10	28500.0	8	30400.0	7	33600.0	8	35400.0	9	37800.0	9	97900.0	18
1952	35400.0	28	39300.0	29	45100.0	29	52400.0	30	70200.0	30	85000.0	31	93000.0	31	95800.0	31	98200.0	30	153000.0	31
1953	25700.0	16	29000.0	20	29300.0	18	31000.0	18	32900.0	17	34800.0	15	38300.0	16	40000.0	15	47300.0	17	103000.0	21
1954	27100.0	18	27200.0	16	28900.0	17	29300.0	16	30100.0	12	32300.0	9	34800.0	11	36200.0	10	36800.0	5	75300.0	9
1955	36700.0	29	38800.0	28	43100.0	28	46600.0	28	50100.0	26	57900.0	26	61400.0	28	66800.0	26	71800.0	26	95500.0	17
1956	23800.0	13	25200.0	14	26300.0	14	27800.0	14	31200.0	16	33700.0	14	34300.0	9	34600.0	7	36400.0	4	61200.0	4
1957	17400.0	3	18800.0	3	19600.0	2	20500.0	1	21800.0	1	24400.0	2	29400.0	4	31300.0	4	35000.0	3	56600.0	2
1958	30200.0	24	31300.0	25	32900.0	24	33500.0	23	37200.0	22	42500.0	22	45400.0	22	46800.0	22	48400.0	20	79000.0	10
1959	18500.0	5	19600.0	4	22100.0	8	25400.0	9	28300.0	7	29200.0	6	33500.0	7	32500.0	5	37500.0	6	71600.0	8
1960	28400.0	22	29900.0	21	31200.0	22	38500.0	25	51100.0	27	51200.0	24	58600.0	24	64500.0	23	70900.0	24	90100.0	15
1961	26800.0	17	28600.0	19	30800.0	19	31800.0	19	33100.0	18	35700.0	17	39800.0	18	43900.0	19	47900.0	19	114000.0	25
1962	28200.0	21	30400.0	22	30800.0	20	32700.0	20	40200.0	23	60800.0	28	60500.0	27	72800.0	28	89400.0	27	110000.0	22
1963	23400.0	12	24100.0	12	26200.0	13	26700.0	12	29200.0	10	33500.0	13	35600.0	13	38500.0	12	49900.0	22	101000.0	20
1964	19200.0	7	19900.0	5	21500.0	5	22600.0	5	23200.0	3	26800.0	4	27300.0	1	27200.0	1	29000.0	1	51200.0	1
1965	17800.0	4	19900.0	6	20700.0	3	22200.0	3	27000.0	6	32300.0	10	34500.0	10	36300.0	11	37700.0	7	68100.0	6
1966	35100.0	27	36100.0	26	41300.0	27	43000.0	27	45400.0	25	63000.0	29	79000.0	29	90000.0	30	98500.0	31	141000.0	30
1967	19200.0	8	20900.0	8	21500.0	4	23600.0	8	30300.0	13	35300.0	16	36000.0	15	38900.0	13	42300.0	12	82400.0	14

MISSISSIPPI RIVER AT ALTON, ILL. 05587500

HIGHEST MEAN DISCHARGE, IN CFS, AND RANKING, FOR THE FOLLOWING NUMBER OF CONSECUTIVE DAYS IN YEAR ENDING SEPTEMBER 30

YEAR	1	3	7	15	30	60	90	120	183	ANNUAL
1934	97200.0 32	96800.0 32	94700.0 32	88800.0 32	75800.0 32	58900.0 32	52100.0 32	47100.0 32	42900.0 32	37200.0 32
1935	231000.0 19	228000.0 19	216000.0 19	203000.0 19	199000.0 15	180000.0 16	172000.0 13	170000.0 11	150000.0 11	107000.0 13
1936	218000.0 22	209000.0 23	189000.0 25	181000.0 24	176000.0 20	168000.0 18	156000.0 18	137000.0 19	103000.0 24	72700.0 25
1937	253000.0 15	251000.0 14	240000.0 15	208000.0 17	176000.0 21	153000.0 22	155000.0 19	145000.0 17	125000.0 16	86500.0 15
1940	128000.0 31	114000.0 31	102000.0 31	96700.0 31	87600.0 31	77300.0 31	77000.0 31	71100.0 31	64600.0 31	47200.0 31
1941	219000.0 20	214000.0 22	207000.0 22	194000.0 20	170000.0 23	140000.0 24	129000.0 25	117000.0 26	95600.0 26	72800.0 24
1942	253000.0 16	248000.0 15	241000.0 14	230000.0 14	202000.0 14	183000.0 14	160000.0 16	161000.0 13	150000.0 12	133000.0 2
1943	434000.0 1	416000.0 1	387000.0 1	336000.0 5	296000.0 6	268000.0 6	244000.0 5	227000.0 4	191000.0 2	142000.0 1
1944	392000.0 2	386000.0 2	371000.0 3	343000.0 3	295000.0 7	274000.0 5	256000.0 2	233000.0 3	182000.0 4	115000.0 9
1945	307000.0 11	303000.0 11	296000.0 11	284000.0 10	265000.0 9	238000.0 9	239000.0 6	223000.0 7	175000.0 7	112000.0 10
1946	313000.0 10	311000.0 10	299000.0 10	266000.0 11	241000.0 11	185000.0 13	167000.0 14	160000.0 14	148000.0 13	109000.0 12
1947	378000.0 4	374000.0 4	362000.0 4	360000.0 2	351000.0 2	281000.0 2	274000.0 1	249000.0 1	188000.0 3	127000.0 6
1948	362000.0 6	359000.0 6	348000.0 6	316000.0 9	264000.0 10	215000.0 10	187000.0 11	156000.0 16	123000.0 18	82500.0 20
1949	218000.0 23	217000.0 21	211000.0 21	193000.0 22	178000.0 19	167000.0 19	146000.0 20	131000.0 23	111000.0 21	75200.0 22
1950	256000.0 13	252000.0 13	250000.0 13	242000.0 13	225000.0 12	208000.0 11	195000.0 10	186000.0 10	158000.0 10	106000.0 14
1951	330000.0 9	328000.0 9	323000.0 9	319000.0 7	316000.0 3	276000.0 4	237000.0 7	238000.0 2	208000.0 1	130000.0 3
1952	337000.0 7	337000.0 7	335000.0 7	321000.0 6	293000.0 8	258000.0 7	223000.0 9	200000.0 8	168000.0 8	130000.0 4
1953	232000.0 18	229000.0 18	217000.0 18	194000.0 21	172000.0 22	154000.0 20	141000.0 23	136000.0 21	124000.0 17	85300.0 16
1954	196000.0 27	195000.0 26	193000.0 24	183000.0 23	163000.0 24	152000.0 23	145000.0 21	133000.0 22	108000.0 22	72900.0 23
1955	207000.0 24	205000.0 24	200000.0 23	176000.0 25	151000.0 25	130000.0 26	126000.0 26	119000.0 25	103000.0 25	83300.0 19
1956	162000.0 30	152000.0 30	140000.0 30	136000.0 30	126000.0 30	110000.0 30	95500.0 30	87800.0 30	77600.0 29	57200.0 29
1957	174000.0 29	166000.0 29	147000.0 29	137000.0 29	135000.0 28	132000.0 25	130000.0 24	127000.0 24	105000.0 23	71200.0 26
1958	204000.0 25	201000.0 25	181000.0 26	156000.0 27	145000.0 27	127000.0 27	106000.0 28	96900.0 28	90000.0 27	68500.0 27
1959	219000.0 21	218000.0 20	214000.0 20	207000.0 18	181000.0 18	154000.0 21	142000.0 22	137000.0 20	113000.0 20	76000.0 21
1960	374000.0 5	371000.0 5	362000.0 5	338000.0 4	302000.0 5	278000.0 3	251000.0 4	224000.0 5	178000.0 5	127000.0 7
1961	245000.0 17	242000.0 17	232000.0 16	211000.0 15	184000.0 17	170000.0 17	158000.0 17	139000.0 18	115000.0 19	84000.0 18
1962	336000.0 8	334000.0 8	329000.0 8	316000.0 8	305000.0 4	254000.0 8	226000.0 8	199000.0 9	167000.0 9	129000.0 5
1963	177000.0 28	174000.0 28	164000.0 28	161000.0 26	150000.0 26	125000.0 28	120000.0 27	107000.0 27	87600.0 28	64600.0 28
1964	204000.0 26	193000.0 27	166000.0 27	150000.0 28	134000.0 29	116000.0 29	100000.0 29	88900.0 29	70800.0 30	51200.0 30
1965	380000.0 3	378000.0 3	376000.0 2	365000.0 1	359000.0 1	295000.0 1	252000.0 3	224000.0 6	176000.0 6	118000.0 8
1966	256000.0 14	243000.0 16	228000.0 17	211000.0 16	189000.0 16	185000.0 12	178000.0 12	166000.0 12	146000.0 14	111000.0 11
1967	264000.0 12	262000.0 12	258000.0 12	244000.0 12	223000.0 13	182000.0 15	165000.0 15	159000.0 15	128000.0 15	84900.0 17

APPENDIX 3 (continued)

MISSISSIPPI RIVER AT ALTON, ILL. 05587500

DURATION TABLE OF DAILY DISCHARGE FOR YEAR ENDING SEPTEMBER 30

CLASS	CFS	TOTAL	ACCUM	PERCT	CLASS	CFS	TOTAL	ACCUM	PERCT	CLASS	CFS	TOTAL	ACCUM	PERCT	CLASS	CFS	TOTAL	ACCUM	PERCT
0	C.CC	0	11688	100.0	9	34000.00	550	10099	86.4	18	84000.0	406	4854	41.5	27	210000	221	836	7.1
1	15000.00	7	11688	100.0	10	37000.00	683	9549	81.7	19	92000.0	414	4448	38.1	28	230000	176	615	5.2
2	17000.00	4	11681	99.9	11	41000.00	757	8866	75.9	20	100000.0	440	4034	34.5	29	250000	170	439	3.7
3	18000.00	17	11677	99.9	12	46000.00	511	8109	69.4	21	110000.0	880	3594	30.7	30	280000	101	269	2.3
4	20000.00	77	11660	99.8	13	50000.00	612	7598	65.0	22	130000.0	372	2714	23.2	31	310000	91	168	1.4
5	22000.00	181	11583	99.1	14	56000.00	567	6986	59.8	23	140000.0	285	2342	20.0	32	340000	69	77	.6
6	25000.00	274	11402	97.6	15	62000.00	487	6419	54.9	24	150000.0	447	2057	17.6	33	380000	6	8	.0
7	28000.00	271	11128	95.2	16	68000.00	573	5932	50.8	25	170000.0	439	1610	13.8	34	420000	2	2	.0
8	30000.00	758	10857	92.9	17	76000.00	505	5359	45.9	26	190000.0	335	1171	10.0					

MISSOURI RIVER AT HERMANN, MO. 06934500

LOWEST MEAN DISCHARGE, IN CFS, AND RANKING, FOR THE FOLLOWING NUMBER OF CONSECUTIVE DAYS IN YEAR ENDING MARCH 31

YEAR	1	3	7	14	30	60	90	120	183	ANNUAL
1910	15000.0 24	15000.0 19	15600.0 18	18700.0 20	20600.0 20	26200.0 23	30000.0 22	33200.0 23	33800.0 16	98100.0 33
1931	15800.0 26	15900.0 23	16700.0 21	17400.0 17	19100.0 16	22500.0 16	26800.0 17	29100.0 16	31100.0 12	47500.0 10
1932	17300.0 28	18400.0 29	20200.0 30	22900.0 31	26000.0 29	28900.0 28	32300.0 26	32400.0 22	39700.0 23	53400.0 14
1933	10700.0 8	11100.0 8	11400.0 5	15100.0 12	18100.0 12	22200.0 13	24100.0 11	27500.0 13	32400.0 14	55900.0 15
1934	12400.0 13	12800.0 13	13400.0 12	13800.0 8	15200.0 6	20300.0 10	21100.0 7	22500.0 7	27200.0 6	48100.0 11
1935	14400.0 21	15000.0 20	15300.0 17	16000.0 14	18800.0 15	21800.0 12	24300.0 12	25200.0 9	29300.0 11	37600.0 4
1936	9300.0 6	9770.0 5	11700.0 6	13400.0 6	15000.0 5	16400.0 5	23400.0 10	28700.0 15	28500.0 9	78500.0 25
1937	12600.0 15	13400.0 15	13800.0 13	16100.0 15	17400.0 11	20600.0 11	25900.0 16	28400.0 14	27800.0 8	45900.0 7
1938	8300.0 4	8430.0 3	8930.0 3	10300.0 3	12100.0 2	13500.0 2	15100.0 2	15200.0 2	19000.0 2	47000.0 9
1939	12600.0 16	13500.0 16	14600.0 16	17200.0 16	20100.0 18	22380.0 14	25300.0 14	27100.0 12	32400.0 15	62000.0 20
1940	4200.0 1	4200.0 1	4310.0 1	4810.0 1	6550.0 1	9030.0 1	11800.0 1	13000.0 1	15100.0 1	43300.0 6
1941	12200.0 12	12800.0 14	13900.0 14	15900.0 13	16600.0 9	17600.0 7	17900.0 6	19900.0 6	26700.0 5	35900.0 2
1942	14000.0 19	16400.0 25	18800.0 25	23200.0 32	31700.0 34	38800.0 33	51000.0 36	57100.0 36	67400.0 36	79000.0 26
1943	23200.0 35	24300.0 34	25400.0 35	27500.0 35	38100.0 36	43300.0 36	47100.0 34	54600.0 35	56300.0 33	87900.0 29
1944	17900.0 29	18100.0 27	18800.0 26	19100.0 21	19900.0 17	26800.0 25	29000.0 20	32100.0 21	35500.0 18	91200.0 32
1945	22900.0 34	24300.0 35	24900.0 34	26800.0 34	30700.0 33	36200.0 32	44000.0 33	44100.0 31	54400.0 32	109000.0 36
1946	10000.0 7	10500.0 5	11800.0 7	12800.0 5	18200.0 13	26500.0 24	34700.0 28	44800.0 32	50800.0 27	102000.0 34
1947	12800.0 17	15000.0 21	17000.0 23	21000.0 26	26100.0 30	27900.0 26	33000.0 27	38200.0 28	51000.0 28	61600.0 19
1948	18000.0 30	18800.0 30	20400.0 31	21500.0 29	24200.0 27	28200.0 27	32200.0 25	37600.0 27	40800.0 25	109000.0 37
1949	19500.0 32	19600.0 32	20700.0 32	22100.0 30	24400.0 28	34100.0 31	40100.0 30	41200.0 30	52300.0 30	89500.0 30
1950	24900.0 37	27400.0 37	29300.0 37	31300.0 36	32500.0 35	42000.0 35	50300.0 35	52900.0 34	59300.0 35	83600.0 27
1951	11000.0 9	12300.0 11	14600.0 15	19400.0 23	23900.0 26	25800.0 21	30200.0 23	36600.0 25	52200.0 29	90400.0 31
1952	23500.0 36	24300.0 36	27200.0 36	34400.0 37	41400.0 38	53800.0 38	66400.0 37	79000.0 38	93300.0 38	158000.0 38
1953	18900.0 31	19000.0 31	19600.0 28	21200.0 28	23500.0 25	25000.0 19	29700.0 21	37000.0 20	36100.0 20	76800.0 24
1954	12500.0 14	12800.0 12	13200.0 11	14000.0 10	16300.0 8	18800.0 8	21700.0 8	24500.0 8	28800.0 10	49600.0 13
1955	17000.0 27	18300.0 28	20100.0 29	21000.0 27	23100.0 22	25700.0 20	27400.0 18	30400.0 19	36800.0 21	49100.0 12
1956	11800.0 11	12100.0 10	12300.0 9	14200.0 11	15300.0 7	16700.0 6	17300.0 5	18200.0 3	27500.0 7	38100.0 5
1957	9000.0 5	10700.0 7	12200.0 8	13900.0 9	14900.0 4	16200.0 3	17100.0 3	18400.0 4	22800.0 3	32800.0 1
1958	15000.0 22	16300.0 24	17300.0 24	20800.0 24	23400.0 23	26100.0 22	28400.0 19	30200.0 17	35100.0 17	58500.0 17
1959	12800.0 18	13500.0 17	15700.0 19	17800.0 19	20400.0 19	23900.0 18	30400.0 24	34100.0 24	45600.0 26	73400.0 22
1960	21400.0 33	22000.0 33	24100.0 33	25600.0 33	26200.0 31	32500.0 30	40300.0 31	41000.0 29	52400.0 31	62300.0 21
1961	11000.0 10	11200.0 9	12400.0 10	13800.0 7	18500.0 14	22500.0 15	25400.0 15	30300.0 18	35600.0 19	74100.0 23
1962	28800.0 38	30500.0 38	34800.0 38	36200.0 38	39900.0 37	43500.0 37	68800.0 38	75500.0 37	83900.0 37	103000.0 35
1963	7530.0 3	8510.0 4	9290.0 4	11500.0 4	16700.0 10	19300.0 9	22000.0 9	26900.0 11	37500.0 22	57900.0 16
1964	6210.0 2	6490.0 2	7400.0 2	9360.0 2	14000.0 3	16300.0 4	17200.0 4	19000.0 5	25400.0 4	37500.0 3
1965	15400.0 25	17000.0 25	18900.0 27	20800.0 25	23500.0 24	32000.0 29	35000.0 29	36800.0 26	39800.0 24	58800.0 18
1966	15000.0 23	15900.0 22	16200.0 20	17500.0 18	30100.0 32	41000.0 34	43900.0 32	50400.0 33	58700.0 34	85100.0 28
1967	14300.0 20	14800.0 18	16900.0 22	19100.0 22	20700.0 21	23800.0 17	24300.0 13	26200.0 10	31500.0 13	46700.0 8

MISSOURI RIVER AT HERMANN, MO. 06934500

HIGHEST MEAN DISCHARGE, IN CFS, AND RANKING, FOR THE FOLLOWING NUMBER OF CONSECUTIVE DAYS IN YEAR ENDING SEPTEMBER 30

YEAR	1	3	7	15	30	60	90	120	183	ANNUAL										
1929	407000.0	7	401000.0	7	377000.0	6	309000.0	9	273000.0	6	253000.0	3	237000.0	3	217000.0	2	171000.0	2	114000.0	2
1930	164000.0	32	151000.0	32	149000.0	29	137000.0	27	109000.0	28	97800.0	25	86900.0	28	83800.0	26	75600.0	24	55400.0	25
1931	121000.0	37	94700.0	38	77500.0	38	61200.0	38	58300.0	37	54400.0	36	51900.0	36	49300.0	36	44200.0	37	37100.0	36
1932	267000.0	17	262000.0	17	233000.0	17	185000.0	19	135000.0	20	114000.0	21	97900.0	20	91400.0	21	81700.0	21	70300.0	18
1933	178000.0	29	168000.0	28	157000.0	26	145000.0	25	128000.0	21	103000.0	23	91000.0	24	86100.0	23	70900.0	27	51900.0	28
1934	82000.0	39	70600.0	39	58000.0	39	48000.0	39	46800.0	39	41000.0	39	38000.0	39	38900.0	39	35600.0	39	29800.0	39
1935	454000.0	5	450000.0	5	434000.0	5	389000.0	4	322000.0	4	247000.0	5	194000.0	7	159000.0	8	124000.0	10	80000.0	13
1936	140000.0	34	133000.0	33	118000.0	33	105000.0	31	96800.0	30	78400.0	32	71500.0	32	67600.0	32	54500.0	34	41100.0	34
1937	185000.0	27	171000.0	27	154000.0	28	137000.0	26	115000.0	27	98100.0	24	91200.0	23	85700.0	25	84300.0	20	59000.0	22
1938	229000.0	22	224000.0	22	201000.0	21	161000.0	22	142000.0	19	120000.0	19	110000.0	19	106000.0	18	89000.0	19	56600.0	24
1939	244000.0	20	232000.0	20	199000.0	22	166000.0	21	127000.0	22	105000.0	22	94900.0	21	93700.0	20	78400.0	22	53200.0	27
1940	107000.0	38	99100.0	37	83600.0	37	68600.0	37	60000.0	36	53400.0	37	50900.0	37	48100.0	37	45600.0	36	31000.0	38
1941	250000.0	19	249000.0	18	223000.0	19	159000.0	23	121000.0	25	85600.0	29	89600.0	26	76800.0	30	67400.0	30	47400.0	29
1942	425000.0	6	408000.0	6	368000.0	8	322000.0	6	247000.0	9	204000.0	9	169000.0	9	149000.0	9	122000.0	11	105000.0	5
1943	544000.0	3	519000.0	3	470000.0	2	353000.0	5	274000.0	5	253000.0	4	207000.0	5	182000.0	5	139000.0	6	96500.0	7
1944	565000.0	2	525000.0	2	464000.0	3	390000.0	3	330000.0	3	222000.0	6	202000.0	6	180000.0	6	152000.0	5	95900.0	8
1945	396000.0	9	389000.0	8	370000.0	7	301000.0	10	244000.0	10	217000.0	7	217000.0	4	209000.0	4	170000.0	3	110000.0	3
1946	202000.0	23	191000.0	24	170000.0	25	123000.0	29	88700.0	31	80800.0	31	77200.0	30	77200.0	29	74400.0	25	61900.0	20
1947	484000.0	4	478000.0	4	460000.0	4	409000.0	2	352000.0	2	260000.0	2	239000.0	2	216000.0	3	165000.0	4	108000.0	4
1948	330000.0	13	322000.0	14	298000.0	14	257000.0	14	184000.0	14	163000.0	14	131000.0	15	121000.0	15	118000.0	12	79900.0	14
1949	235000.0	21	228000.0	21	207000.0	20	198000.0	17	177000.0	15	166000.0	12	146000.0	12	142000.0	10	135000.0	7	92700.0	9
1950	263000.0	18	248000.0	19	224000.0	18	187000.0	18	155000.0	18	146000.0	16	141000.0	13	138000.0	11	125000.0	9	92200.0	10
1951	615000.0	1	600000.0	1	554000.0	1	523000.0	1	481000.0	1	344000.0	1	283000.0	1	257000.0	1	223000.0	1	139000.0	1
1952	366000.0	11	362000.0	11	347000.0	10	310000.0	8	272000.0	7	216000.0	8	181000.0	8	160000.0	7	133000.0	8	103000.0	6
1953	174000.0	31	165000.0	31	140000.0	30	116000.0	30	102000.0	29	96300.0	26	89000.0	27	89500.0	22	75700.0	23	55300.0	26
1954	142000.0	33	131000.0	34	107000.0	35	86000.0	35	84000.0	34	68700.0	34	60600.0	35	57900.0	35	52900.0	35	40800.0	35
1955	178000.0	30	167000.0	29	136000.0	32	104000.0	32	88100.0	32	75600.0	33	67000.0	33	64200.0	33	58900.0	32	47200.0	31
1956	139000.0	35	125000.0	36	98000.0	36	75000.0	36	58100.0	33	49200.0	38	47200.0	38	46100.0	38	42900.0	38	35100.0	37
1957	192000.0	25	186000.0	25	176000.0	24	155000.0	24	123000.0	24	114000.0	20	94000.0	22	86000.0	24	70900.0	28	47000.0	32
1958	337000.0	12	331000.0	12	310000.0	13	269000.0	13	240000.0	11	162000.0	15	131000.0	16	115000.0	17	106000.0	16	73500.0	17
1959	189000.0	26	180000.0	26	156000.0	27	127000.0	28	118000.0	25	93400.0	28	86300.0	29	82700.0	27	74200.0	26	57100.0	23
1960	328000.0	14	326000.0	13	317000.0	12	285000.0	11	232000.0	12	186000.0	10	150000.0	10	135000.0	12	107000.0	15	79200.0	15
1961	401000.0	8	389000.0	9	351000.0	9	274000.0	12	201000.0	13	164000.0	13	148000.0	11	129000.0	13	113000.0	13	79200.0	16
1962	275000.0	16	267000.0	15	247000.0	16	223000.0	15	171000.0	16	132000.0	17	120000.0	17	105000.0	19	100000.0	18	84900.0	11
1963	134000.0	36	130000.0	35	110000.0	34	94100.0	34	76600.0	35	64300.0	35	65700.0	34	61900.0	34	55300.0	33	45000.0	33
1964	199000.0	24	194000.0	23	179000.0	23	174000.0	20	124000.0	23	96000.0	27	90000.0	25	81700.0	28	69400.0	29	47400.0	30
1965	304000.0	15	300000.0	15	273000.0	15	198000.0	16	159000.0	17	131000.0	18	120000.0	18	119000.0	16	112000.0	14	80100.0	12
1966	182000.0	28	165000.0	30	139000.0	31	104000.0	33	87300.0	33	83300.0	30	75300.0	31	69900.0	31	67300.0	31	59800.0	21
1967	367000.0	10	363000.0	10	345000.0	11	315000.0	7	255000.0	8	174000.0	11	141000.0	14	125000.0	14	101000.0	17	66500.0	19

APPENDIX 3 (continued)

WATER RESOURCES OF THE ST. LOUIS AREA, MISSOURI

MISSOURI RIVER AT HERMANN, MO. 06934500

DURATION TABLE OF DAILY DISCHARGE FOR YEAR ENDING SEPTEMBER 30

CFS_DAYS
24258100.0

CLASS	CFS	TOTAL	ACCUM	PERCT	CLASS	CFS	TOTAL	ACCUM	PERCT	CLASS	CFS	TOTAL	ACCUM	PERCT	CLASS	CFS	TOTAL	ACCUM	PERCT
0	0.00	0	14244	100.0	9	14000.00	214	14024	98.5	18	54000.0	1227	6277	44.1	27	210000	178	609	4.2
1	4200.00	8	14244	100.0	10	16000.00	479	13810	97.0	19	63000.0	898	5050	35.5	28	240000	180	431	3.0
2	4900.00	5	14236	99.9	11	19000.00	552	13331	93.6	20	73000.0	768	4152	29.1	29	280000	122	251	1.7
3	5700.00	6	14231	99.9	12	22000.00	728	12779	89.7	21	85000.0	773	3384	23.8	30	330000	55	129	.9
4	6600.00	7	14225	99.9	13	26000.00	746	12051	84.6	22	99000.0	698	2611	18.3	31	380000	39	74	.5
5	7700.00	10	14218	99.8	14	30000.00	864	11305	79.4	23	120000.0	229	1913	13.4	32	450000	28	35	.2
6	8900.00	30	14208	99.7	15	35000.00	1284	10441	73.3	24	130000.0	570	1684	11.8	33	520000	5	7	.0
7	10000.00	38	14178	99.5	16	40000.00	1634	9157	64.3	25	160000.0	261	1114	7.8	34	600000	2	2	.0
8	12000.00	116	14140	99.3	17	47000.00	1246	7523	52.8	26	180000.0	244	853	6.0					

MISSISSIPPI RIVER AT ST. LOUIS, MO. 07010000

LOWEST MEAN DISCHARGE, IN CFS, AND RANKING, FOR THE FOLLOWING NUMBER OF CONSECUTIVE DAYS IN YEAR ENDING MARCH 31

YEAR	1	3	7	14	30	60	90	120	183	ANNUAL
1934	35200.0 4	36600.0 4	40100.0 5	41800.0 6	44200.0 5	50700.0 5	52100.0 4	54100.0 4	59600.0 4	120000.0 7
1935	39900.0 7	40500.0 7	42600.0 7	45200.0 7	50200.0 8	56700.0 13	62200.0 11	64100.0 9	68600.0 8	100000.0 5
1936	43800.0 10	44100.0 8	46600.0 9	50600.0 14	51300.0 10	55000.0 8	67000.0 12	77800.0 17	76400.0 11	179000.0 24
1937	39700.0 6	39900.0 6	40400.0 6	41200.0 5	43000.0 4	49300.0 4	60200.0 10	70900.0 12	71400.0 9	125000.0 10
1938	27800.0 1	28200.0 2	29800.0 2	34700.0 2	40900.0 3	45900.0 3	47200.0 2	48100.0 2	57900.0 2	124000.0 8
1939	49100.0 18	51900.0 19	56700.0 20	58800.0 19	65400.0 21	75800.0 24	85200.0 24	91300.0 24	114000.0 25	177000.0 22
1940	28000.0 2	28100.0 1	28200.0 1	28700.0 1	30900.0 1	35700.0 1	41000.0 1	42600.0 1	45100.0 1	110000.0 6
1941	46500.0 15	47200.0 14	48000.0 12	48900.0 9	49600.0 7	51600.0 6	56200.0 6	61400.0 7	71700.0 10	92700.0 3
1942	57100.0 22	57800.0 22	59200.0 22	60200.0 21	62200.0 18	80000.0 25	113000.0 31	129000.0 31	161000.0 33	191000.0 28
1943	76200.0 33	78100.0 33	79500.0 33	84000.0 34	108000.0 35	125000.0 34	136000.0 34	142000.0 33	153000.0 32	206000.0 29
1944	66700.0 27	66700.0 26	66800.0 26	67000.0 25	67700.0 22	71400.0 18	75300.0 19	81600.0 20	87300.0 18	210000.0 30
1945	69000.0 29	69000.0 29	69200.0 28	69500.0 27	70700.0 26	73700.0 21	82900.0 23	84100.0 22	103000.0 23	221000.0 32
1946	69000.0 30	70300.0 30	71200.0 30	71700.0 28	76600.0 28	89300.0 28	98000.0 28	116000.0 28	132000.0 30	240000.0 35
1947	70100.0 31	72200.0 32	73000.0 31	76100.0 30	88700.0 30	91900.0 29	97500.0 27	108000.0 27	127000.0 28	157000.0 17
1948	41500.0 8	44100.0 9	47600.0 10	50200.0 10	58500.0 15	70400.0 16	80600.0 22	84800.0 23	87100.0 17	237000.0 34
1949	52100.0 20	53800.0 20	55500.0 19	58000.0 17	62300.0 19	72100.0 19	74200.0 18	74300.0 15	95100.0 22	171000.0 20
1950	57900.0 23	59600.0 23	62600.0 24	63100.0 23	67900.0 25	66800.0 27	91700.0 26	96000.0 25	115000.0 26	165000.0 19
1951	42300.0 9	44800.0 10	50200.0 16	56900.0 16	60000.0 16	65900.0 15	69400.0 15	73200.0 13	92500.0 21	188000.0 26
1952	80600.0 36	82100.0 36	85900.0 35	89800.0 35	112000.0 36	144000.0 36	162000.0 36	180000.0 36	199000.0 36	307000.0 36
1953	58000.0 24	59800.0 24	61900.0 23	63700.0 24	67800.0 24	70600.0 17	74100.0 17	73700.0 14	85500.0 14	180000.0 25
1954	45500.0 14	47900.0 15	49000.0 13	50400.0 12	52400.0 11	55600.0 11	59800.0 8	61900.0 8	66000.0 6	125000.0 9
1955	64600.0 25	65400.0 25	66600.0 25	67200.0 26	71300.0 27	84500.0 26	87900.0 25	97300.0 26	109000.0 24	144000.0 14
1956	44400.0 11	44800.0 11	46000.0 8	47100.0 8	50800.0 9	52000.0 7	52900.0 5	57300.0 6	67700.0 7	100000.0 4
1957	45000.0 13	45700.0 13	47800.0 11	51400.0 15	54800.0 13	55500.0 10	56400.0 7	57100.0 5	61800.0 5	91700.0 2
1958	55400.0 21	56500.0 21	57300.0 21	61100.0 22	67700.0 23	74300.0 22	79600.0 21	82700.0 21	85600.0 15	142000.0 13
1959	47600.0 16	48300.0 16	49100.0 14	50400.0 13	53400.0 12	56200.0 12	67000.0 13	70700.0 11	87700.0 19	149000.0 15
1960	65800.0 26	67000.0 27	68700.0 27	77100.0 31	90400.0 31	101000.0 31	112000.0 30	122000.0 29	127000.0 29	155000.0 16
1961	49000.0 17	49000.0 17	49300.0 15	50200.0 11	54900.0 14	60200.0 14	67300.0 14	77000.0 16	87000.0 16	191000.0 27
1962	77000.0 34	78900.0 34	82100.0 34	83100.0 33	96900.0 32	120000.0 32	133000.0 32	158000.0 35	181000.0 35	218000.0 31
1963	35800.0 5	37100.0 5	38400.0 4	40900.0 4	48600.0 6	55200.0 9	60100.0 9	67700.0 10	90000.0 20	163000.0 18
1964	34600.0 3	35400.0 3	36400.0 3	37200.0 3	39800.0 2	45500.0 2	47700.0 3	52800.0 3	58000.0 3	91500.0 1
1965	50600.0 19	50600.0 18	52700.0 18	58800.0 20	60800.0 17	72100.0 20	71700.0 16	80300.0 19	81300.0 12	129000.0 11
1966	70600.0 32	71500.0 31	73200.0 32	77600.0 32	104000.0 33	135000.0 35	135000.0 33	144000.0 34	175000.0 34	226000.0 33
1967	44700.0 12	45600.0 12	52300.0 17	58200.0 18	63300.0 20	75500.0 23	77500.0 20	78200.0 18	82000.0 13	132000.0 12
1968	67700.0 28	68200.0 28	69600.0 29	73500.0 29	87100.0 29	94700.0 30	107000.0 29	122000.0 30	126000.0 27	179000.0 23
1969	77200.0 35	81200.0 35	88400.0 36	93500.0 36	106000.0 34	123000.0 33	138000.0 35	138000.0 32	149000.0 31	177000.0 21

MISSISSIPPI RIVER AT ST. LOUIS, MO. 07010000

HIGHEST MEAN DISCHARGE, IN CFS, AND RANKING, FOR THE FOLLOWING NUMBER OF CONSECUTIVE DAYS IN YEAR ENDING SEPTEMBER 30

YEAR	1	3	7	15	30	60	90	120	183	ANNUAL
1934	136000.0 36	134000.0 36	131000.0 36	124000.0 36	112000.0 36	98400.0 36	90100.0 36	85400.0 36	78800.0 36	67700.0 36
1935	649000.0 8	641000.0 8	621000.0 7	560000.0 7	486000.0 8	428000.0 8	364000.0 9	325000.0 10	274000.0 10	188000.0 13
1936	332000.0 29	326000.0 29	292000.0 29	274000.0 28	268000.0 24	240000.0 25	223000.0 27	201000.0 27	154000.0 31	114000.0 31
1937	372000.0 24	365000.0 24	330000.0 25	299000.0 24	264000.0 27	235000.0 26	233000.0 25	231000.0 22	209000.0 21	147000.0 23
1938	431000.0 21	426000.0 21	401000.0 21	357000.0 21	343000.0 18	293000.0 19	279000.0 18	268000.0 16	231000.0 16	157000.0 19
1939	529000.0 15	514000.0 16	473000.0 17	396000.0 17	332000.0 20	302000.0 18	252000.0 20	242000.0 19	202000.0 22	148000.0 22
1940	184000.0 35	178000.0 35	164000.0 35	145000.0 35	136000.0 35	125000.0 35	127000.0 35	119000.0 35	111000.0 35	79100.0 35
1941	451000.0 20	446000.0 20	422000.0 20	344000.0 22	267000.0 25	212000.0 30	210000.0 28	192000.0 29	161000.0 28	120000.0 29
1942	663000.0 7	649000.0 7	608000.0 8	539000.0 10	459000.0 11	375000.0 12	323000.0 13	308000.0 11	270000.0 13	236000.0 4
1943	833000.0 2	820000.0 2	786000.0 2	670000.0 4	557000.0 4	516000.0 3	445000.0 5	400000.0 5	323000.0 6	235000.0 5
1944	834000.0 1	829000.0 1	789000.0 1	711000.0 3	611000.0 3	487000.0 4	449000.0 4	404000.0 4	326000.0 5	209000.0 9
1945	610000.0 11	608000.0 11	591000.0 11	547000.0 9	508000.0 7	449000.0 7	458000.0 3	434000.0 3	347000.0 3	223000.0 7
1946	500000.0 18	494000.0 18	468000.0 18	387000.0 19	327000.0 21	261000.0 22	245000.0 21	234000.0 21	224000.0 19	173000.0 15
1947	783000.0 3	777000.0 3	765000.0 3	736000.0 1	687000.0 1	531000.0 1	510000.0 1	463000.0 2	350000.0 2	237000.0 3
1948	629000.0 9	622000.0 9	597000.0 9	529000.0 12	427000.0 14	339000.0 14	296000.0 16	263000.0 18	241000.0 15	163000.0 18
1949	422000.0 22	418000.0 22	394000.0 22	363000.0 20	339000.0 19	332000.0 16	292000.0 17	267000.0 17	247000.0 14	170000.0 16
1950	461000.0 19	449000.0 19	429000.0 19	396000.0 18	378000.0 16	351000.0 13	333000.0 12	308000.0 12	271000.0 12	199000.0 11
1951	779000.0 4	772000.0 4	754000.0 4	719000.0 2	664000.0 2	522000.0 2	485000.0 2	475000.0 1	408000.0 1	265000.0 1
1952	682000.0 5	679000.0 5	664000.0 5	612000.0 5	548000.0 5	467000.0 5	403000.0 6	358000.0 8	301000.0 7	233000.0 6
1953	367000.0 25	361000.0 25	334000.0 24	296000.0 26	265000.0 26	250000.0 24	230000.0 26	226000.0 23	200000.0 23	141000.0 25
1954	289000.0 33	277000.0 33	258000.0 33	234000.0 33	226000.0 30	218000.0 28	206000.0 30	188000.0 30	160000.0 29	114000.0 30
1955	309000.0 30	295000.0 30	269000.0 31	237000.0 32	210000.0 33	194000.0 31	192000.0 31	182000.0 31	159000.0 30	130000.0 27
1956	225000.0 34	206000.0 34	183000.0 34	174000.0 34	165000.0 34	151000.0 34	138000.0 34	133000.0 34	120000.0 34	94000.0 34
1957	338000.0 28	329000.0 28	327000.0 26	299000.0 23	272000.0 23	255000.0 23	234000.0 23	223000.0 25	182000.0 26	123000.0 28
1958	504000.0 17	499000.0 17	477000.0 16	431000.0 16	385000.0 15	292000.0 20	240000.0 22	215000.0 26	200000.0 24	145000.0 24
1959	362000.0 26	348000.0 26	311000.0 28	290000.0 27	254000.0 28	230000.0 27	233000.0 24	225000.0 24	191000.0 25	136000.0 26
1960	667000.0 6	663000.0 6	648000.0 6	609000.0 6	528000.0 6	460000.0 6	403000.0 7	361000.0 7	285000.0 8	208000.0 10
1961	588000.0 12	578000.0 13	543000.0 13	449000.0 15	368000.0 17	335000.0 15	312000.0 14	274000.0 15	228000.0 17	167000.0 17
1962	588000.0 13	583000.0 12	568000.0 12	535000.0 11	476000.0 10	379000.0 11	341000.0 11	308000.0 13	273000.0 11	219000.0 8
1963	299000.0 32	291000.0 32	258000.0 32	240000.0 31	230000.0 29	189000.0 33	189000.0 33	174000.0 32	147000.0 32	113000.0 32
1964	306000.0 31	293000.0 31	277000.0 30	252000.0 30	212000.0 32	191000.0 32	190000.0 32	168000.0 33	140000.0 33	99600.0 33
1965	549000.0 14	544000.0 14	518000.0 14	498000.0 14	458000.0 12	389000.0 10	353000.0 10	328000.0 9	278000.0 9	198000.0 12
1966	410000.0 23	365000.0 23	342000.0 23	297000.0 25	275000.0 22	263000.0 21	253000.0 19	237000.0 20	213000.0 20	174000.0 14
1967	528000.0 16	525000.0 15	518000.0 15	503000.0 13	435000.0 13	315000.0 17	305000.0 15	285000.0 14	228000.0 18	156000.0 20
1968	344000.0 27	339000.0 27	317000.0 27	273000.0 29	218000.0 31	214000.0 29	210000.0 29	200000.0 28	175000.0 27	156000.0 21
1969	616000.0 10	613000.0 10	596000.0 10	558000.0 8	477000.0 9	398000.0 9	382000.0 8	383000.0 6	330000.0 4	243000.0 2

APPENDIX 3 (continued)

MISSISSIPPI RIVER AT ST. LOUIS, MO. 07010000

DURATION TABLE OF DAILY DISCHARGE FOR YEAR ENDING SEPTEMBER 30

CLASS	CFS	TOTAL	ACCUM	PERCT	CLASS	CFS	TOTAL	ACCUM	PERCT	CLASS	CFS	TOTAL	ACCUM	PERCT	CLASS	CFS	TOTAL	ACCUM	PERCT
0	0.00	0	13149	100.0	9	63000.00	669	11686	88.9	18	160000.0	808	5184	39.4	27	410000	188	665	5.0
1	27800.00	19	13149	100.0	10	70000.00	885	11017	83.8	19	180000.0	629	4376	33.3	28	450000	148	477	3.6
2	31000.00	18	13130	99.9	11	78000.00	671	10132	77.1	20	200000.0	656	3747	28.5	29	500000	127	329	2.5
3	34000.00	33	13112	99.7	12	86000.00	832	9461	72.0	21	220000.0	522	3091	23.5	30	550000	90	202	1.5
4	38000.00	62	13079	99.5	13	96000.00	932	8629	65.6	22	240000.0	565	2569	19.5	31	610000	64	112	.8
5	42000.00	167	13017	99.0	14	110000.00	606	7697	58.5	23	270000.0	424	2004	15.2	32	680000	27	48	.3
6	47000.00	296	12850	97.7	15	120000.00	517	7091	53.9	24	300000.0	333	1580	12.0	33	750000	18	21	.1
7	52000.00	407	12554	95.5	16	130000.00	506	6574	50.0	25	330000.0	349	1247	9.5	34	830000	3	3	.0
8	57000.00	461	12147	92.4	17	140000.00	884	6068	46.1	26	370000.0	233	898	6.8					

APPENDIX 4

Compilation of miscellaneous quality of surface-water data collected in the St. Louis area, 1967-70

Map number	Date of collection	Discharge (cfs)	Temperature (°C)	Milligrams per liter																		Hardness as CaCO ₃		Specific conductance (microhm at 25°C)	pH	Color	Turbidity (JTU)	Chemical oxygen demand, mg/l	Dissolved oxygen		Colonies per 100 milliliters																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																	
				Silica (SiO ₂)	Iron (Fe)	Manganese (Mn)	Calcium (Ca)	Magnesium (Mg)	Sodium (Na)	Potassium (K)	Organic nitrogen (N)	Ammonia nitrogen (N)	Bicarbonate (HCO ₃)	Sulfate (SO ₄)	Chloride (Cl)	Fluoride (F)	Nitrate (NO ₃)	Phosphorus (PO ₄)	Detergents (NDAS)	Dissolved solids (residue at 180°C)	Calcium magnesium	Noncarbonate	Milligrams per liter						Percent saturation	Total coliform	Fecal coliform	Fecal streptococci																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																
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4	11-3-70	-----	10.0	15	1.5 <u>u</u>	.30 <u>u</u>	54	8.3	6.7	3.1	----	Cuivre River near Old Monroe, Mo.																		---	---	239	170	27	380	7.6	--	--	--	10.5	93	2100	1000	200																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																				

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APPENDIX 5

Summary of annual average water-quality characteristics of the Missouri River
at Howard Bend Plant near St. Louis, Missouri, 1951-70; analyses by City of St. Louis

Annual average for year ending March 31	Milligrams per liter														Color	Turbidity (JTU)	pH	Temperature (°C)	Total coliform (Col/100 ml)
	Silica (SiO2)	Iron oxide (Fe2O3) and aluminum oxide (Al2O3)	Calcium (Ca)	Magnesium (Mg)	Sodium (Na) and potassium (K)	Carbonate (CO3)	Bicarbonate (HCO3)	Sulfate (SO4)	Chloride (Cl)	Fluoride (F)	Nitrate (NO3)	Dissolved solids (residue at 105°C)	Alkalinity as CaCO3	Hardness as CaCO3					
1951-----	13	0.5	52	14	41	0	172	107	19	---	5.7	344	140	188	18	1,760	8.1	13	7,500
1952-----	12	0.3	52	14	30	0	168	81	17	---	5.8	313	137	189	15	1,400	8.0	13	6,800
1953-----	14	0.4	59	18	47	0	198	125	21	C.4	5.2	402	165	223	12	1,100	8.2	14	5,500
1954-----	14	0.2	60	19	57	0	196	162	23	C.5	4.6	403	162	230	11	760	8.1	15	5,300
1955-----	11	0.8	53	16	51	0	169	118	21	C.5	5.8	370	138	196	15	890	8.0	15.5	5,200
1956-----	11	1.5	56	17	58	0	182	139	26	0.5	4.5	410	149	211	13	500	8.0	15	4,000
1957-----	11	0.9	54	18	55	0	178	136	26	0.5	4.4	404	146	207	14	500	8.2	15.5	4,000
1958-----	10	0.9	50	15	43	0	160	107	24	0.4	5.2	339	132	185	17	700	8.0	15	9,800
1959-----	12	3.5	53	14	42	0	176	98	24	0.4	4.6	338	144	192	20	700	8.0	15	5,100
1960-----	12	1.3	55	16	44	0	183	103	23	0.5	4.4	351	151	204	19	900	8.1	15	5,400
1961-----	12	1.2	57	16	46	0	187	107	22	0.4	4.9	367	153	208	18	850	8.1	14.5	19,000
1962-----	11	1.2	51	13	34	0	170	80	17	0.3	4.5	302	139	183	21	700	8.1	14	8,500
1963-----	13	1.1	64	18	49	0	206	119	23	0.5	5.4	425	169	233	19	700	8.2	15	8,700
1964-----	12	0.8	64	19	63	0	199	157	29	0.5	4.6	479	163	238	15	475	8.1	15	6,800
1965-----	10	0.9	55	15	54	0	170	130	24	0.5	4.8	391	140	200	16	860	8.0	15	13,000
1966-----	10	1.4	58	14	42	0	185	112	23	0.4	4.2	362	153	204	16	700	8.1	14.5	21,000
1967-----	11	1.8	59	18	59	0	198	143	26	0.4	3.6	436	165	220	16	309	8.0	14	5,100
1968-----	9.2	1.2	55	15	49	0	180	120	21	0.4	3.3	384	148	201	18	364	8.0	14	9,900
1969-----	11	1.0	55	14	46	0	163	120	21	0.4	5.7	378	138	194	17	383	8.1	14	12,000
1970-----	10	0.8	57	16	43	0	190	109	20	0.4	4.5	383	156	208	13	396	8.0	13.5	19,000

APPENDIX 6

Summary of annual average water-quality characteristics of the Mississippi River
at Chain of Rocks Plant at St. Louis, Missouri, 1951-70; analyses by City of St. Louis

Annual average for year ending March 31	Silica (SiO2)	Milligrams per liter												Color	Turbidity (JTU)	pH	Temperature (°C)	Total coliform (Col/100 ml)	
		Iron oxide (Fe2O3) and aluminum oxide (Al2O3)	Calcium (Ca)	Magnesium (Mg)	Sodium (Na) and potassium (K)	Carbonate (CO3)	Bicarbonate (HCO3)	Sulfate (SO4)	Chloride (Cl)	Fluoride (F)	Nitrate (NO3)	Dissolved solids (residue at 105°C)	Alkalinity as CaCO3						Hardness as CaCO3
1951-----	13	0.4	50	14	38	1	162	101	18	----	5.8	325	135	186	17	1,400	7.8	13.5	7,300
1952-----	14	0.3	51	15	32	1	166	82	18	----	5.5	311	138	189	18	1,200	7.8	14.5	19,000
1953-----	15	0.2	57	18	46	1	190	122	21	0.3	5.3	381	158	217	14	960	8.0	15.5	7,700
1954-----	14	0.2	58	19	56	1	187	153	23	0.4	4.5	423	155	225	15	700	8.0	15.5	5,600
1955-----	12	0.3	53	16	45	1	164	114	23	0.4	6.1	364	136	195	17	850	8.0	15.5	7,700
1956-----	11	0.3	55	17	51	1	176	130	26	0.3	5.8	409	146	207	15	400	8.0	15	4,900
1957-----	10	0.4	53	17	50	1	171	131	25	0.4	4.5	393	142	203	16	400	7.9	15.5	5,600
1958-----	11	0.3	51	14	37	1	156	102	23	0.3	4.7	341	131	185	19	630	7.9	14.5	10,000
1959-----	11	0.3	52	14	35	1	167	90	23	0.3	4.3	331	139	188	19	565	8.0	15	10,000
1960-----	12	0.3	56	15	37	1	181	95	24	0.3	4.9	348	150	202	19	775	8.0	14.5	8,900
1961-----	11	0.3	57	15	40	1	185	98	27	0.3	6.4	356	154	206	17	700	8.1	14.5	9,300
1962-----	11	0.3	52	13	30	1	168	75	21	0.3	5.9	300	139	185	20	662	8.1	14	16,000
1963-----	13	0.4	63	18	30	1	202	87	27	0.3	5.8	399	168	230	17	568	8.2	14	13,000
1964-----	12	0.2	62	19	39	1	197	104	31	0.4	5.5	450	163	233	13	342	8.2	15	7,200
1965-----	11	0.4	54	15	49	1	169	127	22	0.3	5.0	379	140	197	16	711	8.2	14	31,000
1966-----	11	0.4	54	16	40	1	174	109	19	0.3	5.0	354	144	198	16	626	8.2	15	31,000
1967-----	9.8	0.6	58	18	53	1	186	141	23	0.4	4.4	409	159	219	13	258	8.0	14.5	10,000
1968-----	10	0.5	54	16	48	0	176	118	21	0.3	6.2	381	144	198	13	352	8.1	14.5	7,900
1969-----	11	0.2	54	14	47	0	170	121	20	0.2	5.3	370	130	194	13	348	8.2	14	48,000
1970-----	13	0.2	57	15	39	0	180	106	21	0.2	3.6	372	148	206	14	442	8.1	14.5	25,000

APPENDIX 7

DEFINITION OF TERMS AND
CONVERSION OF UNITS

Acre-foot — The volume of water required to cover one acre to a depth of 1 foot.

1 acre-foot = 43,560 cubic feet
= 325,851 gallons

Alluvium — A general term for all detrital deposits resulting from the operations of modern rivers, thus including the sediments laid down in riverbeds, floodplains and lakes.

Anticline — A fold or arch of rock strata, dipping in opposite directions from an axis.

Aquifer — A formation, group of formations, or part of a formation that contains sufficient saturated permeable material to yield significant quantities of water to wells and springs.

Artesian water — Ground water under sufficient pressure to rise above the level at which the water-bearing bed is reached in a well. Ground water under artesian pressure is also called confined water.

Confining bed — A body of relatively impermeable material stratigraphically adjacent to one or more aquifers.

Connate water — Water entrapped in interstices of a sedimentary rock at the time the rock was deposited.

Continuous-record station — A site on a stream where continuous records of discharge are obtained.

Cubic feet per second (cfs) — The unit expressing rate of discharge. One cfs is the rate of discharge of a stream having a cross-sectional area of 1 square foot and an average velocity of 1 foot per second.

1 cfs = 7.48 U.S. Gallons per second
= 449 U.S. Gallons per minute
= 0.646 millions of U.S. gallons per day.

Disconformity — An unconformity in which the beds on opposite sides are parallel.

Dolomite — A term applied to rocks that approximate the mineral dolomite [$\text{CaMg}(\text{CO}_3)_2$] in composition.

Epicontinental sea — Those shallow portions of the sea which lie upon the continental shelf, and those portions which extend into the interior of the continent with like shallow depths, such as the Baltic Sea and Hudson Bay.

Evapotranspiration — The movement of water into the atmosphere by the combined processes of direct evaporation and transpiration by plants.

Fault — A fracture or fracture zone in the rocks along which there has been displacement of the two sides relative to one another, parallel to the fracture.

Groundwater reservoir — See aquifer.

Hydrology — The science that relates to the water of the earth.

Intermittent stream — A stream that flows only part of the time or through only part of its reach.

Lithology — The physical character of a rock.

Loess — A sediment, commonly nonstratified and unconsolidated, composed dominantly of silt-size particles, with accessory clay and sand, deposited primarily by the wind.

Low flow — The portion of stream discharge that is derived primarily from groundwater outflow.

Partial-record station — A site on a stream where occasional discharge measurements have been collected over a period of years.

Perennial stream — A stream that flows continuously throughout its reach.

Permeability — A measure of the relative ease with which a porous medium can transmit a liquid under a potential gradient.

Porosity — The property of a rock or soil containing voids.

Potentiometric surface — A surface which represents the static head. As related to an aquifer it is defined by the levels to which water will rise in tightly cased wells.

Recharge — The addition of water to the zone of saturation. Infiltration of precipitation is a form of natural recharge.

Recurrence interval — The average interval of time within which a given event will be exceeded once. Recurrence intervals are averages and do not imply regularity of occurrence; an event of 50-year recurrence interval might be exceeded in consecutive years or it might not be exceeded in a 100-year period. In other words, a 50-year drought or flood has a 2-percent chance of occurrence in any year.

Regional dip — The general inclination of strata over a large area in which they dip in one direction with or without interruptions.

Residual errors — Ratio of observed values of stream-flow characteristics at gaging stations to the values computed from equations.

Seepage run — A series of discharge measurements made in a short time to identify stream reaches where gains or losses in flow occur.

7-day Q_2 — The annual minimum average discharge for seven consecutive days that will occur on an average of once in 2 years. This is an index to the low-flow potential of a stream and can be used as a guide in comparing one stream to another.

Soil infiltration index — This value is the maximum potential difference, in inches, between storm rainfall and storm runoff. It is dependent on soil-water storage and infiltration rates of a watershed.

Specific capacity — The rate of discharge of water from a well divided by the drawdown of water level in the well. If a well yields 500 gpm with a drawdown of 25 feet, its specific capacity is $500/25$ or 20 gpm per foot of drawdown.

Specific conductance — A measure of the capacity of water to conduct a current of electricity, expressed in micromhos per centimeter at 25°C. Conductance varies with the quantities of dissolved mineral constituents and with the degree of ionization of the constituents as well as with the temperature of the water. It is useful in indicating the approximate concentration of mineral matter in water.

Standard error of estimate — A measure of the reliability of a regression. It is the standard deviation of the distribution of residuals about the regression line.

Storage coefficient — The volume of water an aquifer releases from or takes into storage per unit surface area of the aquifer per unit change in head.

Transmissivity — The rate at which water of the prevailing kinematic viscosity is transmitted through a unit width of the aquifer under a unit hydraulic gradient.

Transpiration — The process by which water vapor escapes from a living plant and enters the atmosphere.

Tributary streams — Those streams that originate in or have much of their drainage basin in the project area.

Unconformity — A surface of erosion or nondeposition that separates younger strata from older rocks.

Water table — That surface in an unconfined water body at which the pressure is atmospheric.

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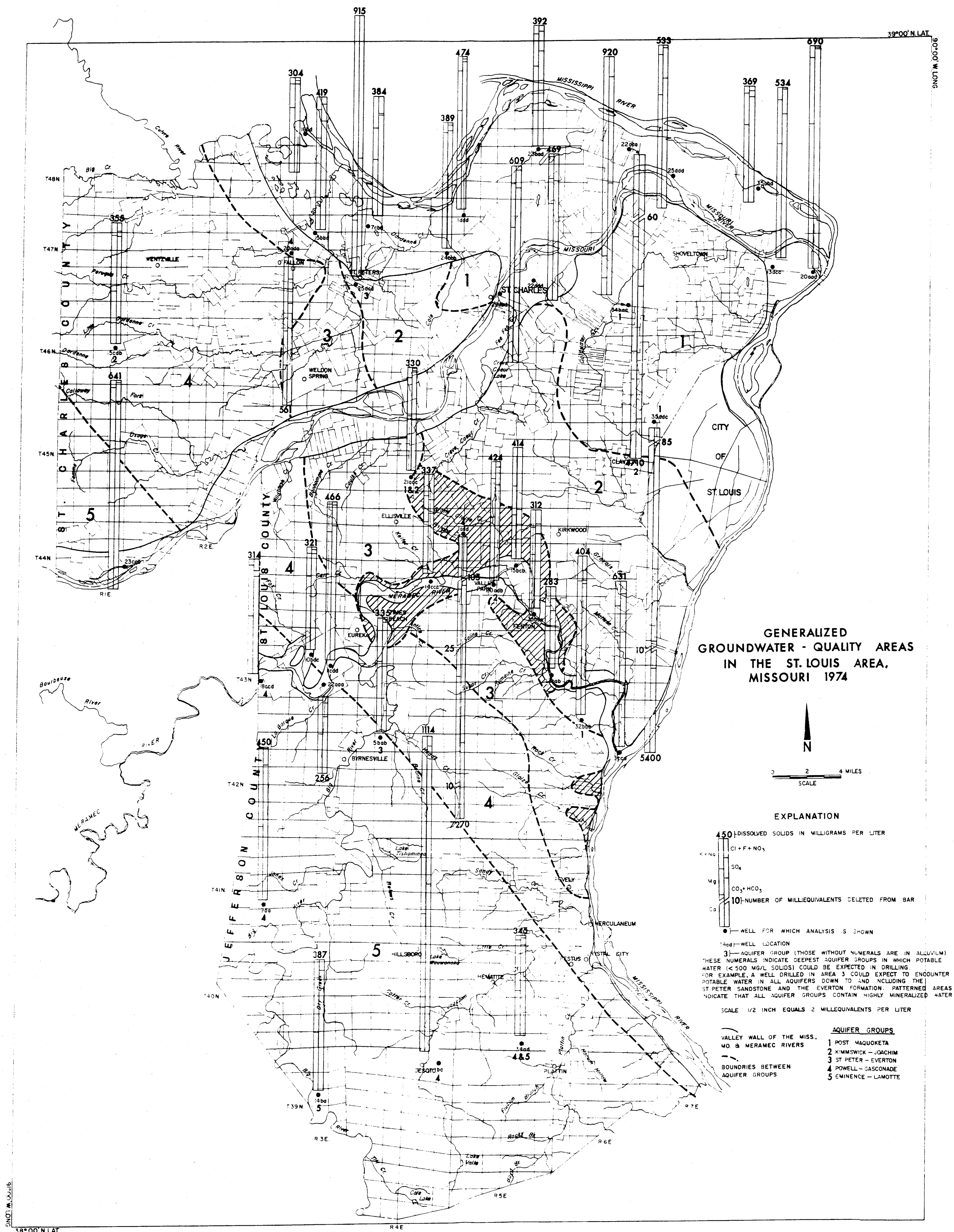
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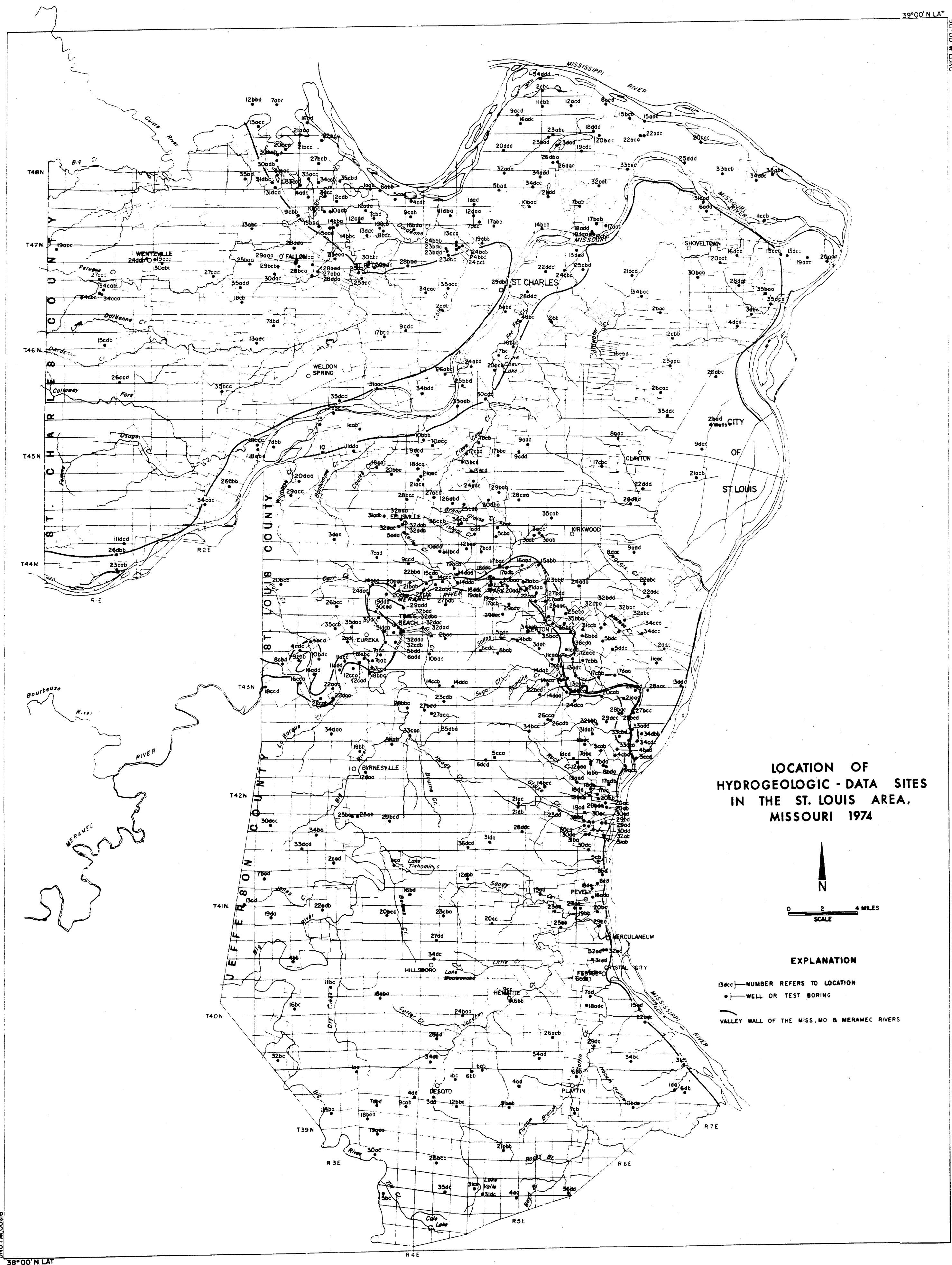
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